Continuous Curves

Justin Solomon

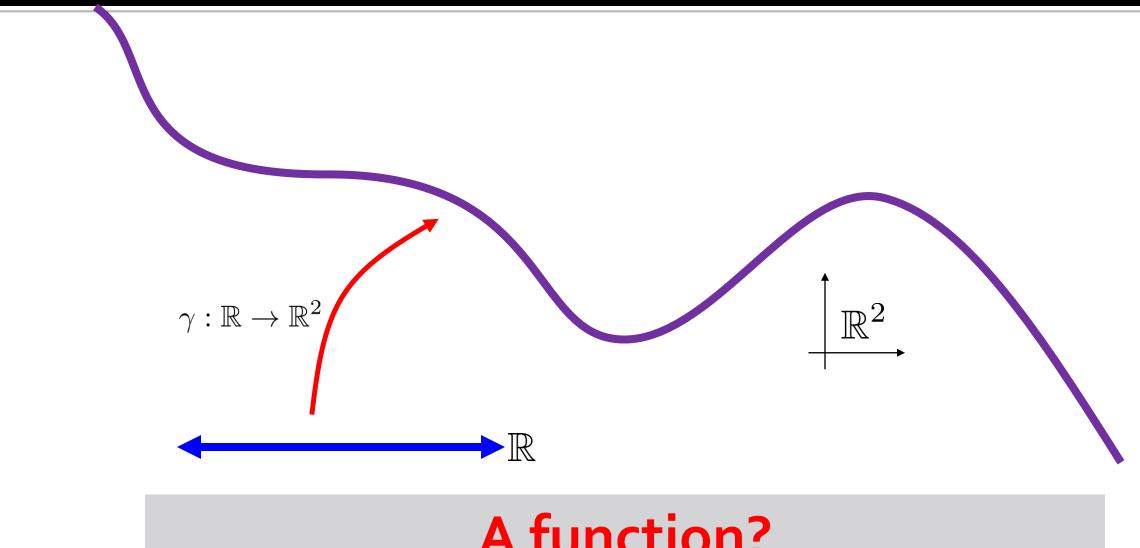
6.8410: Shape Analysis
Spring 2023





What is a curve?

Defining "Curve"



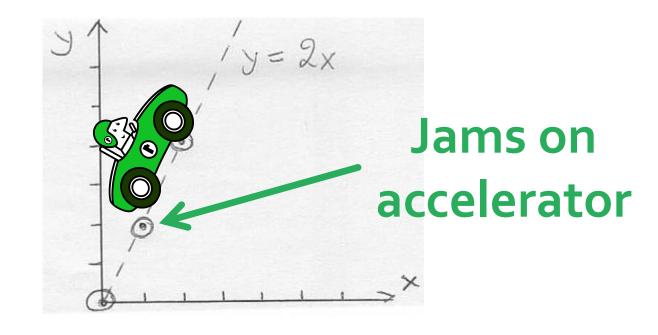
A function?

Subtlety

$$\gamma(t) \equiv (0,0)$$

Not a curve

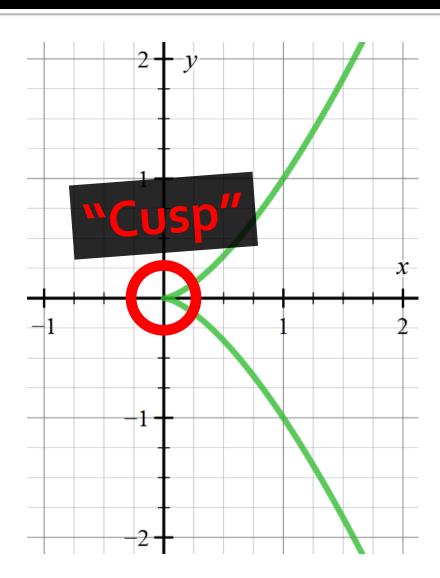
Different from Calculus



$$\gamma_1(t) = (t, 2t)$$

$$\gamma_2(t) = \begin{cases} (t, 2t) & t \le 1 \\ (2(t - \frac{1}{2}), 4(t - \frac{1}{2}) & t > 1 \end{cases}$$

Graphs of Smooth Functions



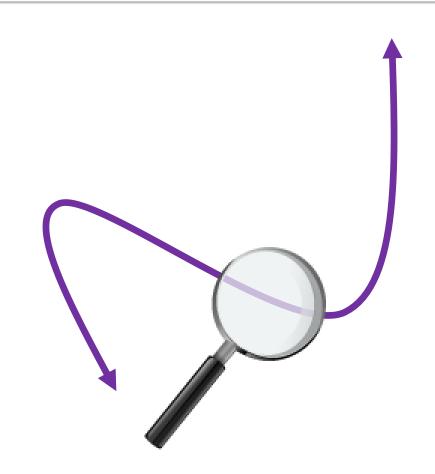
$$\gamma(t) = (t^2, t^3)$$

Geometry of a Curve

A curve is a set of points with certain properties.

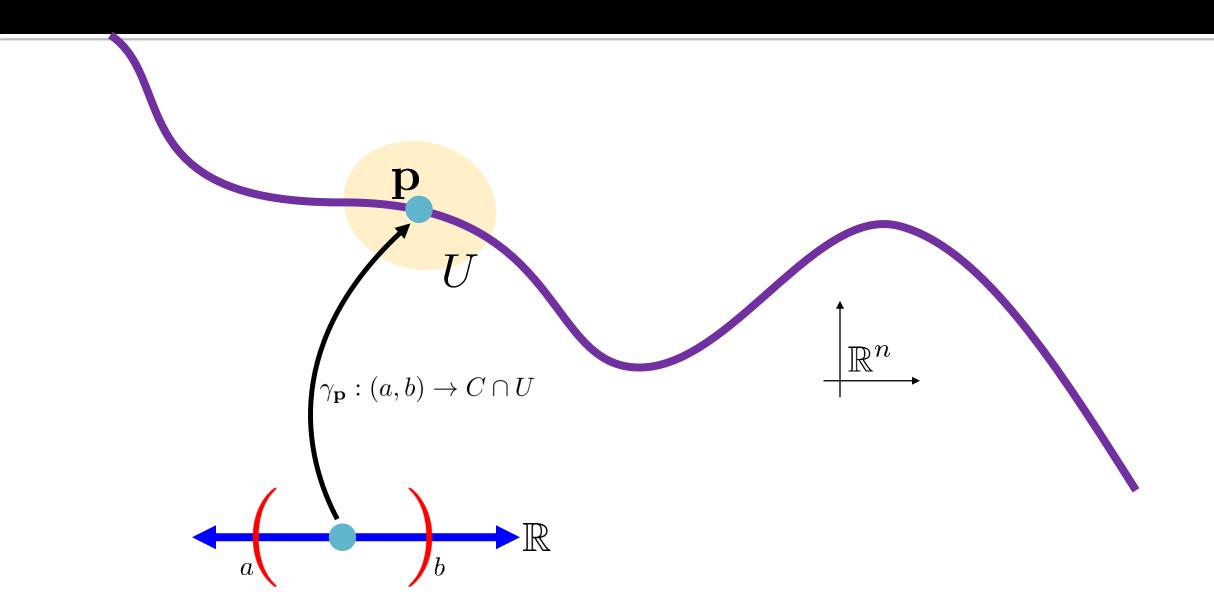
It is not a function.

Geometric Definition

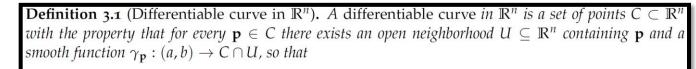


Set of points that locally looks like a line.

Differential Geometry Definition

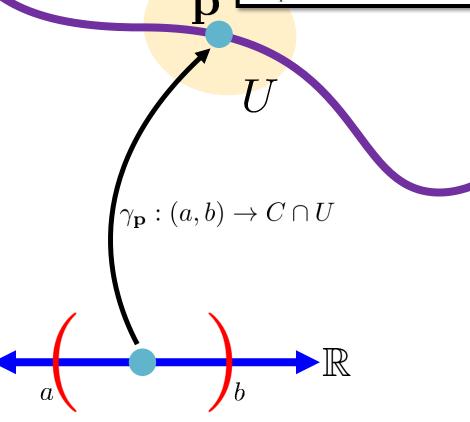


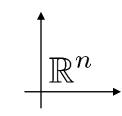
Formal Statement



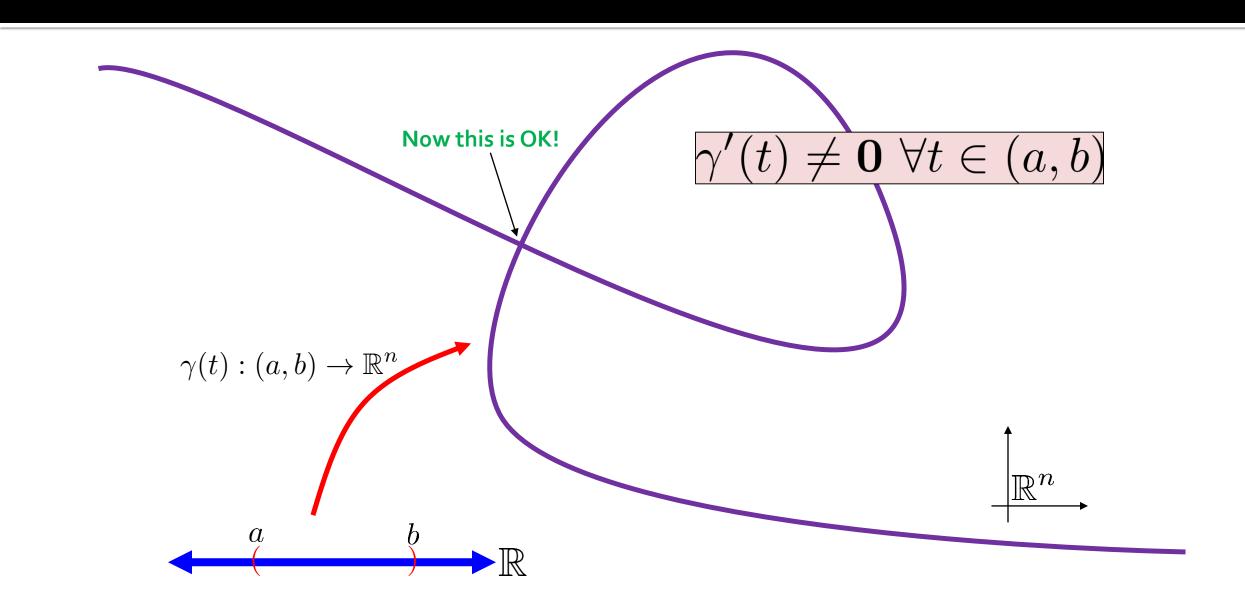
$$C \cap U = \{ \gamma_{\mathbf{p}}(t) : t \in (a, b) \}$$

and $\gamma'_{\mathbf{p}}(t) \neq \mathbf{0}$ for all $t \in (a,b)$. The function $\gamma_{\mathbf{p}}$ is known as a local parameterization of C at \mathbf{p} .





Parameterized Curve



Some Vocabulary

Trace of parameterized curve

$$\{\gamma(t):t\in(a,b)\}\subseteq\mathbb{R}^n$$

Component functions

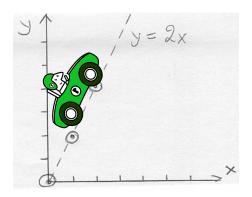
$$\gamma(t) = (x(t), y(t), z(t))$$

Change of Parameter

$$t \mapsto \gamma \circ \phi(t)$$

Geometric measurements should be invariant

to changes of parameter.



Dependence of Velocity

$$\tilde{\gamma}(t) := \gamma(\phi(t))$$

Effect on velocity and acceleration?

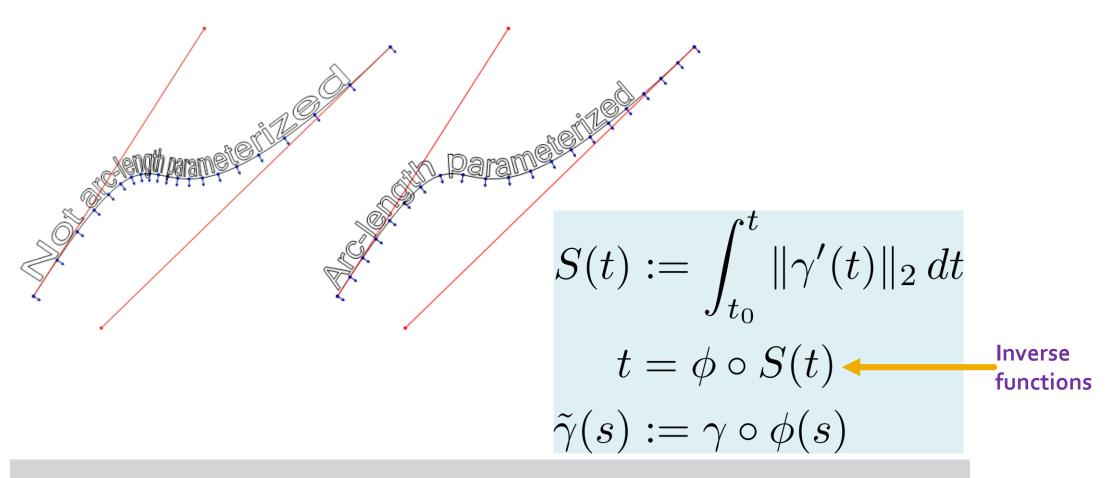
Arc Length

$$\int_a^b \|\gamma'(t)\|_2 dt$$

Independent of parameter!

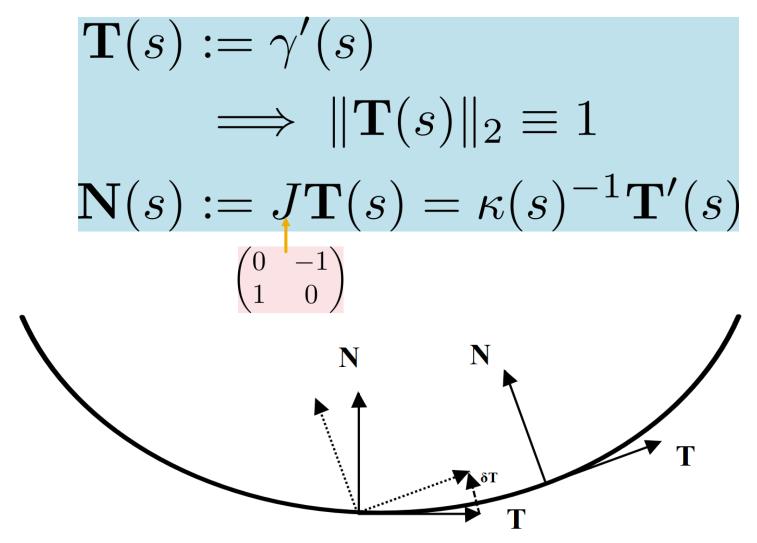
Parameterization by Arc Length

http://www.planetclegg.com/projects/WarpingTextToSplines.html



Constant-speed parameterization

Moving Frame in 2D



Philosophical Point

Differential geometry "should" be coordinate-invariant.

Referring to x and y is a hack!

(but sometimes convenient...)

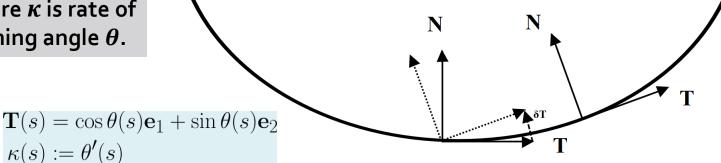


How do you describe a curve without coordinates?

Turtles All The Way Down

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix} := \begin{pmatrix} 0 & \kappa(s) \\ -\kappa(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix}$$

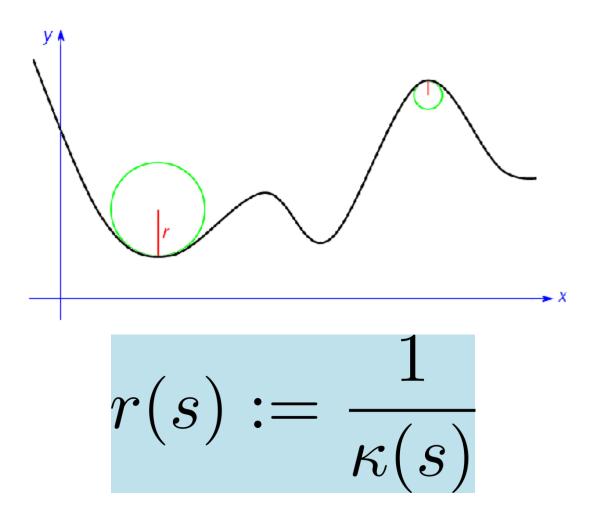
Signed curvature κ is rate of change of turning angle θ .



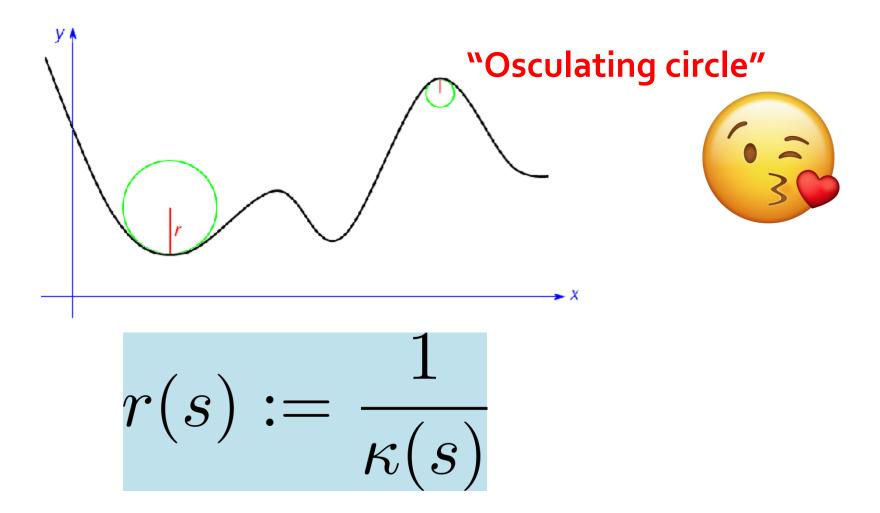
https://en.wikipedia.org/wiki/Frenet%E2%80%93Serret_formulas

Use coordinates *from* the curve to express its shape!

Radius of Curvature



Radius of Curvature



Fundamental theorem of the local theory of plane curves:

 $\kappa(s)$ distinguishes a planar curve up to rigid motion.

Fundamental theorem of the local theory of plane curves:

 $\kappa(s)$ distinguishes a planar curve up to rigid motion.

Statement shorter than the name!

Idea of Proof

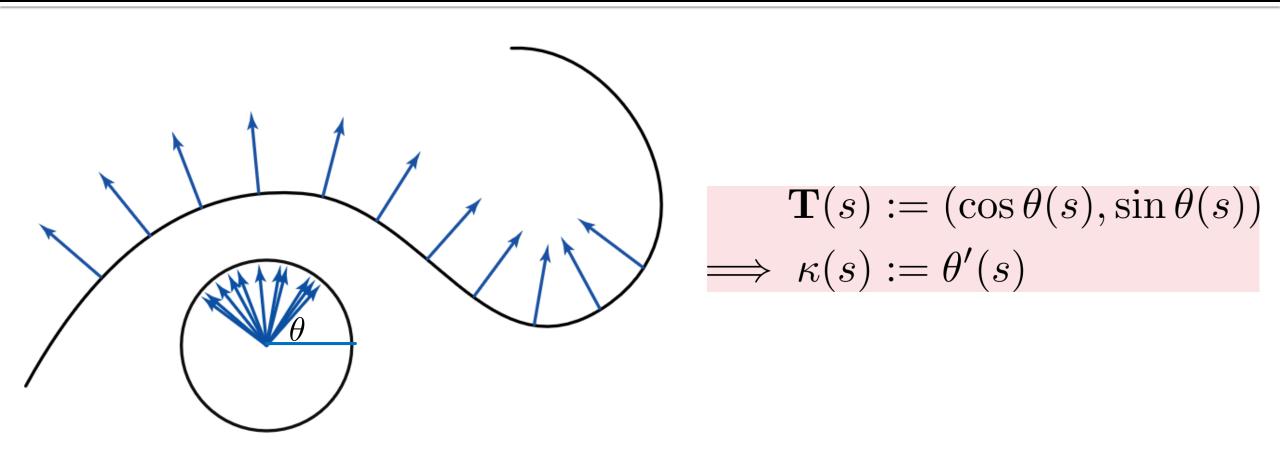
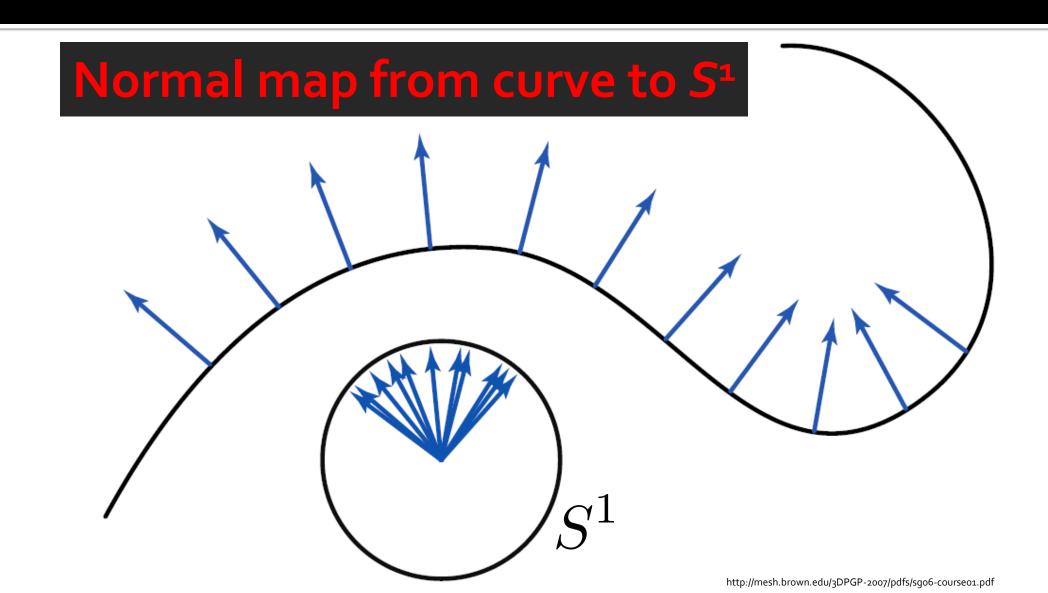


Image from DDG course notes by E. Grinspun

Provides intuition for curvature

Gauss Map



Winding Number

$$W[\gamma] := \frac{1}{2\pi} \int_{a}^{b} \kappa(s) \, ds \in \mathbb{Z}$$

 $W[\gamma]$ is an integer, and smoothly deforming γ does not affect $W[\gamma]$.

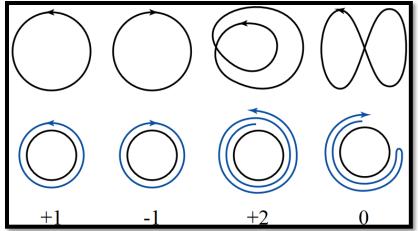
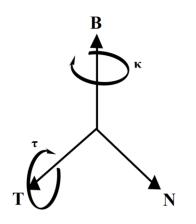


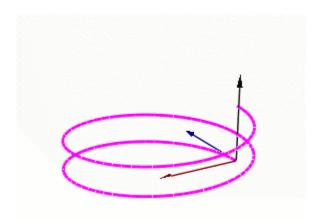
Image from: Grinspun and Secord, "The Geometry of Plane Curves" (SIGGRAPH 2006)

Frenet Frame: Curves in \mathbb{R}^3

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

- **Binormal:** $T \times N$
- Curvature: In-plane motion
- Torsion: Out-of-plane motion





Fundamental theorem of the local theory of space curves:

Curvature and torsion distinguish a 3D curve up to rigid motion.

Aside: Generalized Frenet Frame

$$\gamma(s): \mathbb{R} \to \mathbb{R}^n$$

$$\frac{d}{ds} \begin{pmatrix} \mathbf{e}_{1}(s) \\ \mathbf{e}_{2}(s) \\ \vdots \\ \mathbf{e}_{n}(s) \end{pmatrix} = \begin{pmatrix} 0 & \chi_{1}(s) & & & \\ -\chi_{1}(s) & \ddots & & \ddots & \\ & \ddots & & 0 & & \chi_{n-1}(s) \\ & & & -\chi_{n-1}(s) & & 0 \end{pmatrix} \begin{pmatrix} \mathbf{e}_{1}(s) \\ \mathbf{e}_{2}(s) \\ \vdots \\ \mathbf{e}_{n}(s) \end{pmatrix}$$

Suspicion: Application to time series analysis? ML?

C. Jordan, 1874

Gram-Schmidt on first *n* derivatives

Continuous Curves

Justin Solomon

6.8410: Shape Analysis
Spring 2023



Discrete Curves

Justin Solomon

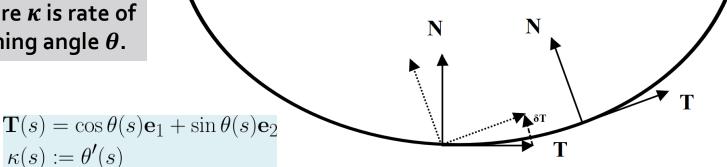
6.8410: Shape Analysis
Spring 2023



Frenet Frame: Curves in \mathbb{R}^2

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix} := \begin{pmatrix} 0 & \kappa(s) \\ -\kappa(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix}$$





https://en.wikipedia.org/wiki/Frenet%E2%80%93Serret_formulas

Use coordinates *from* the curve to express its shape!

Winding Number

$$W[\gamma] := \frac{1}{2\pi} \int_{a}^{b} \kappa(s) \, ds \in \mathbb{Z}$$

 $W[\gamma]$ is an integer, and smoothly deforming γ does not affect $W[\gamma]$.

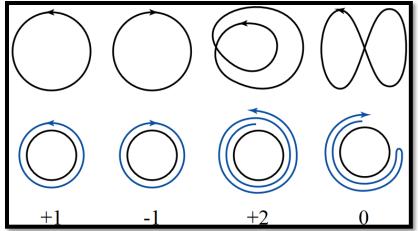
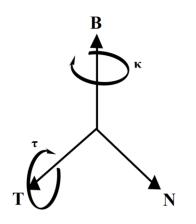


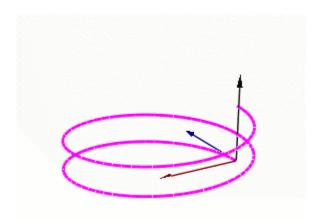
Image from: Grinspun and Secord, "The Geometry of Plane Curves" (SIGGRAPH 2006)

Frenet Frame: Curves in \mathbb{R}^3

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

- Binormal: $T \times N$
- Curvature: In-plane motion
- Torsion: Out-of-plane motion

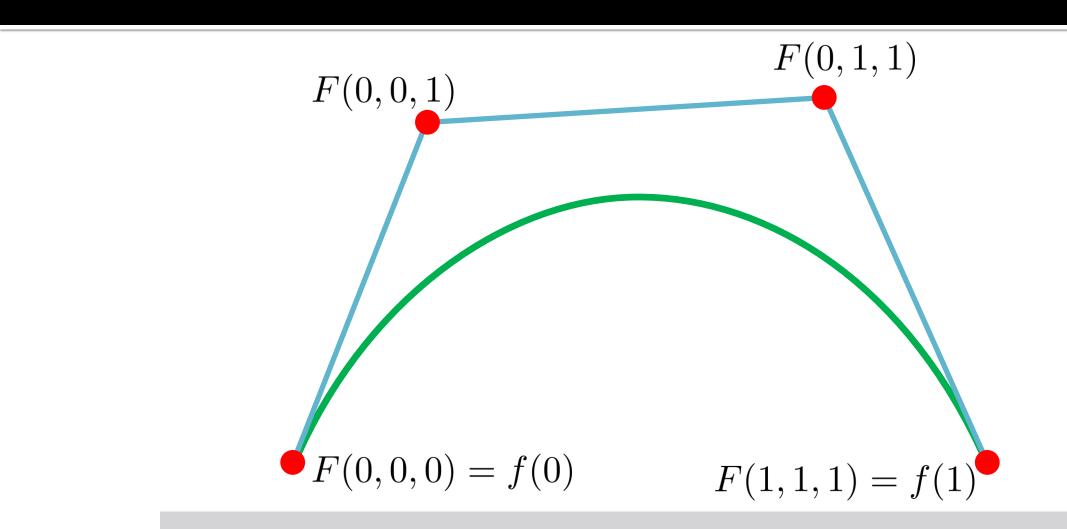






What do these calculations look like in software?

Old-School Approach



Piecewise smooth approximations

Question

What is the arc length of a cubic Bézier curve?

$$\int_a^b \|\gamma'(t)\|_2 dt$$

Question

What is the arc length of a cubic Bézier curve?

$$\int_a^b \|\gamma'(t)\|_2 dt$$

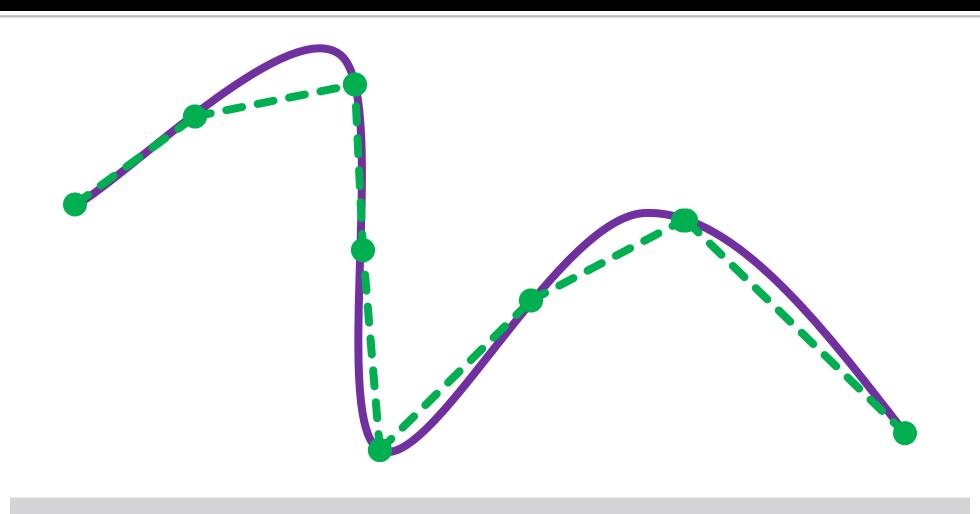
Not known in closed form.

Sad fact: **Closed-form** expressions rarely exist. When they do exist, they usually are messy.

Only Approximations Anyway

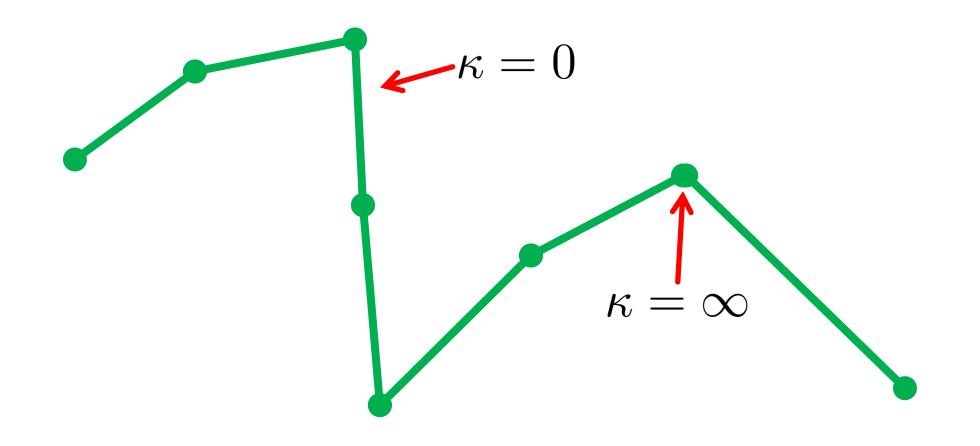
$$\{\text{B\'ezier curves}\} \subseteq \{\gamma : \mathbb{R} \to \mathbb{R}^3\}$$

Simpler Approximation



Piecewise linear: Poly-line

Big Problem



Boring differential structure

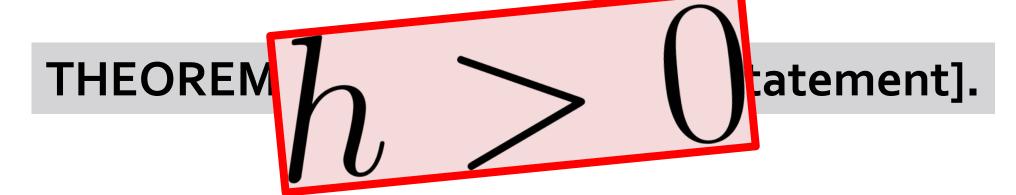
Finite Difference Approach

$$f'(x) \approx \frac{1}{h} [f(x+h) - f(x)]$$

THEOREM: As $\Delta h \rightarrow 0$, [insert statement].

Reality Check

$$f'(x) \approx \frac{1}{h} [f(x+h) - f(x)]$$



Two Key Considerations

Convergence to continuous theory

Discrete behavior

Goal

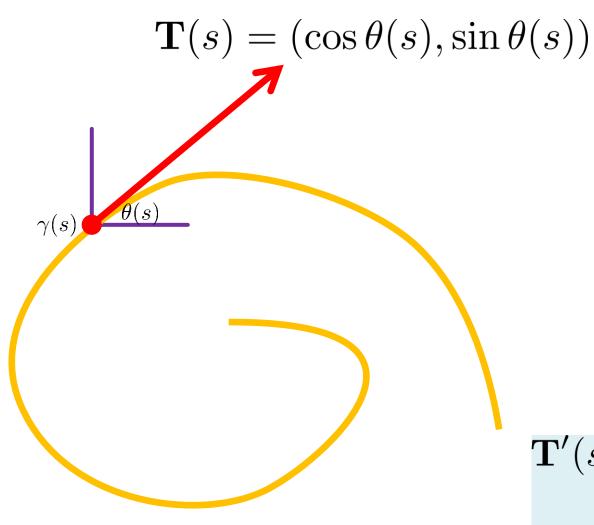
Examine discrete theories of differentiable curves.

Goal

Examine discrete theor<u>ies</u> of differentiable curves.

Recall:

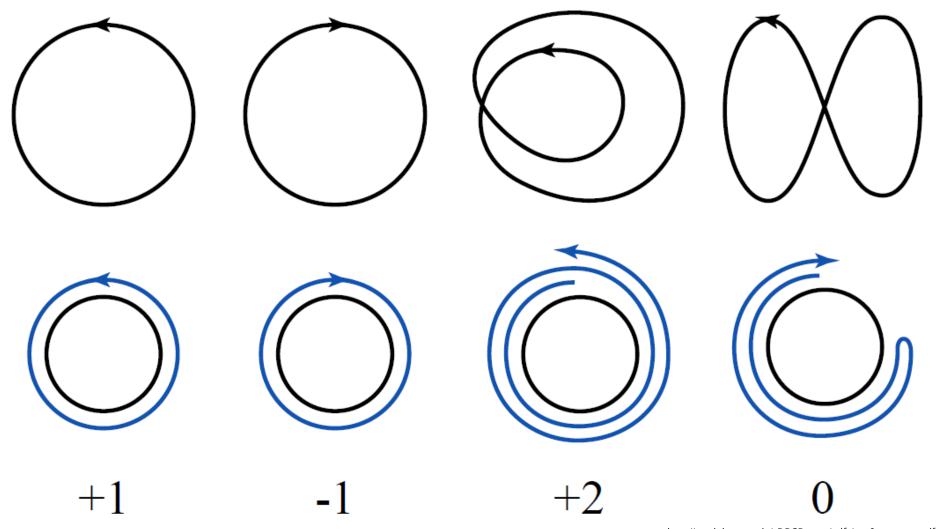
Signed Curvature on Plane Curves



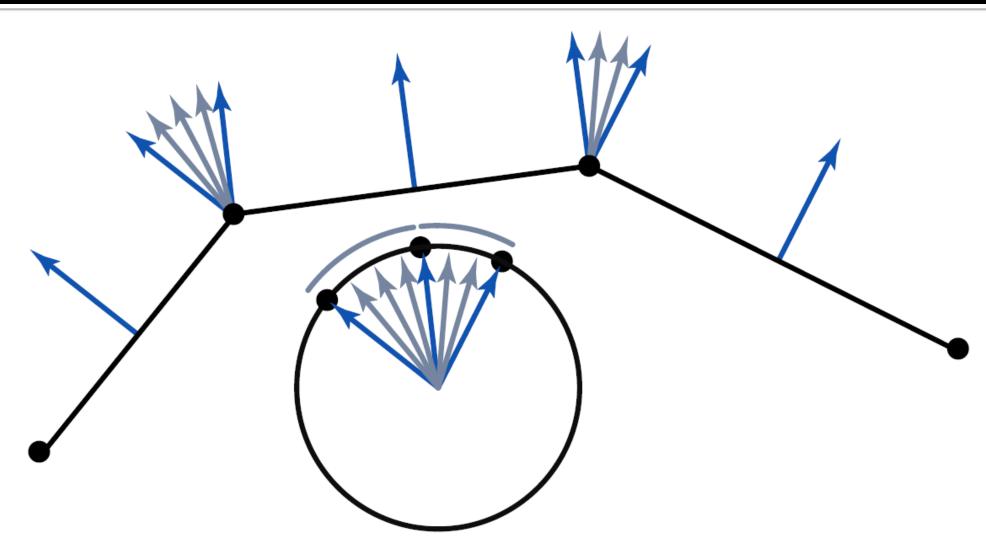
Gauss map: Map from curve to its normals.

$$\mathbf{T}'(s) = \theta'(s)(-\sin\theta(s), \cos\theta(s))$$
$$:= \kappa(s)\mathbf{N}(s)$$

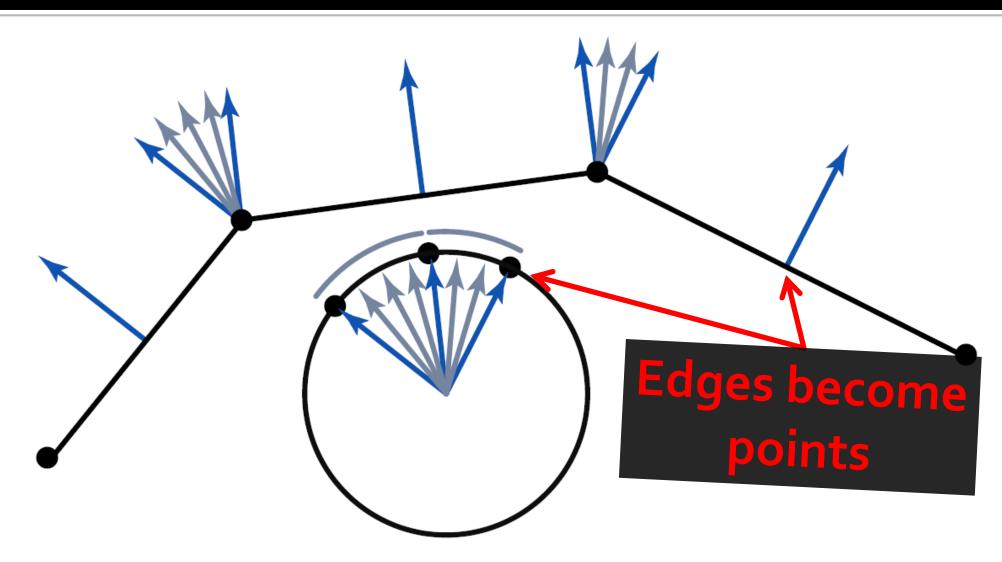
Turning Numbers



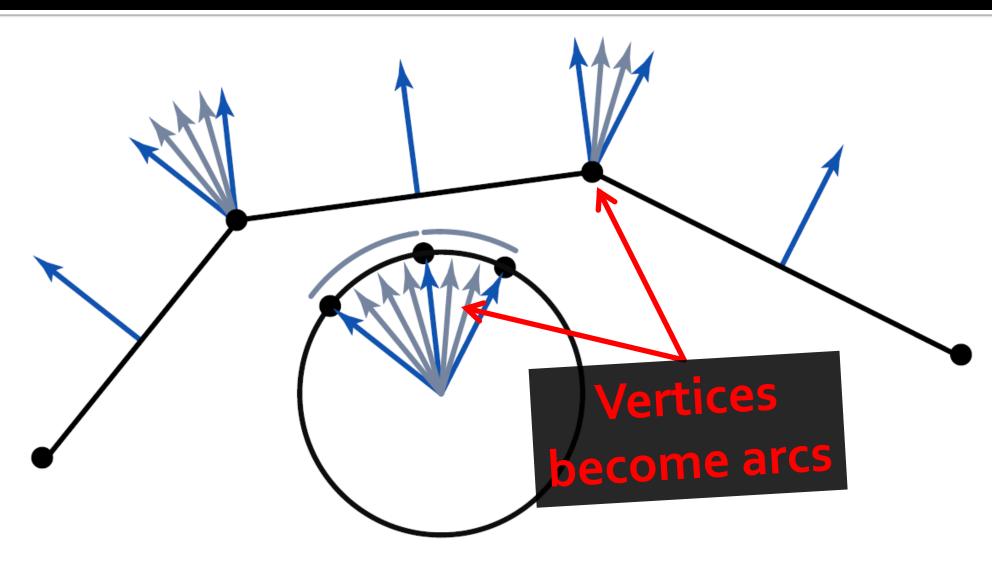
Discrete Gauss Map



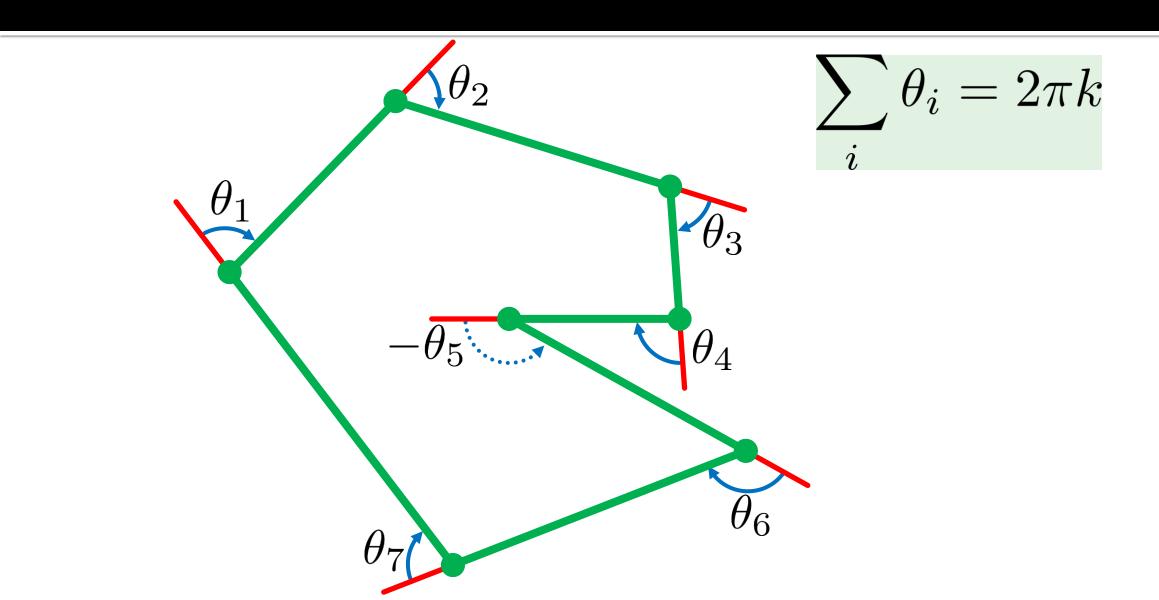
Discrete Gauss Map



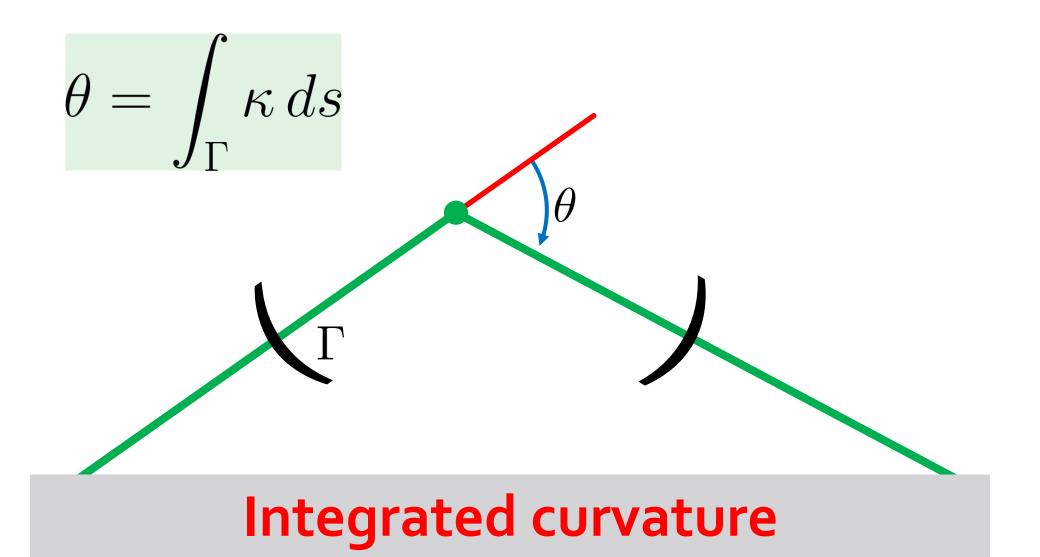
Discrete Gauss Map



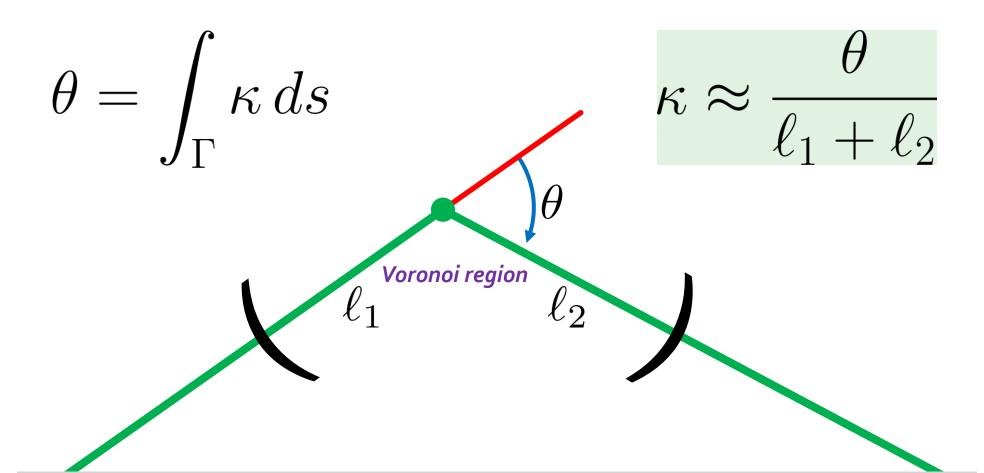
Key Observation



What's Going On?

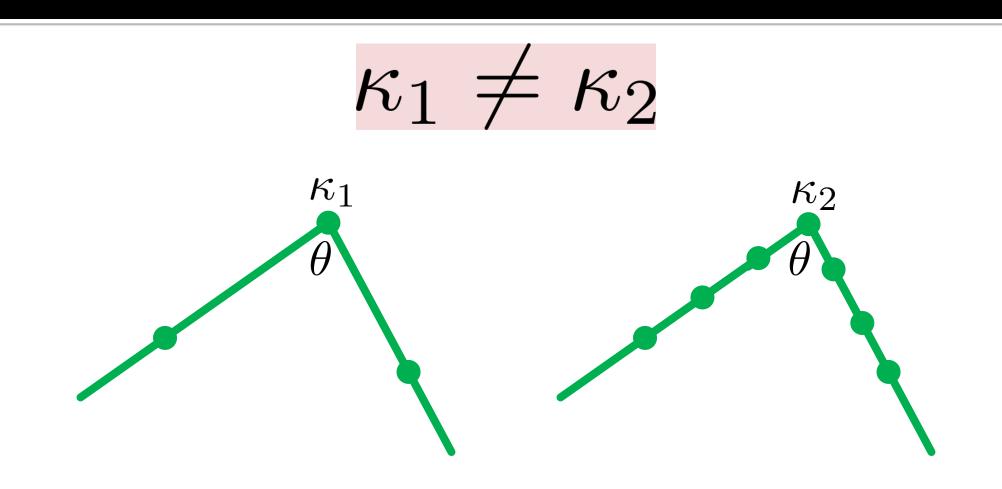


What's Going On?



Total change in curvature

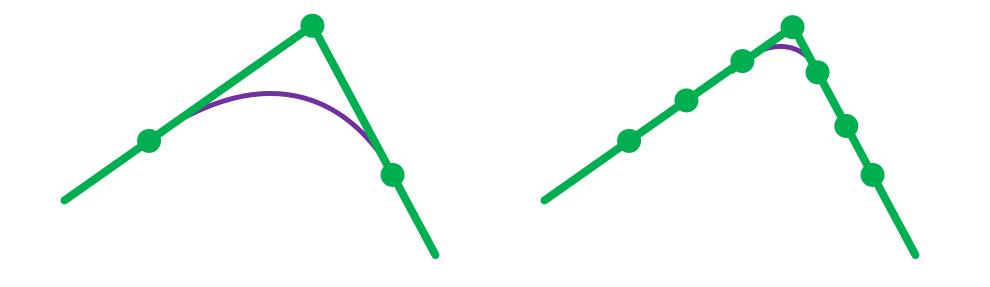
Interesting Distinction



Same integrated curvature

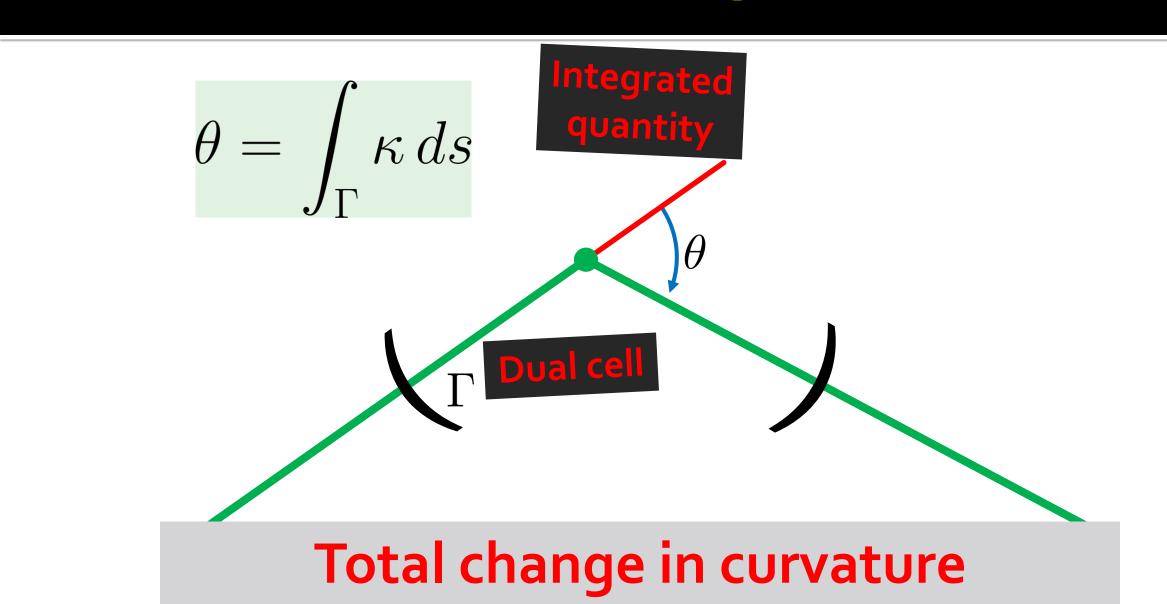
Interesting Distinction

$$\kappa_1 \neq \kappa_2$$

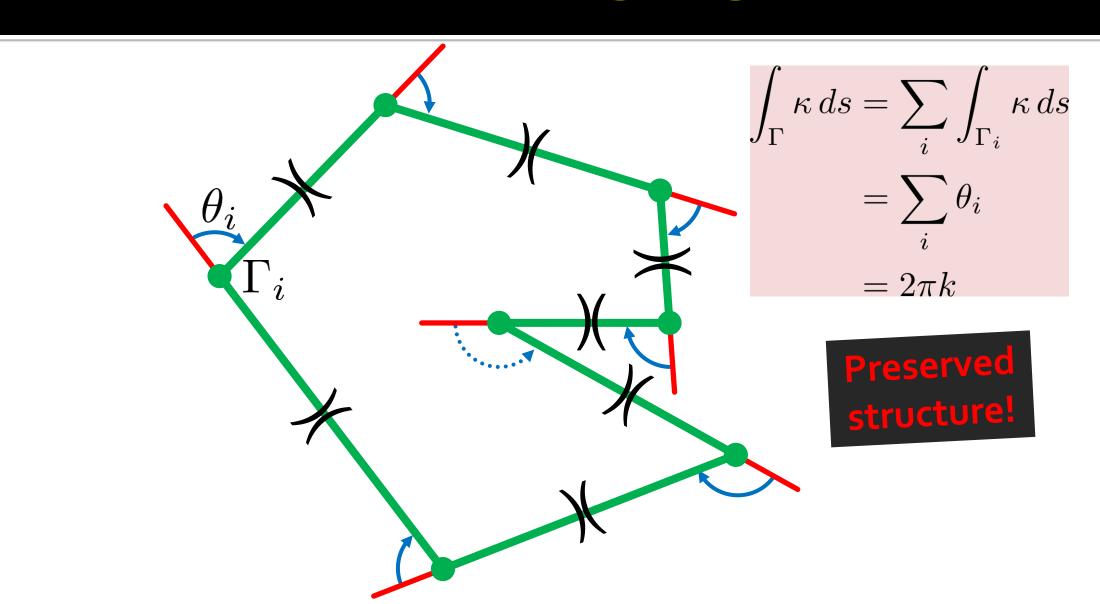


Same integrated curvature

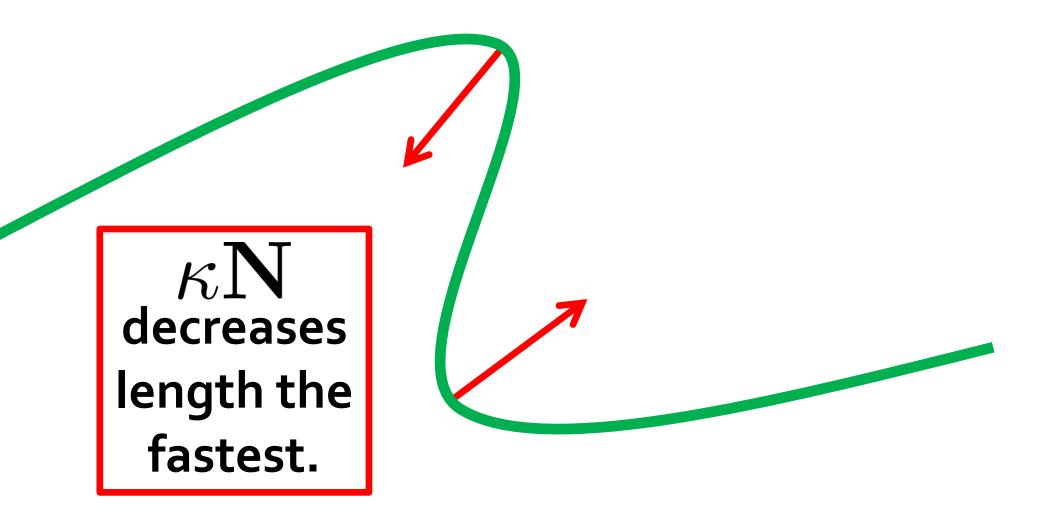
What's Going On?



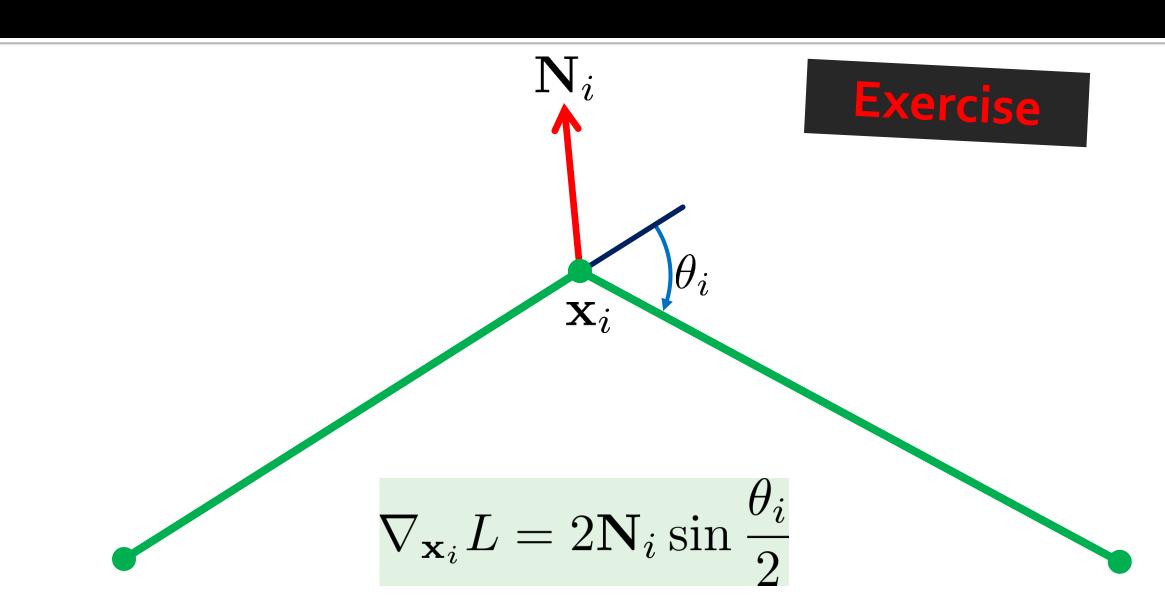
Discrete Turning Angle Theorem



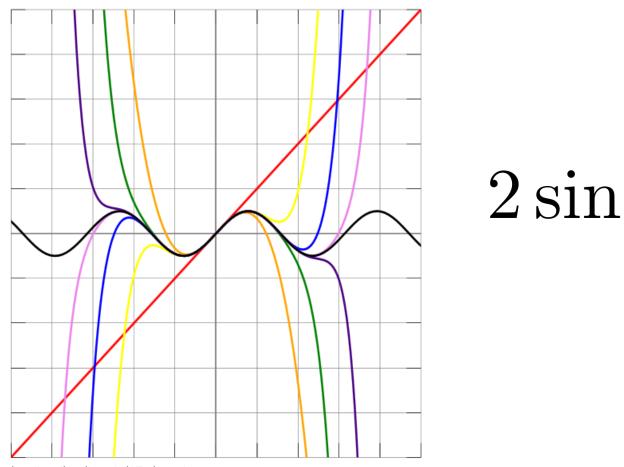
First Variation Formula



Discrete Case



For Small θ



$$2\sin\frac{\theta}{2} \approx 2 \cdot \frac{\theta}{2}$$
$$= \theta$$

 $http:/\!/en.wikipedia.org/wiki/\!Taylor_series$

Same behavior in the limit

No Free Lunch

Choose one:

- Discrete curvature with turning angle theorem
- Discrete curvature from gradient of arc length



Remaining Question

Does discrete curvature converge in limit?

Ges!
Under some assumptions!

Remaining Question

Does discrete curvature converge in limit?

Questions:

- Type of convergence?
- Sampling?
- Class of curves?

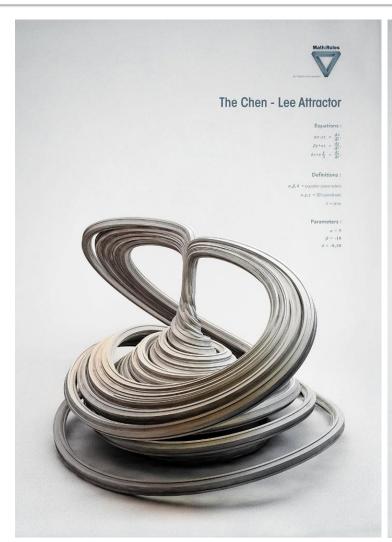


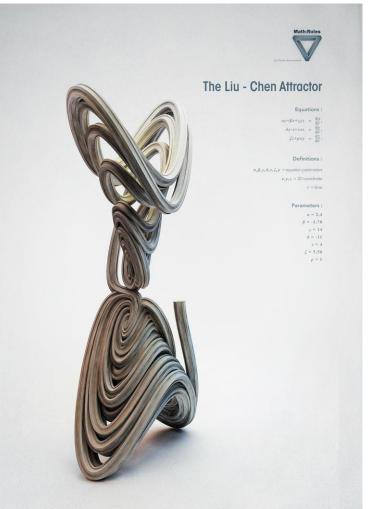
Discrete Differential Geometry

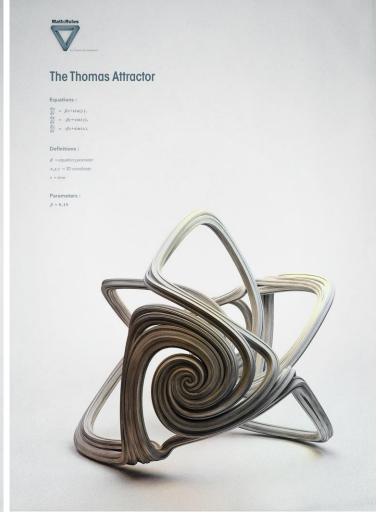
Different discretebehavior

Same convergence

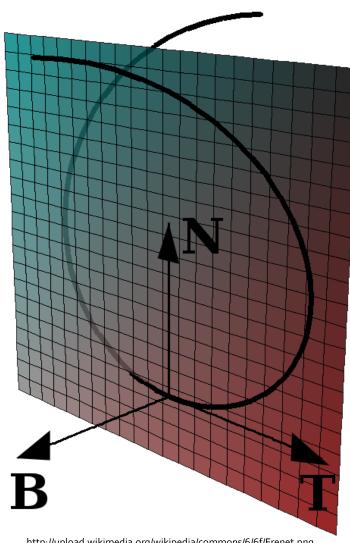
Curves in 3D?







Frenet Frame



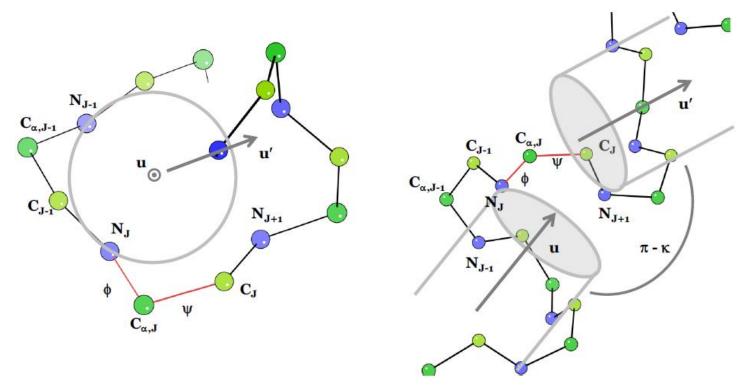
$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

http://upload.wikimedia.org/wikipedia/commons/6/6f/Frenet.png

Application



NMR scanner



Kinked alpha helix

Structure Determination of Membrane Proteins Using Discrete Frenet Frame and Solid State NMR Restraints

Achuthan and Quine

Discrete Mathematics and its Applications, ed. M. Sethumadhavan (2006)

Potential Discretization

$$egin{aligned} \mathbf{T}_j &= rac{\mathbf{p}_{j+1} - \mathbf{p}_j}{\|\mathbf{p}_{j+1} - \mathbf{p}_j\|_2} \ \mathbf{B}_j &= \mathbf{T}_{j-1} imes \mathbf{T}_j \ \mathbf{N}_j &= \mathbf{B}_j imes \mathbf{T}_j \ \end{aligned}$$
 Discrete Frenet frame

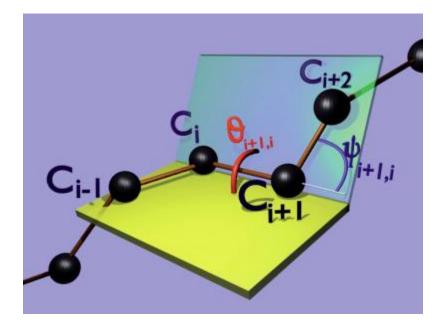
$$\mathbf{T}_k = R(\mathbf{B}_k, \theta_k) \mathbf{T}_{k-1}$$
 $\mathbf{B}_{k+1} = R(\mathbf{T}_k, \phi_k) \mathbf{B}_k$ "Bond and torsion angles" (derivatives converge to κ and τ , resp.)

Discrete frame introduced in:

The resultant electric moment of complex molecules Eyring, Physical Review, 39(4):746—748, 1932.

Transfer Matrix

$$egin{pmatrix} \mathbf{T}_{i+1} \\ \mathbf{N}_{i+1} \\ \mathbf{B}_{i+1} \end{pmatrix} = R_{i+1,i} egin{pmatrix} \mathbf{T}_i \\ \mathbf{N}_i \\ \mathbf{B}_i \end{pmatrix}$$

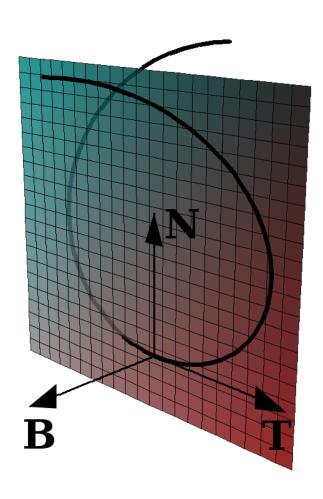


<u>Discrete</u> construction that works for fractal curves and converges in continuum limit.

Discrete Frenet Frame, Inflection Point Solitons, and Curve Visualization with Applications to Folded Proteins

Hu, Lundgren, and Niemi *Physical Review E* 83 (2011)

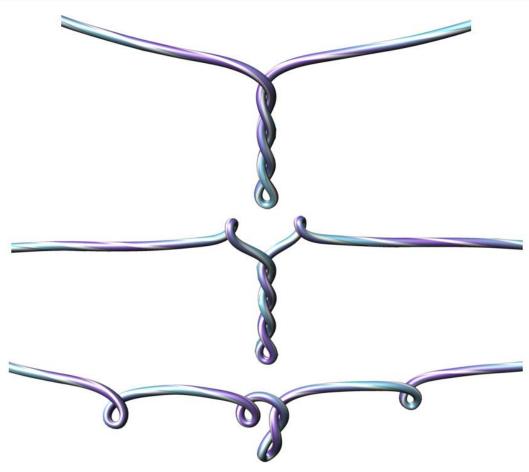
Frenet Frame: Issue



$$\kappa = 0$$
?

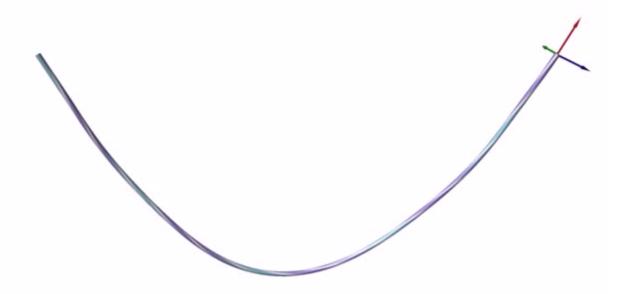
$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

Segments Not Always Enough

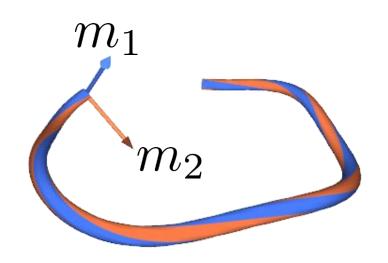


Discrete Elastic Rods
Bergou, Wardetzky, Robinson, Audoly, and Grinspun
SIGGRAPH 2008

Simulation Goal



Adapted Framed Curve



$$\Gamma = \{\gamma(s); \mathbf{T}, \mathbf{m}_1, \mathbf{m}_2\}$$

Material frame

http://www.cs.columbia.edu/cg/rods/

Normal part encodes twist

Bending Energy

$$E_{\rm bend}(\Gamma) := \frac{1}{2} \int_{\Gamma} \alpha \kappa^2 \, ds$$

Penalize turning the steering wheel

$$\kappa \mathbf{N} = \mathbf{T}'$$

$$= (\mathbf{T}' \cdot \mathbf{T})\mathbf{T} + (\mathbf{T}' \cdot \mathbf{m}_1)\mathbf{m}_1 + (\mathbf{T}' \cdot \mathbf{m}_2)\mathbf{m}_2$$

$$= (\mathbf{T}' \cdot \mathbf{m}_1)\mathbf{m}_1 + (\mathbf{T}' \cdot \mathbf{m}_2)\mathbf{m}_2$$

$$:= \omega_1 \mathbf{m}_1 + \omega_2 \mathbf{m}_2$$

Bending Energy

$$E_{\text{bend}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \alpha(\omega_1^2 + \omega_2^2) \, ds$$

Penalize turning the steering wheel

$$\kappa \mathbf{N} = \mathbf{T}'$$

$$= (\mathbf{T}' \cdot \mathbf{T})\mathbf{T} + (\mathbf{T}' \cdot \mathbf{m}_1)\mathbf{m}_1 + (\mathbf{T}' \cdot \mathbf{m}_2)\mathbf{m}_2$$

$$= (\mathbf{T}' \cdot \mathbf{m}_1)\mathbf{m}_1 + (\mathbf{T}' \cdot \mathbf{m}_2)\mathbf{m}_2$$

$$:= \omega_1 \mathbf{m}_1 + \omega_2 \mathbf{m}_2$$

Twisting Energy

$$E_{\text{twist}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \beta m^2 \, ds$$

Penalize non-tangent change in material frame

$$egin{aligned} m := \mathbf{m}_1' \cdot \mathbf{m}_2 \ &= rac{d}{dt} (\mathbf{m}_1 \cdot \mathbf{m}_2) - \mathbf{m}_1 \cdot \mathbf{m}_2' \ &= -\mathbf{m}_1 \cdot \mathbf{m}_2' \longleftarrow ext{Swapping } m_1 ext{ and } m_2 \ ext{does not affect } E_{twist}! \end{aligned}$$

Bishop Frame: The Hipster Framed Curve

THERE IS MORE THAN ONE WAY TO FRAME A CURVE

RICHARD L. BISHOP

The Frenet frame of a 3-times continuously differentiable (that is, C^3) nondegenerate curve in euclidean space has long been the standard vehicle for analysing properties of the curve invariant under euclidean motions. For arbitrary moving frames, that is, orthonormal basis fields, we can express the derivatives of the frame with respect to the curve parameter in terms of the frame itself, and due to orthonormality the coefficient matrix is always skew-symmetric. Thus it generally has three nonzero entries. The Frenet frame gains part of its special significance from the fact that one of the three derivatives is always zero. Another feature of the Frenet frame is that it is adapted to the curve: the members are either tangent to or perpendicular to the curve. It is the purpose of this paper to show that there are other frames which have these same advantages and to compare them with the Frenet frame.

Relatively parallel fields. We say that a normal vector field M along a cur atively parallel if its derivative is tangential. Such a field turns only whate int is necessary for it to remain normal, so it is as close to being parallel ble without losing normality. Since its derivative is perpendicular to it, a parallel normal fie (couldn't decide on a meme) h fields occur classically in

DON'T CALL ME

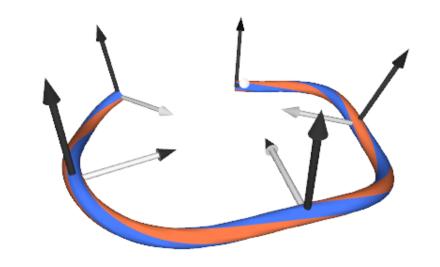
ARIEL

Bishop Frame

$$\mathbf{T}' = \mathbf{\Omega} imes \mathbf{T}$$

$$\mathbf{u}' = \mathbf{\Omega} imes \mathbf{u}$$

$$\mathbf{v}' = \mathbf{\Omega} imes \mathbf{v}$$



$$\Omega := \kappa \mathbf{B}$$
 ("curvature binormal")

Darboux vector

http://www.cs.columbia.edu/cg/rods/

Most relaxed frame

Bishop Frame

$$\mathbf{T}' = \mathbf{\Omega} imes \mathbf{T}$$

$$\mathbf{u}' = \mathbf{\Omega} imes \mathbf{u}$$

$$\mathbf{v}' = \mathbf{\Omega} imes \mathbf{v}$$

$$\mathbf{u}' \cdot \mathbf{v} \equiv 0$$

No twist ("parallel transport")

 $\Omega := \kappa \mathbf{B}$ ("curvature binormal")

Darboux vector

http://www.cs.columbia.edu/cg/rods/

Most relaxed frame

Curve-Angle Representation

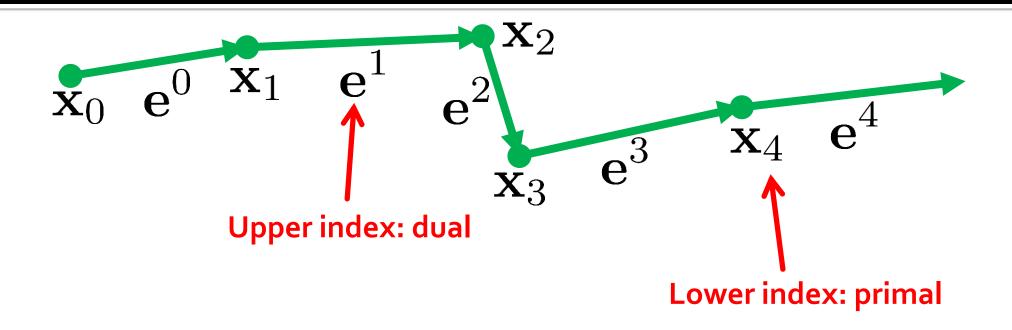
$$\mathbf{m}_1 = \mathbf{u}\cos\theta + \mathbf{v}\sin\theta$$

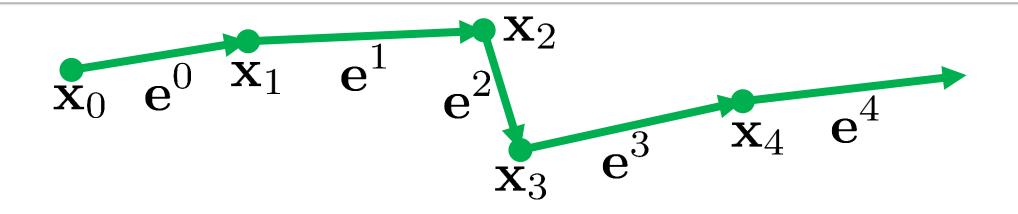
 $\mathbf{m}_2 = -\mathbf{u}\sin\theta + \mathbf{v}\cos\theta$

$$E_{\text{twist}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \beta(\theta')^2 ds$$

Degrees of freedom for elastic energy:

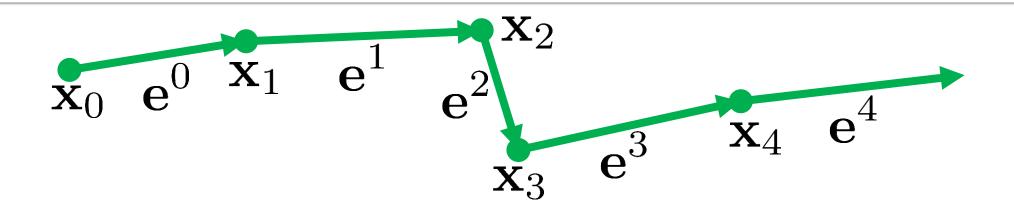
- Shape of curve
- Twist angle θ





$$\mathbf{T}^i := rac{\mathbf{e}^i}{\|\mathbf{e}^i\|_2}$$

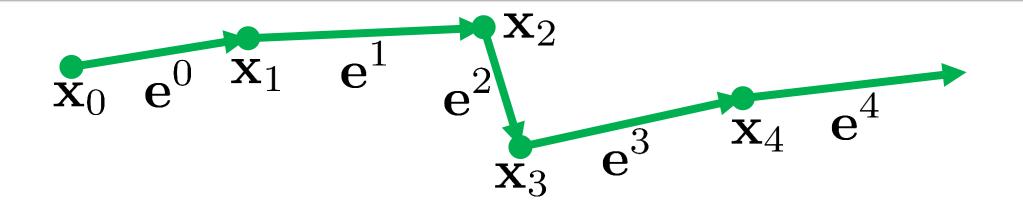
Tangent unambiguous on edge



$$\kappa_i := 2 an rac{\phi_i}{2}$$

Yet another curvature!

Integrated curvature



$$\kappa_i := 2 \tan \frac{\phi_i}{2}$$

Yet another curvature!

$$(\kappa \mathbf{B})_i := rac{2\mathbf{e}^{i-1} imes \mathbf{e}^i}{\|\mathbf{e}^{i-1}\|_2 \|\mathbf{e}^i\|_2 + \mathbf{e}^{i-1} \cdot \mathbf{e}^i}$$

Orthogonal to osculating plane, norm κ_i

Darboux vector

Bending Energy

$$E_{\text{bend}}(\Gamma) := \frac{\alpha}{2} \sum_{i} \left(\frac{(\kappa \mathbf{B})_{i}}{\ell_{i}/2} \right)^{2} \frac{\ell_{i}}{2}$$
$$= \alpha \sum_{i} \frac{\|(\kappa \mathbf{B})_{i}\|_{2}^{2}}{\ell_{i}}$$

Convert to pointwise and integrate

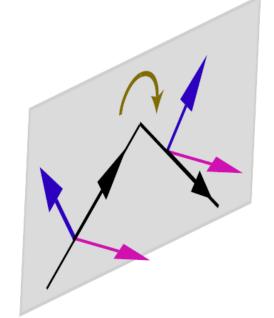
Discrete Parallel Transport

$$P_i(\mathbf{T}^{i-1}) = \mathbf{T}^i$$

$$P_i(\mathbf{T}^{i-1} \times \mathbf{T}^i) = \mathbf{T}^{i-1} \times \mathbf{T}^i$$

- Map tangent to tangent
- Preserve binormal
- Orthogonal

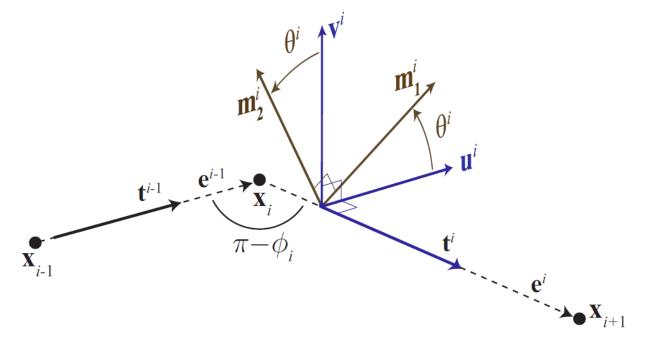
$$\mathbf{u}^i = P_i(\mathbf{u}^{i-1})$$
$$\mathbf{v}^i = \mathbf{T}^i \times \mathbf{u}^i$$



Discrete Material Frame

$$\mathbf{m}_{1}^{i} = \mathbf{u}^{i} \cos \theta^{i} + \mathbf{v}^{i} \sin \theta^{i}$$

$$\mathbf{m}_{2}^{i} = -\mathbf{u}^{i} \sin \theta^{i} + \mathbf{v}^{i} \cos \theta^{i}$$



Discrete Twisting Energy

$$E_{\text{twist}}(\Gamma) := \beta \sum_{i} \frac{(\theta^{i} - \theta^{i-1})^{2}}{\ell_{i}}$$

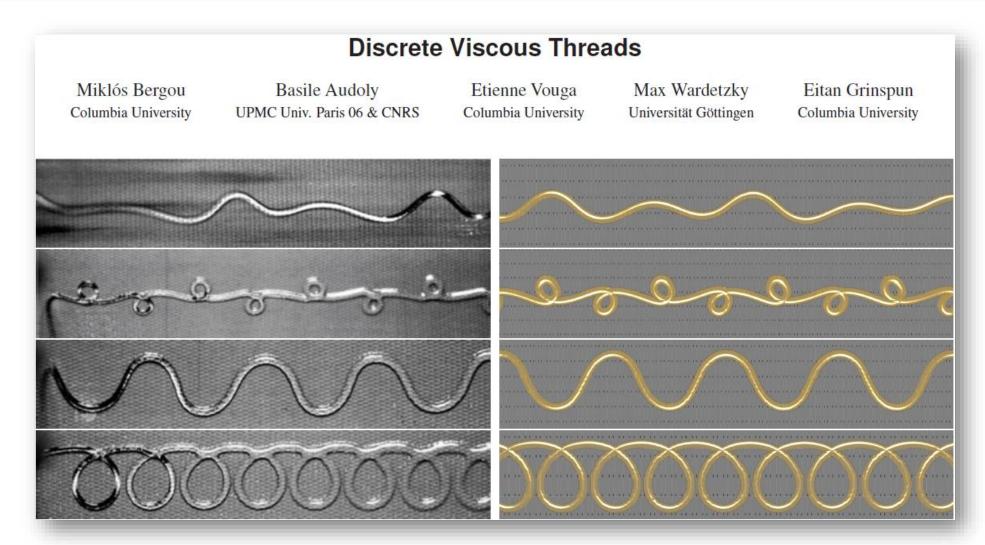
Note θ_0 can be arbitrary

Simulation

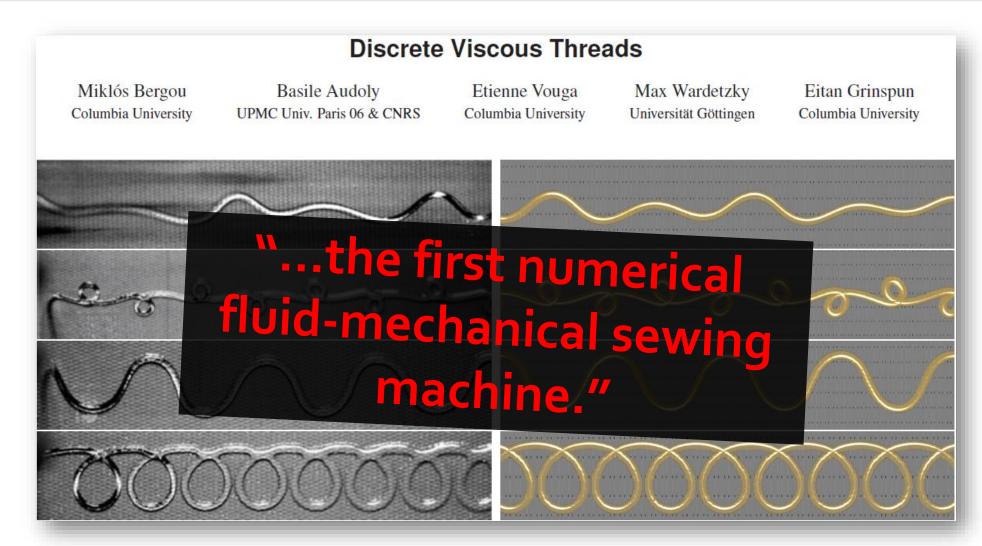
```
\omit{physics}

Worth reading!
```

Extension and Speedup



Extension and Speedup



Morals

One curve, three curvatures.

$$\theta$$

$$2\sin\frac{\theta}{2}$$

$$2 an rac{ heta}{2}$$

Morals

Easy theoretical object, hard to use.

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

Morals

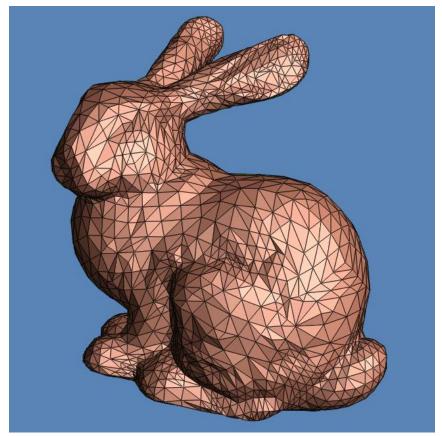
Proper frames and DOFs go a long way.

$$\mathbf{m}_{1}^{i} = \mathbf{u}^{i} \cos \theta^{i} + \mathbf{v}^{i} \sin \theta^{i}$$

$$\mathbf{m}_{2}^{i} = -\mathbf{u}^{i} \sin \theta^{i} + \mathbf{v}^{i} \cos \theta^{i}$$

Next





http://graphics.stanford.edu/data/3Dscanrep/stanford-bunny-cebal-ssh.jpg http://www.stat.washington.edu/wxs/images/BUNMID.gif

Surfaces

Discrete Curves

Justin Solomon

6.8410: Shape Analysis
Spring 2023

