

MASSACHUSETTS INSTITUTE OF TECHNOLOGY  
Department of Electrical Engineering and Computer Science

6.002x – Circuits and Electronics  
Spring 2004

Problem Set 9

Issued: 21 April 2004

**Quiz 3 will be on Friday, May 7 in your recitation section**

**Reading:** Finish reading chapter 4 from Bose and Stevens *Introductory Network Theory* (copies were distributed in lecture on April 5)

**To write up and hand in at lecture on Monday, May 3.**

This is the last problem set of the semester. (Hooray!)

For this assignment, you are to write up and hand in the following problems from chapter 4 of Bose and Stevens:

- Problem 4-20. Note: The notation “cps” means “cycles per second”. This notation was replaced by “Hertz” in the late 70’s.

– Part a

$$H(s_p) = \frac{V_2}{V_1} \quad (1)$$

$$H(s_p) = \frac{R}{R + \frac{1}{sC}} \quad (2)$$

$$H(s_p) = \frac{s}{s + \frac{1}{RC}} \quad (3)$$

There is a pole at  $\frac{-1}{RC}$  and a zero at zero.

The magnitude of  $H(s_p)$  starts from 0 and increases by 20db per decade until it hits 1. The breakpoint frequency is  $\omega = \frac{1}{RC}$ .

The phase starts at 90 degrees and decreases to 0, intersecting 45 degrees at  $\omega = \frac{1}{RC}$ .

– Part b

The half-power frequency is the frequency for which the magnitude of the system function is  $\frac{1}{\sqrt{2}}$  its maximum. Since the maximum magnitude of the system is 1, we need to find the frequency where  $H(j\omega) = \frac{1}{\sqrt{2}}$ . This happens at  $\omega = \frac{1}{RC}$ .

Setting  $f = \frac{\omega}{2\pi} = \frac{\frac{1}{RC}}{2\pi} = \frac{1}{2\pi RC} = 5000$ , we get  $C = 1.9\mu F$

- Problem 4-24.

– Part a

The voltage transfer ratio  $H(s_p)$  can be obtained as follows:

$$H(s_p) = \frac{\frac{1}{sC}}{\frac{1}{sC} + sL + R} \quad (4)$$

$$H(s_p) = \frac{\frac{1}{LC}}{s^2 + \frac{R}{L}s + \frac{1}{LC}} \quad (5)$$

The system function has 2 poles and no zeros. The two poles are given by the roots of the denominator, where  $p_1 = \frac{-R}{2L} + j\sqrt{\frac{1}{LC} - \frac{R^2}{4L^2}}$  and  $p_2 = \frac{-R}{2L} + j\sqrt{\frac{1}{LC} + \frac{R^2}{4L^2}}$

– Part b

$$\alpha = \frac{R}{2L} \quad (6)$$

$$\omega_d = \sqrt{\frac{1}{LC} - \frac{R^2}{4L^2}} \quad (7)$$

$$\omega_o = \sqrt{\frac{1}{LC}} \quad (8)$$

– Part c

We find the frequency at which  $|H(j\omega)|$  is maximum.

$$H(j\omega) = \frac{\frac{1}{LC}}{(-\omega^2 + \frac{1}{LC}) + \frac{R}{L}j\omega} \quad (9)$$

$$|H(j\omega)| = \frac{\frac{1}{LC}}{\sqrt{(-\omega^2 + \frac{1}{LC})^2 + (\frac{R}{L}\omega)^2}} \quad (10)$$

Thus,  $|H(j\omega)|$  will be maximum when  $\omega^2 = \frac{1}{LC}$ . The frequency is  $\frac{1}{2\pi\sqrt{LC}}$ .

For systems where  $\alpha \ll \omega$  (stated in this problem), the half power points are at  $\omega_d + \alpha$  and  $\omega_d - \alpha$ . The frequencies are  $\frac{\omega_d + \alpha}{2\pi}$  and  $\frac{\omega_d - \alpha}{2\pi}$

– Part d

Looking at the pole-zero diagram, the magnitude of the system starts at a constant and peaks at the resonance frequency of  $\omega = \frac{1}{\sqrt{LC}}$ . As  $\omega$  increases further, the magnitude decreases at the rate of 40db per decade.

The phase of the system starts at 0 degrees and hits -90 degrees at the resonance frequency. At large  $\omega$ , the phase approaches -180 degrees.

Figure 1 shows the magnitude and phase of such a system.

– Part e

$$Q = \frac{\omega}{2\alpha} \quad (11)$$

$$\text{Bandwidth} = 2\alpha \quad (12)$$

– Part f

$v_2(t) = V_o(1 - \frac{\omega_o}{\omega_d}e^{-\alpha t}\cos(\omega_d t - \tan^{-1}(\frac{\alpha}{\omega_d})))$ , where  $V_o = 1$ . See page 889-893 in Agarwal and Lang for detailed derivation.

As  $Q$  changes from low to high, the amount of ringing changes accordingly.

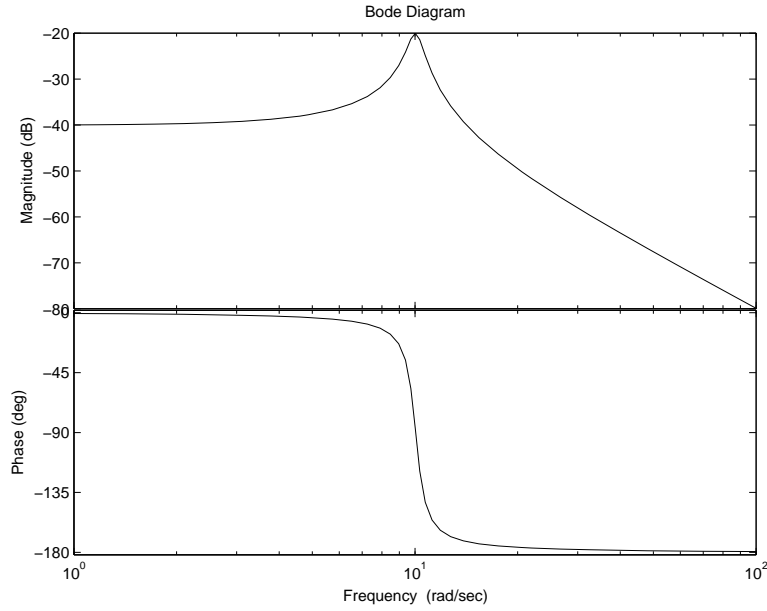


Figure 1: Bode Plot

- Problem 4-31.

–  $Z(s_p) = \frac{s_p}{s_p+1}$

For circuit shown in Figure 2,  $Z(s_p) = \frac{s_p L R}{s_p L + R} = \frac{s_p}{s_p+1}$

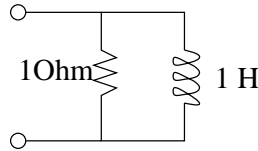


Figure 2: Circuit with  $Z(s_p)$  for 4-31, Part 1

–  $Z(s_p) = \frac{s_p+2}{s_p+1}$

Expressing the impedance as sum of two impedances in series, we get  $Z(s_p) = \frac{s_p+2}{s_p+1} = \frac{s_p}{s_p+1} + \frac{2}{s_p+1}$

Circuit shown in Figure 3 shows the correct component values which will result in the above  $Z(s_p)$ .

–  $Z(s_p) = 2 \frac{s_p^2+2s_p+2}{s_p(s_p+1)}$

The circuit shown in Figure 4 will give the correct impedance.

–  $Z(s_p) = \frac{s_p^2+1}{s_p(s_p^2+2)}$

The circuit shown in Figure 5 will give the correct impedance.

$$Z(s_p) = (s_p L_1 + \frac{1}{s_p C_1}) \parallel \frac{1}{s_p C_2} \quad (13)$$

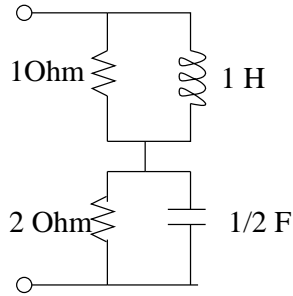


Figure 3: Circuit with  $Z(s_p)$  for 4-31, Part 2

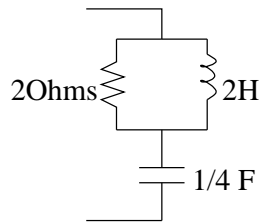


Figure 4: Circuit with  $Z(s_p)$  for 4-31, Part 3

$$Z(s_p) = \frac{s_p^2 L_1 C_1 + 1}{s_p(s_p^2 C_1 C_2 L_1 + (C_1 + C_2))} \quad (14)$$

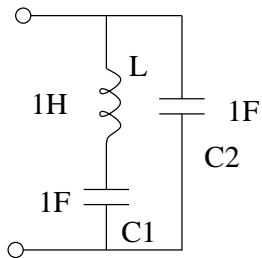


Figure 5: Circuit with  $Z(s_p)$  for 4-31, Part 4

- Problem 4-44.

We start by writing the system function for the three networks.

- Network 1

$$Z(s_p) = R_1 + \frac{s_p L R_2}{s_p L + R_2} \quad (15)$$

$$Z(s_p) = \frac{s_p(L R_2 + L R_1) + R_1 R_2}{s_p L + R_2} \quad (16)$$

- Network 2

$$Z(s_p) = s_p L \parallel (R + \frac{1}{s_p C}) \quad (17)$$

$$Z(s_p) = \frac{s_p L (s_p C R + 1)}{s_p^2 L C + R C s_p + 1} \quad (18)$$

– Network 3

$$Z(s_p) = \frac{1}{s_p C_1} \parallel (R + \frac{1}{s_p C_2}) \quad (19)$$

$$Z(s_p) = \frac{s_p R C_2 + 1}{s_p (C_1 + C_2) + s_p^2 C_1 C_2 R} \quad (20)$$

1. Property 1

Looking at the system functions, the 2 pole, 1 zero system corresponds to Network 3.

2. Property 2

This does not correspond to any network.

3. Property 3

The voltage response of  $v(t) = Ae^{-3t} - Be^{-t}$  suggests that the system has 2 complex poles, resulting in a response in the form of  $Ae^{st} + Be^{st}$ . Thus, network 2 could have this property.

4. Property 4

$|Z(j\omega) = \sqrt{\frac{\omega^2+1}{\omega^2+2}}$  implies a single pole and single zero system. Thus, network 1 could have this property.

5. Property 5

None of the networks will have this property.

6. Property 6

Voltage across the inductor is  $L \frac{di}{dt}$ , when the current changes from 0 to 1 (step current source), the voltage across the inductor will have a discontinuity. Network 1, 2 could have this property.