

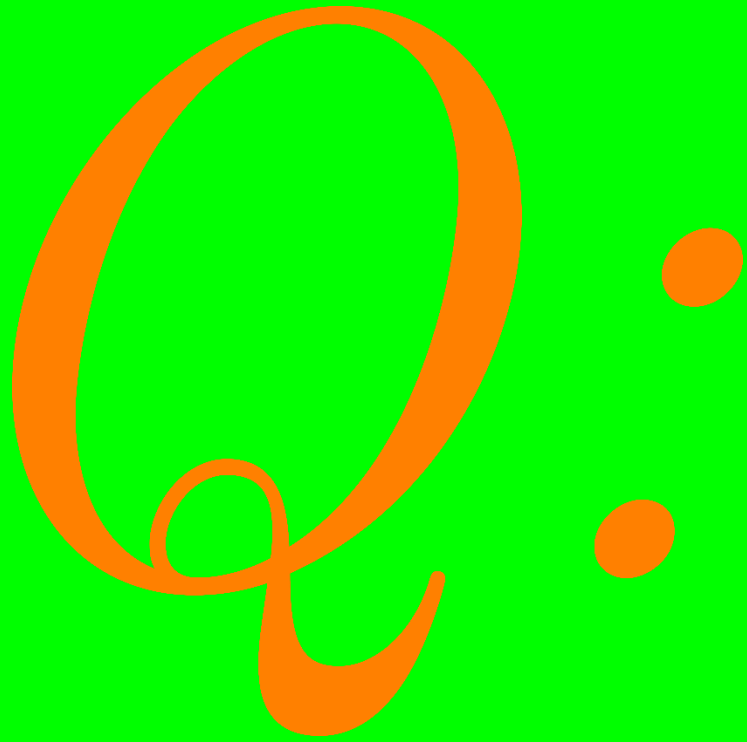
# Continuous Curves

Justin Solomon

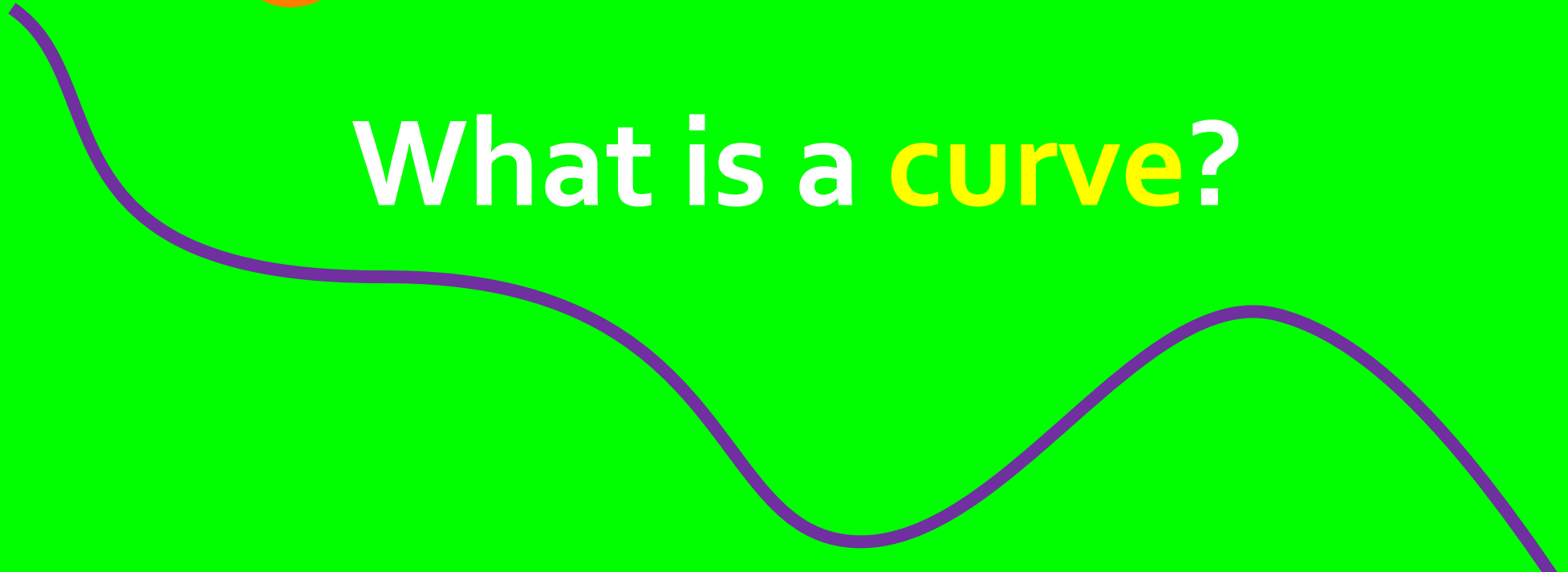
6.838: Shape Analysis

Spring 2021

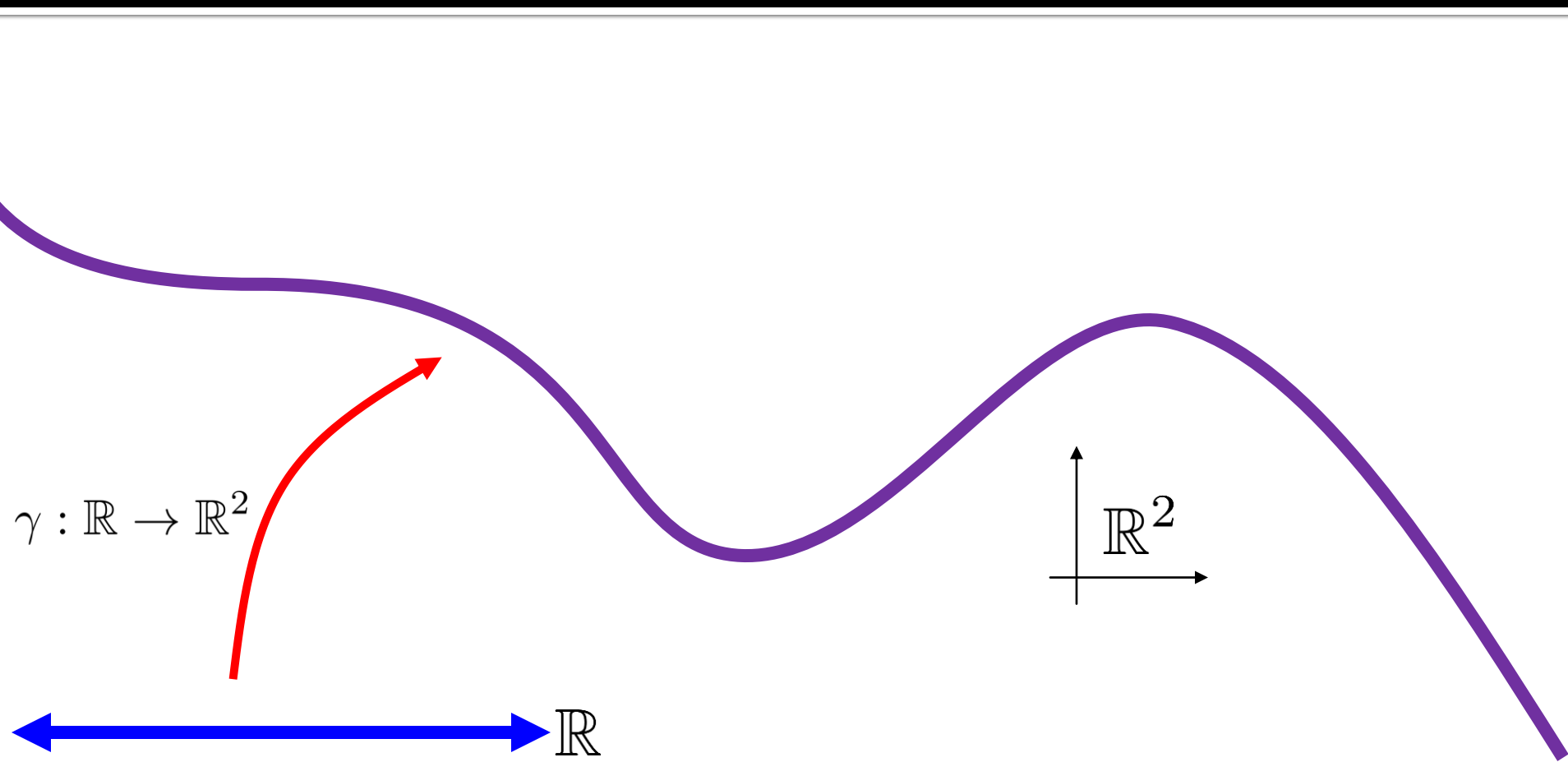




What is a **curve**?



# Defining "Curve"



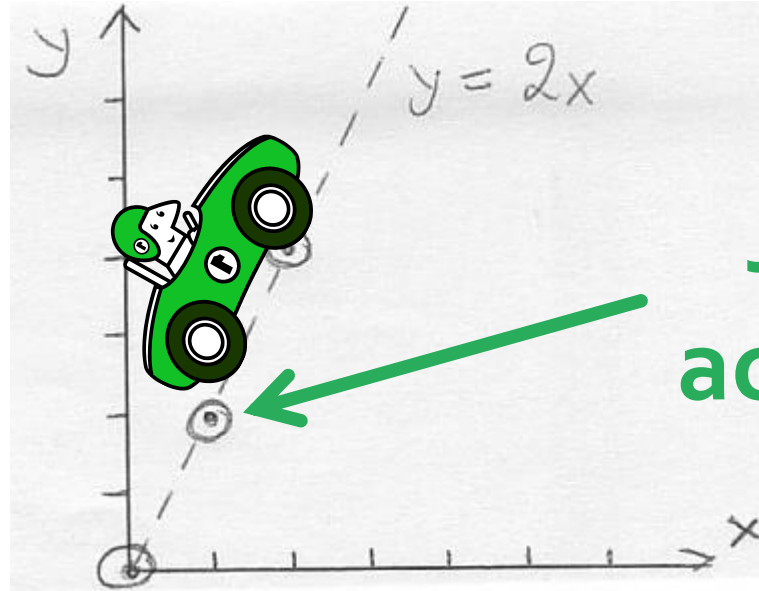
**A function?**

# Subtlety

$$\gamma(t) \equiv (0, 0)$$

**Not a curve**

# Different from Calculus

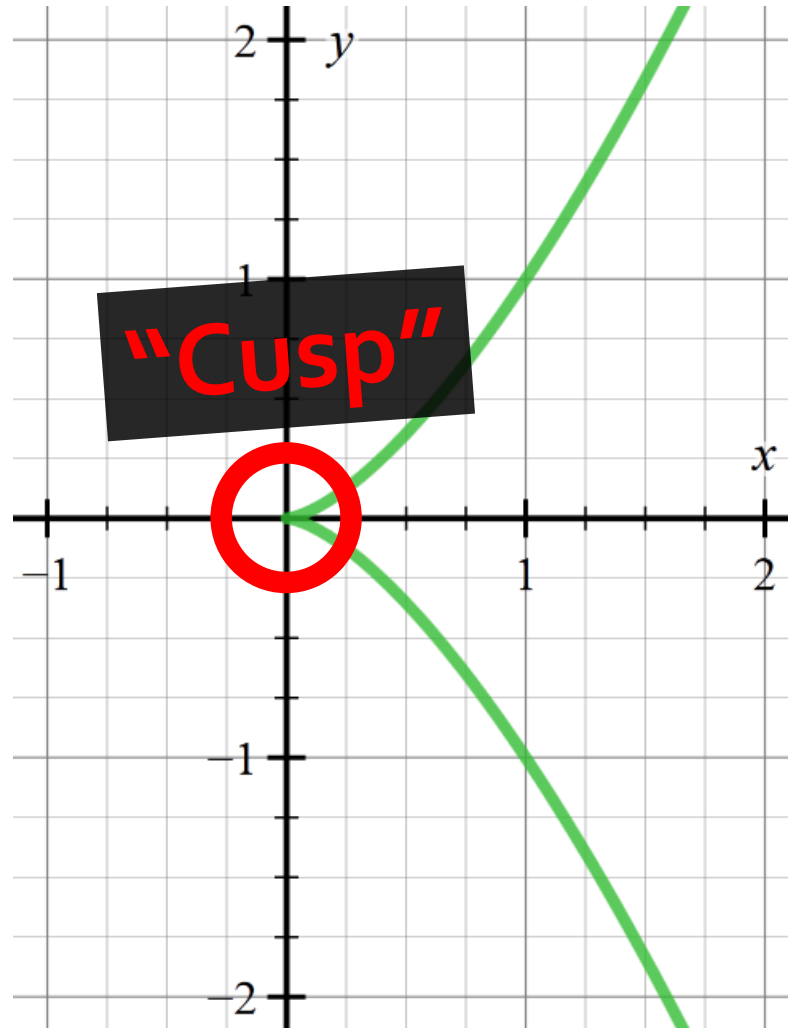


Jams on  
accelerator

$$\gamma_1(t) = (t, 2t)$$

$$\gamma_2(t) = \begin{cases} (t, 2t) & t \leq 1 \\ (2(t - \frac{1}{2}), 4(t - \frac{1}{2})) & t > 1 \end{cases}$$

# Graphs of Smooth Functions



$$\gamma(t) = (t^2, t^3)$$

# Geometry of a Curve

A curve is a  
**set of points**  
with certain properties.

It is not a function.

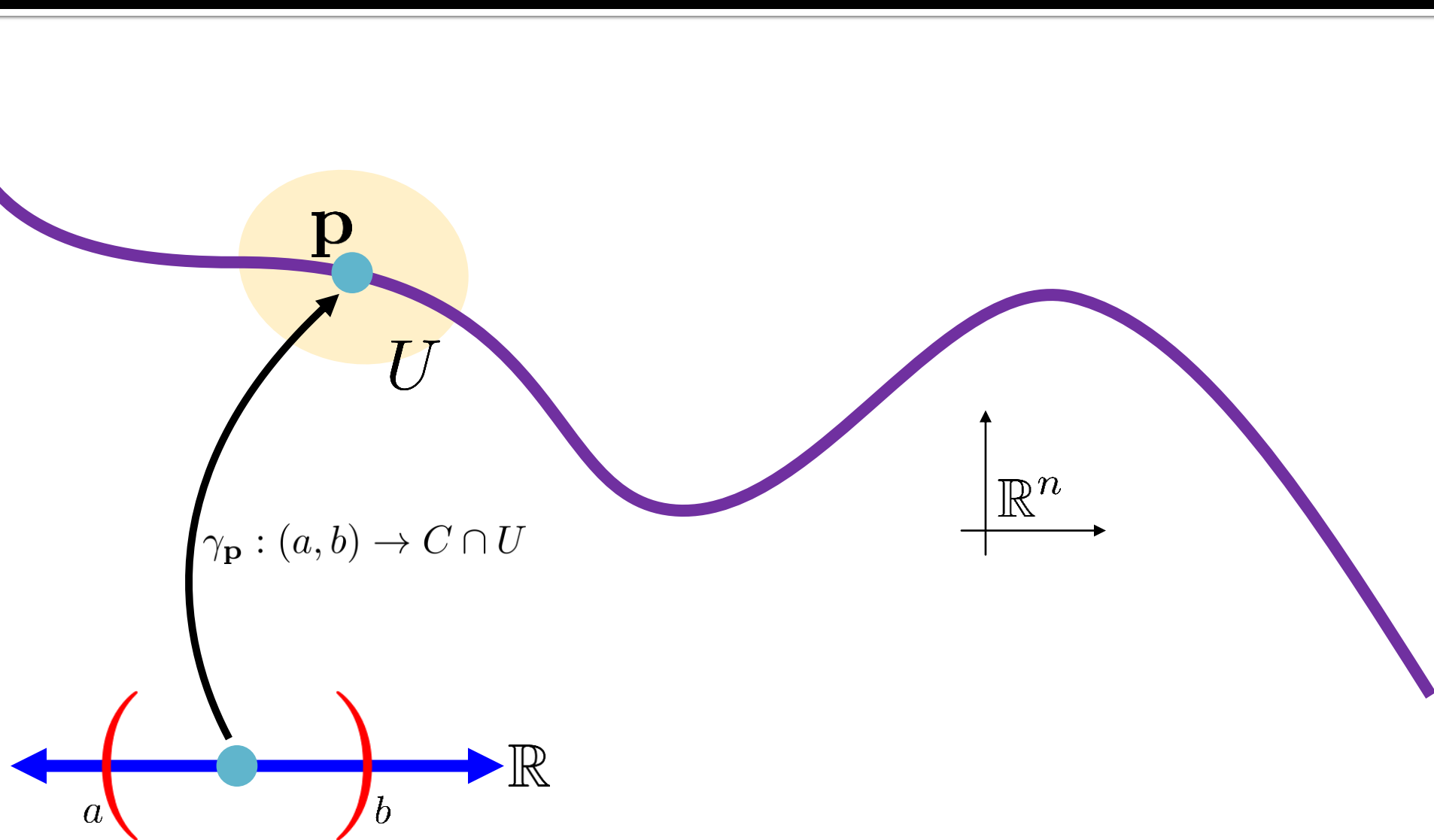
# Geometric Definition



Set of points that locally looks like a line.



# Differential Geometry Definition

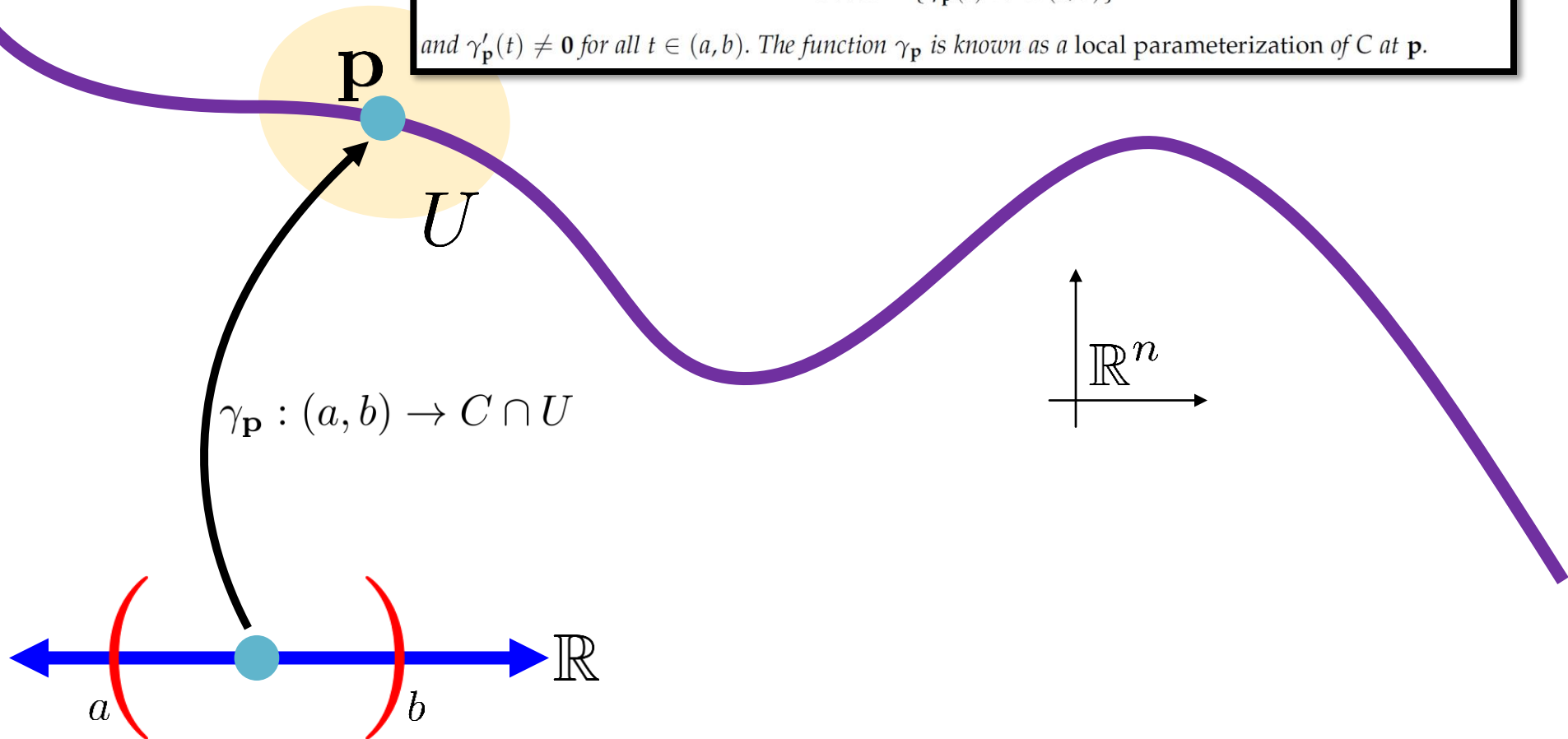


# Formal Statement

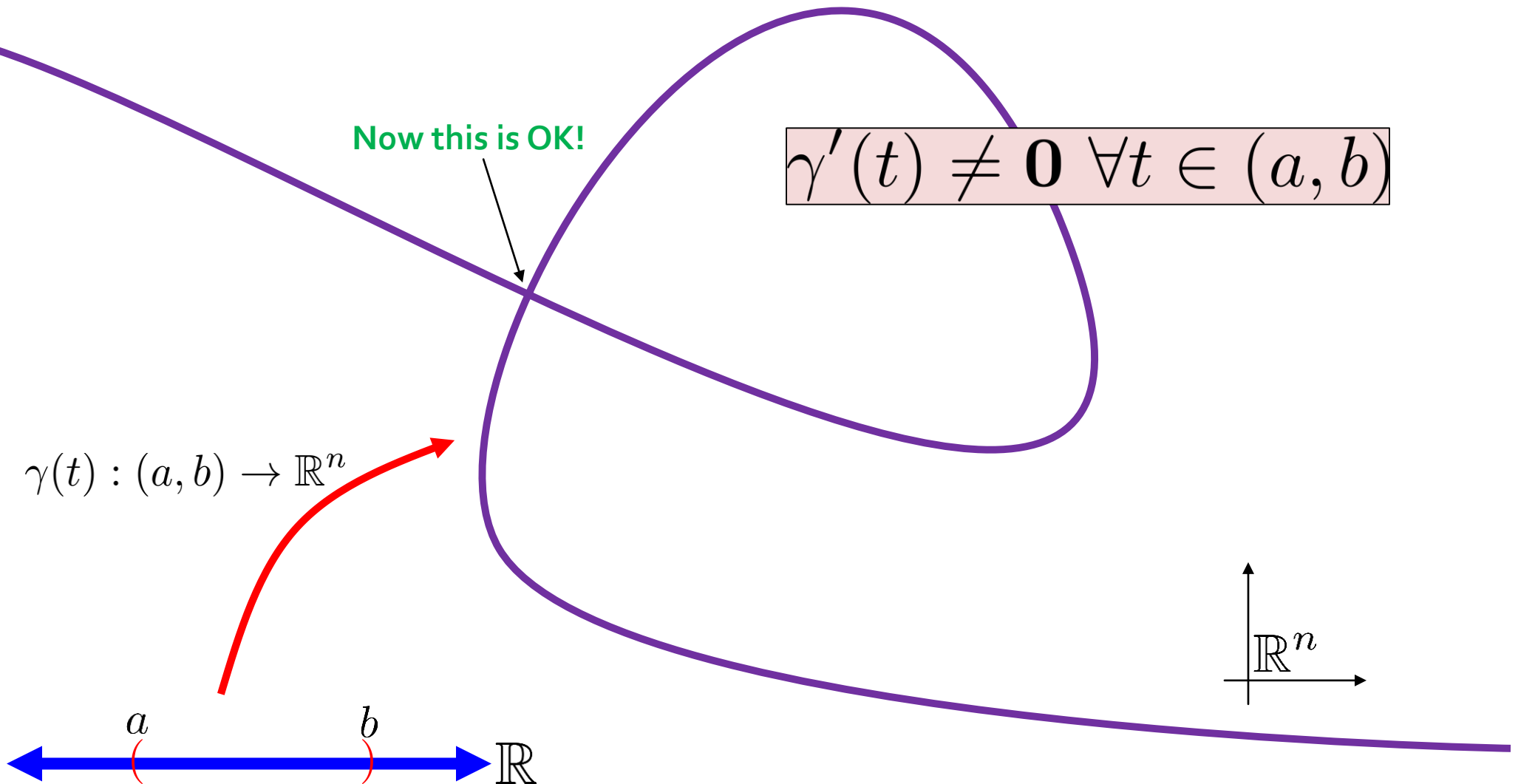
**Definition 3.1** (Differentiable curve in  $\mathbb{R}^n$ ). A differentiable curve in  $\mathbb{R}^n$  is a set of points  $C \subset \mathbb{R}^n$  with the property that for every  $\mathbf{p} \in C$  there exists an open neighborhood  $U \subseteq \mathbb{R}^n$  containing  $\mathbf{p}$  and a smooth function  $\gamma_{\mathbf{p}} : (a, b) \rightarrow C \cap U$ , so that

$$C \cap U = \{\gamma_{\mathbf{p}}(t) : t \in (a, b)\}$$

and  $\gamma'_{\mathbf{p}}(t) \neq \mathbf{0}$  for all  $t \in (a, b)$ . The function  $\gamma_{\mathbf{p}}$  is known as a local parameterization of  $C$  at  $\mathbf{p}$ .



# Parameterized Curve



# Some Vocabulary

- **Trace** of parameterized curve

$$\{\gamma(t) : t \in (a, b)\} \subseteq \mathbb{R}^n$$

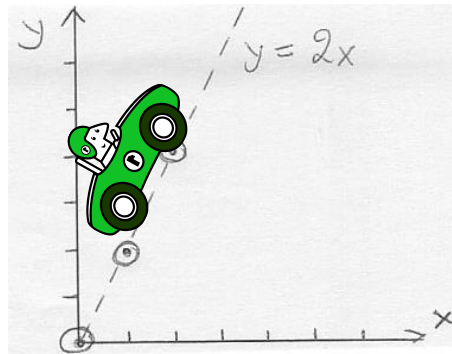
- **Component** functions

$$\gamma(t) = (x(t), y(t), z(t))$$

# Change of Parameter

$$t \mapsto \gamma \circ \phi(t)$$

Geometric measurements should be  
**invariant**  
to changes of parameter.



# Dependence of Velocity

$$\tilde{\gamma}(t) := \gamma(\phi(t))$$

Effect on velocity and acceleration?

$$\tilde{\gamma}(t) := \gamma(\phi(t))$$

# Arc Length

$$\int_a^b \|\gamma'(t)\|_2 dt$$

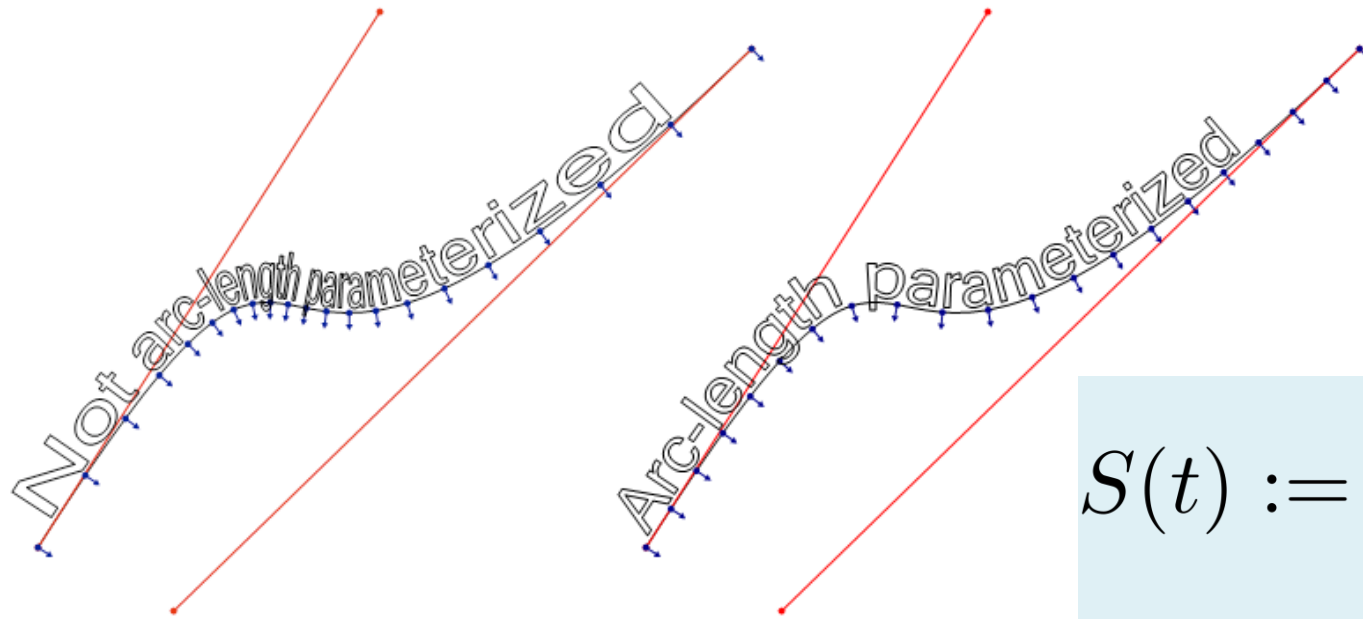
Independent of parameter!



$$\int_a^b \|\gamma'(t)\|_2 \, dt$$

# Parameterization by Arc Length

<http://www.planetclegg.com/projects/WarpingTextToSplines.html>



$$S(t) := \int_{t_0}^t \|\gamma'(t)\|_2 dt$$

$$t = \phi \circ S(t)$$

$$\tilde{\gamma}(s) := \gamma \circ \phi(s)$$

← Inverse  
functions

**Constant-speed parameterization**

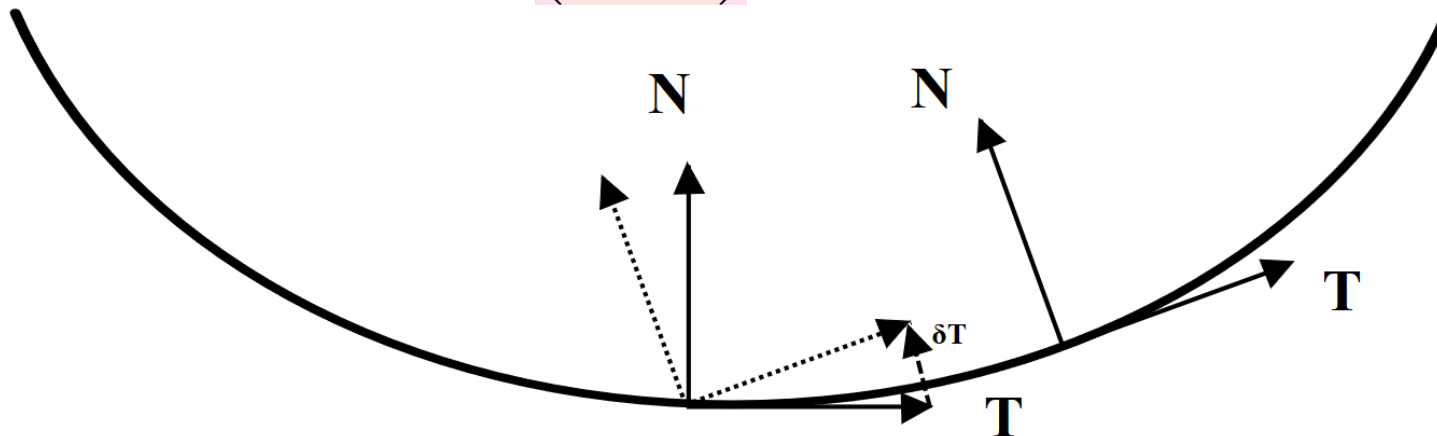
# Moving Frame in 2D

$$\mathbf{T}(s) := \gamma'(s)$$

$$\Rightarrow \|\mathbf{T}(s)\|_2 \equiv 1$$

$$\mathbf{N}(s) := J\mathbf{T}(s) = T'(s)$$

$$\begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix}$$

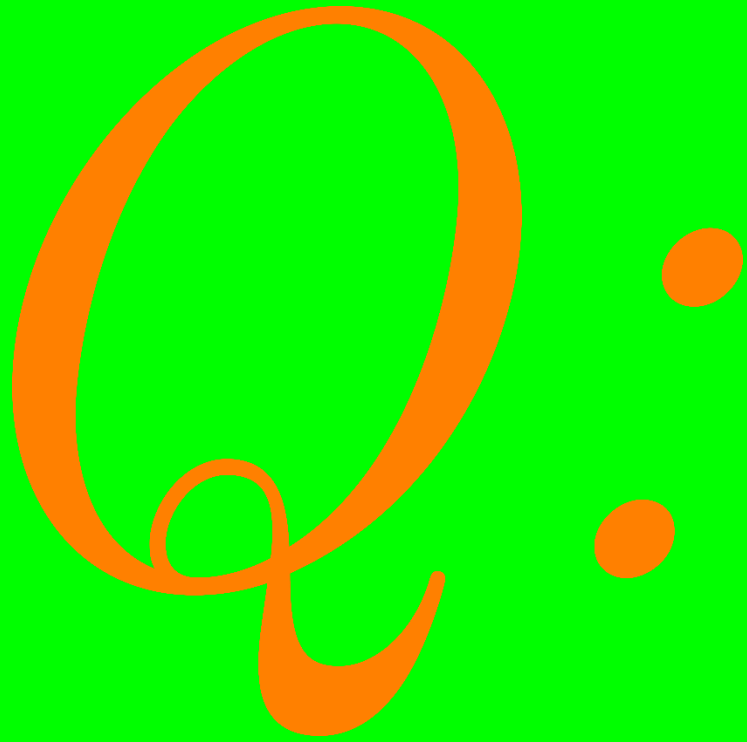


# Philosophical Point

Differential geometry “should” be  
**coordinate-invariant.**

Referring to  $x$  and  $y$  is a hack!

*(but sometimes convenient...)*



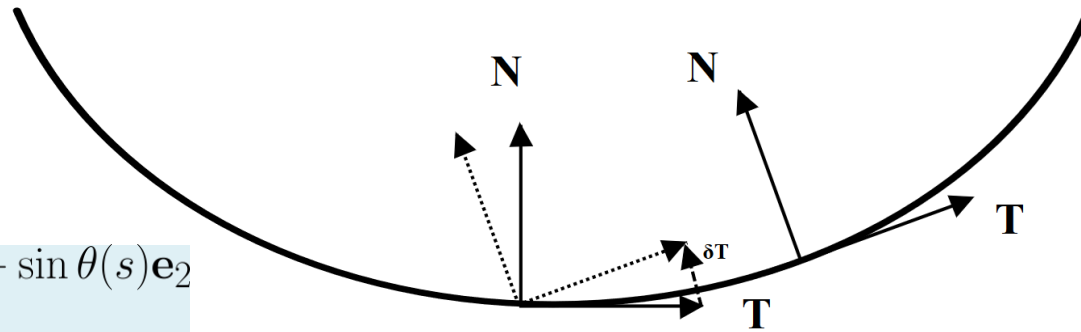
How do you  
describe a curve  
without coordinates?

# Turtles All The Way Down

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix} := \begin{pmatrix} 0 & \kappa(s) \\ -\kappa(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix}$$

Signed curvature  $\kappa$  is rate of change of turning angle  $\theta$ .

$$\begin{aligned} \mathbf{T}(s) &= \cos \theta(s) \mathbf{e}_1 + \sin \theta(s) \mathbf{e}_2 \\ \kappa(s) &:= \theta'(s) \end{aligned}$$

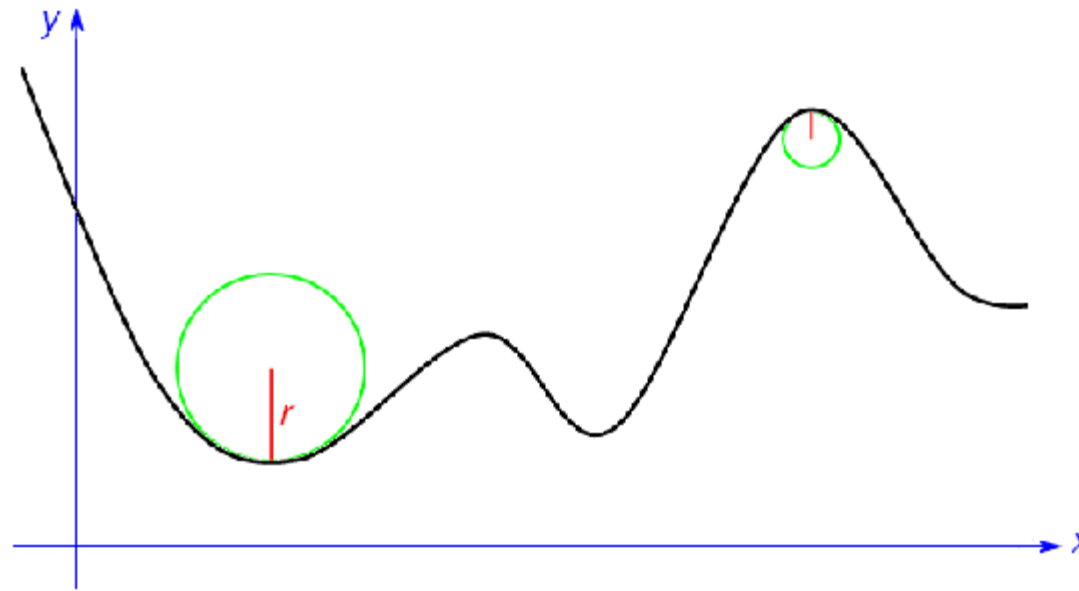


[https://en.wikipedia.org/wiki/Frenet%E2%80%93Serret\\_formulas](https://en.wikipedia.org/wiki/Frenet%E2%80%93Serret_formulas)

Use coordinates *from* the curve to  
express its shape!

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix} := \begin{pmatrix} 0 & \kappa(s) \\ -\kappa(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix}$$

# Radius of Curvature



$$r(s) := \frac{1}{\kappa(s)}$$



Fundamental theorem of the  
local theory of plane curves:

$\kappa(s)$  distinguishes a planar  
curve up to rigid motion.

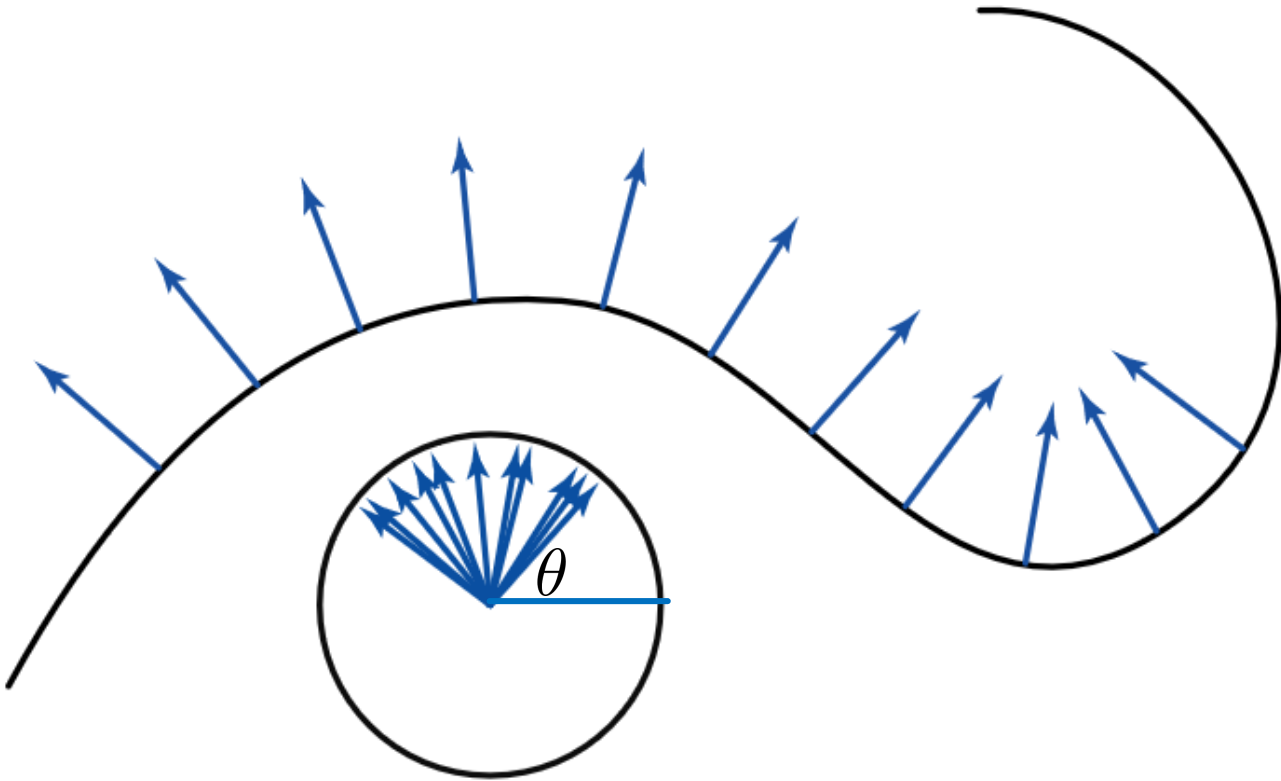
# Fundamental theorem of the local theory of plane curves:

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curve up to rigid motion.



*Statement shorter than the name!*

# Idea of Proof



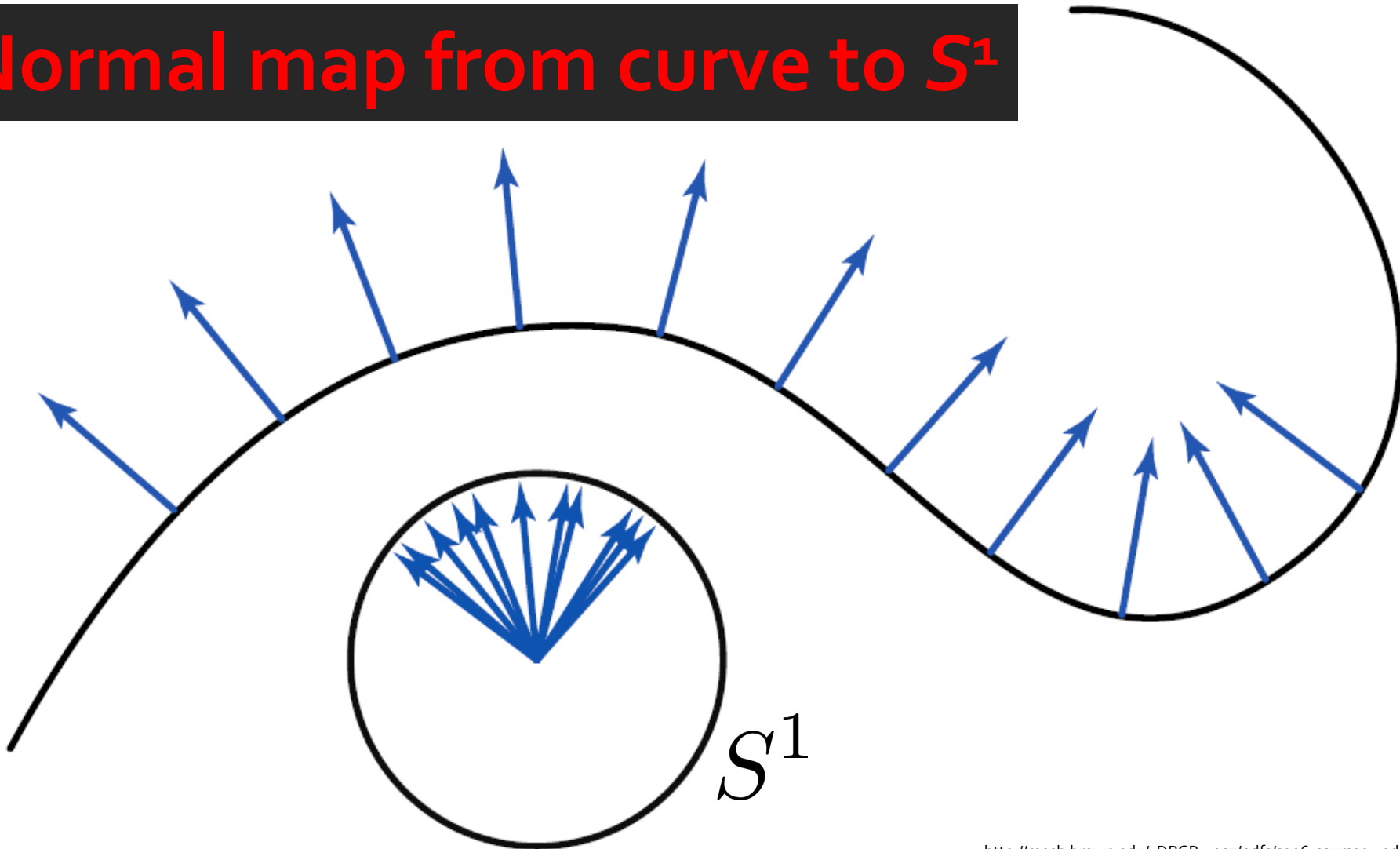
$$\begin{aligned}\mathbf{T}(s) &:= (\cos \theta(s), \sin \theta(s)) \\ \implies \kappa(s) &:= \theta'(s)\end{aligned}$$

Image from DDG course notes by E. Grinspun

**Provides intuition for curvature**

# Gauss Map

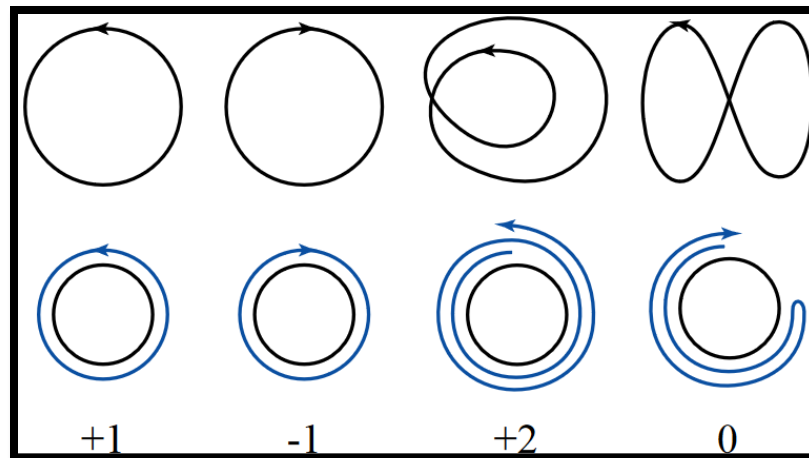
Normal map from curve to  $S^1$



# Winding Number

$$W[\gamma] := \frac{1}{2\pi} \int_a^b \kappa(s) ds \in \mathbb{Z}$$

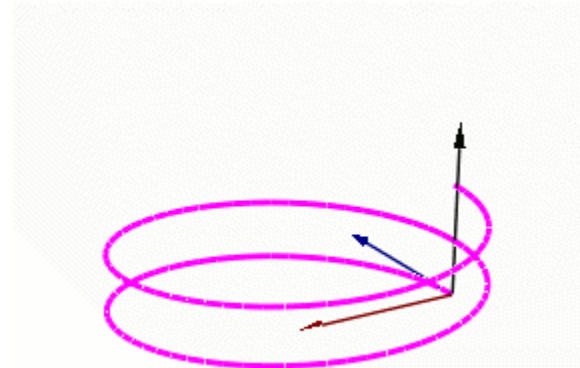
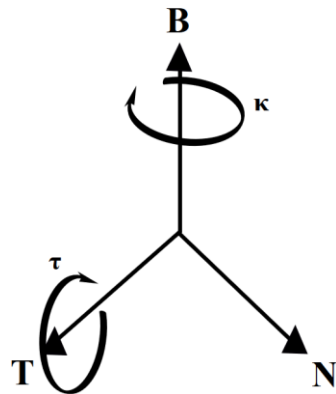
$W[\gamma]$  is an integer, and smoothly deforming  $\gamma$  does not affect  $W[\gamma]$ .



# Frenet Frame: Curves in $\mathbb{R}^3$

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

- **Binormal:**  $\mathbf{T} \times \mathbf{N}$
- **Curvature:** In-plane motion
- **Torsion:** Out-of-plane motion



$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

**Fundamental theorem of the  
local theory of space curves:**

**Curvature and torsion  
distinguish a 3D curve up to  
rigid motion.**



# Aside: Generalized Frenet Frame

$$\gamma(s) : \mathbb{R} \rightarrow \mathbb{R}^n$$

$$\frac{d}{ds} \begin{pmatrix} \mathbf{e}_1(s) \\ \mathbf{e}_2(s) \\ \vdots \\ \mathbf{e}_n(s) \end{pmatrix} = \begin{pmatrix} 0 & \chi_1(s) & & \\ -\chi_1(s) & \ddots & \ddots & \\ & \ddots & 0 & \chi_{n-1}(s) \\ & & -\chi_{n-1}(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{e}_1(s) \\ \mathbf{e}_2(s) \\ \vdots \\ \mathbf{e}_n(s) \end{pmatrix}$$

*Suspicion: Application to time series analysis? ML?*

C. Jordan, 1874

**Gram-Schmidt on first  $n$  derivatives**

# Continuous Curves

Justin Solomon

6.838: Shape Analysis

Spring 2021



# Extra: First Variation Formula

Justin Solomon

6.838: Shape Analysis

Spring 2021



# Discrete Curves

Justin Solomon

6.838: Shape Analysis

Spring 2021

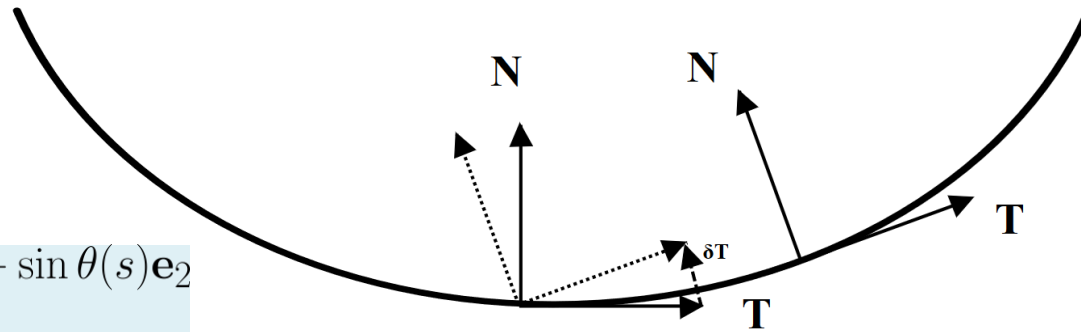


# Frenet Frame: Curves in $\mathbb{R}^2$

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix} := \begin{pmatrix} 0 & \kappa(s) \\ -\kappa(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \end{pmatrix}$$

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$$\begin{aligned} \mathbf{T}(s) &= \cos \theta(s) \mathbf{e}_1 + \sin \theta(s) \mathbf{e}_2 \\ \kappa(s) &:= \theta'(s) \end{aligned}$$



[https://en.wikipedia.org/wiki/Frenet%E2%80%93Serret\\_formulas](https://en.wikipedia.org/wiki/Frenet%E2%80%93Serret_formulas)

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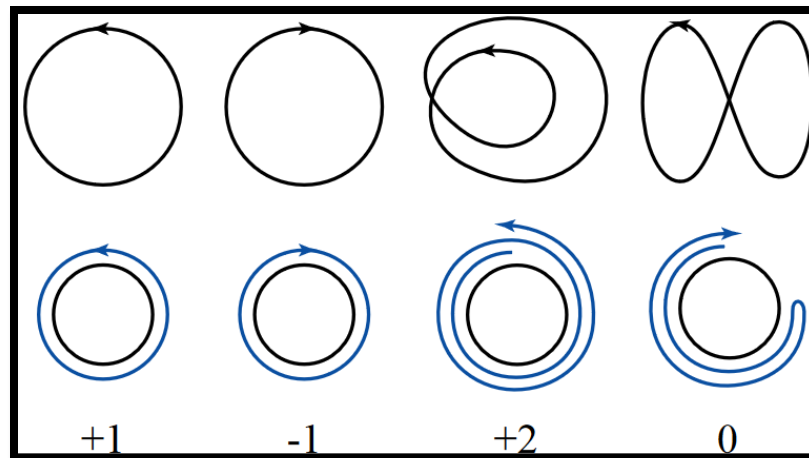
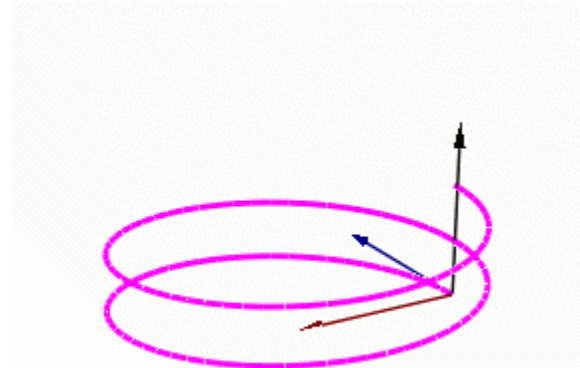
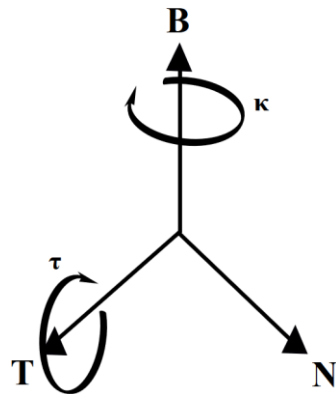


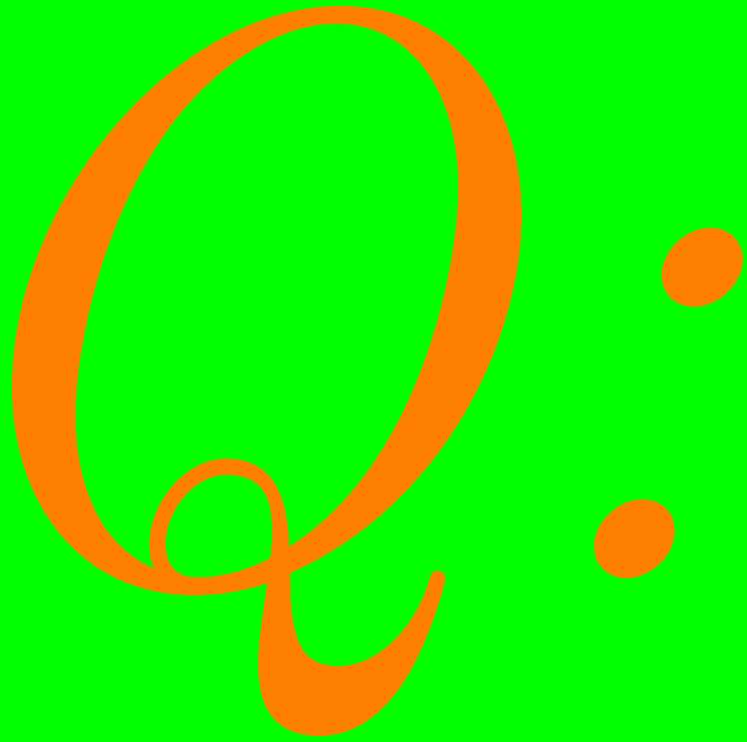
Image from: Grinspun and Secord, "The Geometry of Plane Curves" (SIGGRAPH 2006)

# Frenet Frame: Curves in $\mathbb{R}^3$

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

- **Binormal:**  $\mathbf{T} \times \mathbf{N}$
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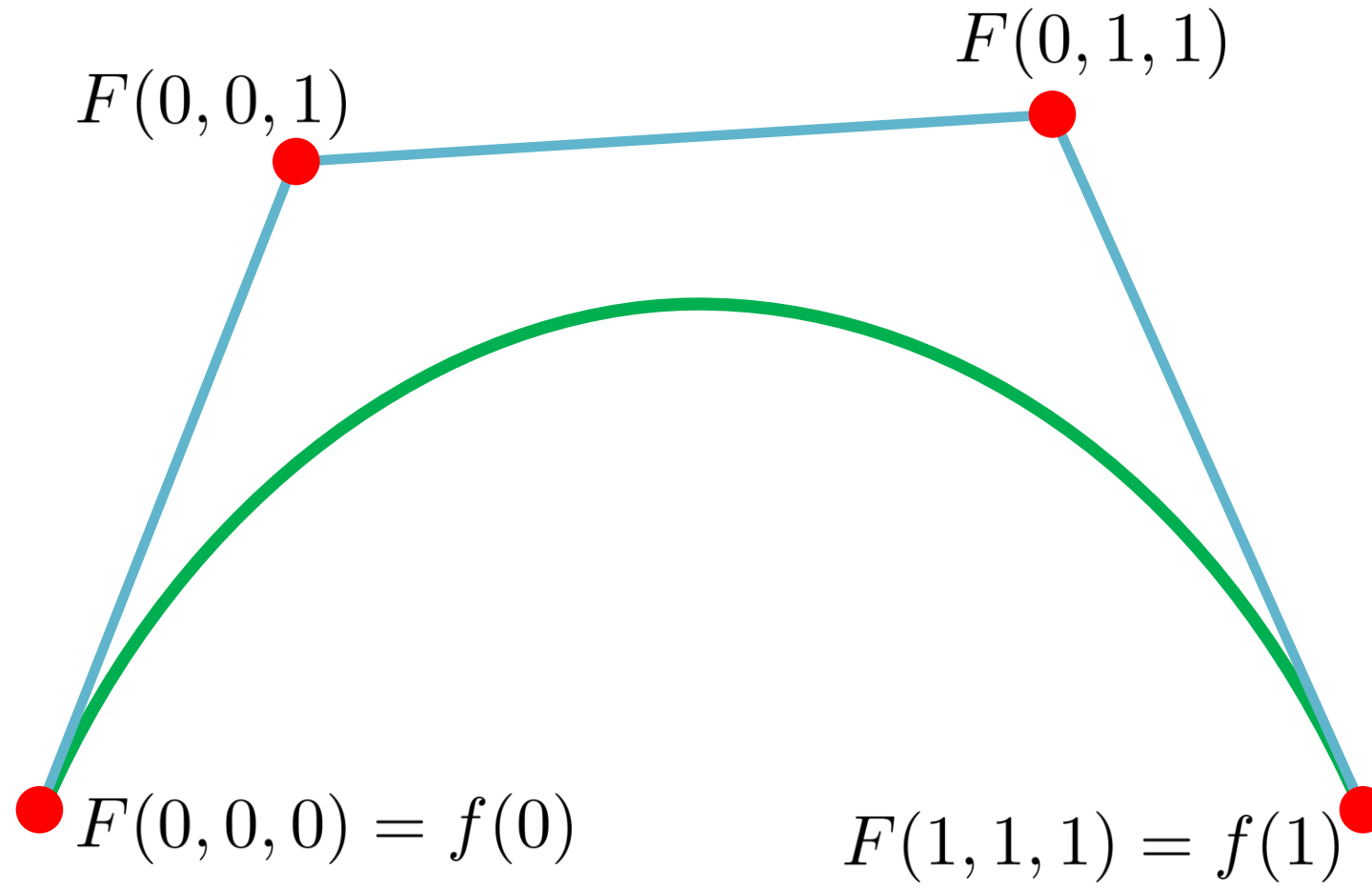




What do these  
calculations look like  
in software?



# Old-School Approach



**Piecewise smooth approximations**

# Question

**What is the arc length of a cubic Bézier curve?**

$$\int_a^b \|\gamma'(t)\|_2 dt$$

# Question

What is the arc length of a cubic Bézier curve?

$$\int_a^b \|\gamma'(t)\|_2 dt$$

Not known in closed form.

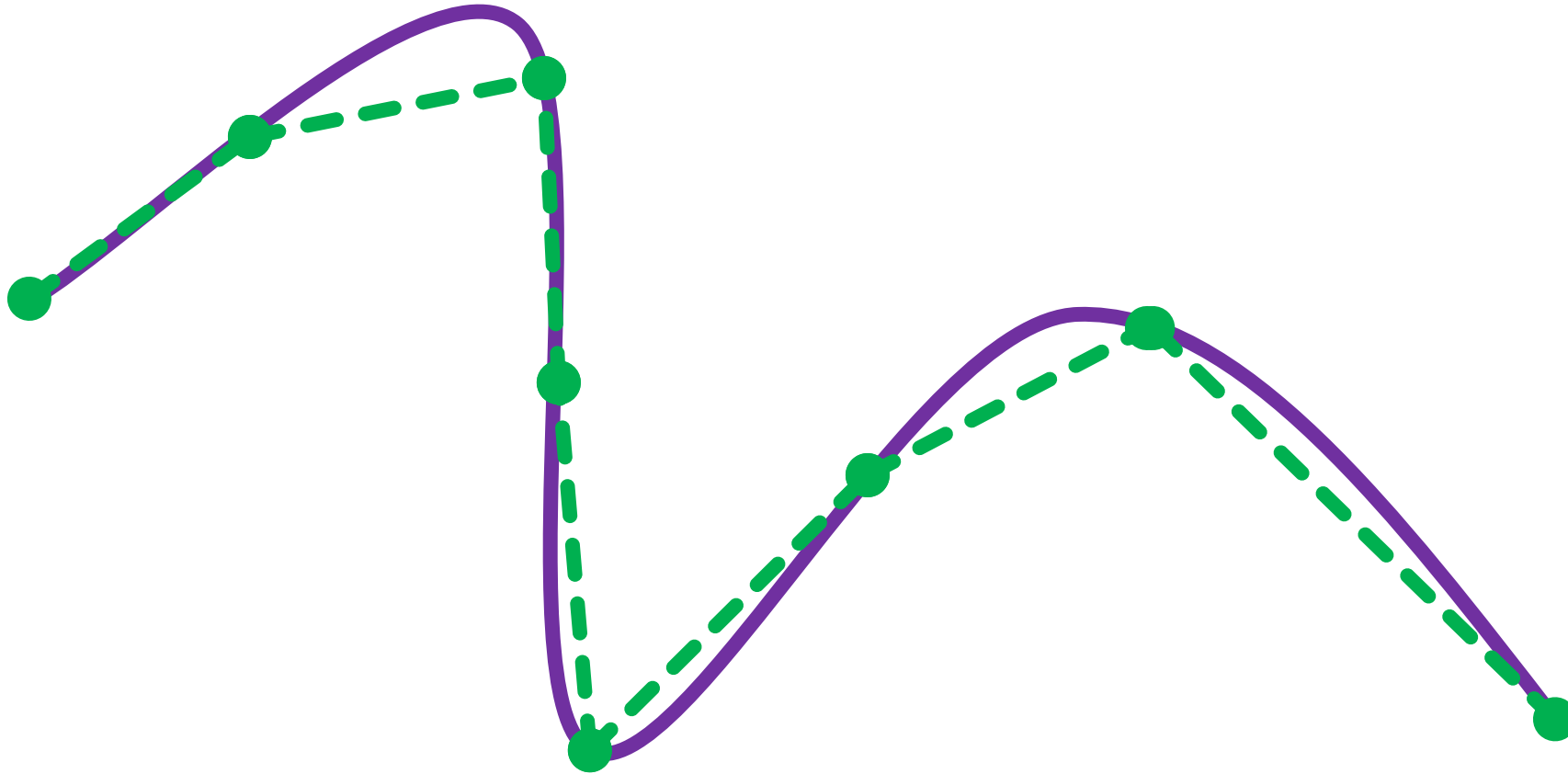
*Sad fact:*

Closed-form  
expressions **rarely exist**.  
When they do exist, they  
usually are **messy**.

# Only Approximations Anyway

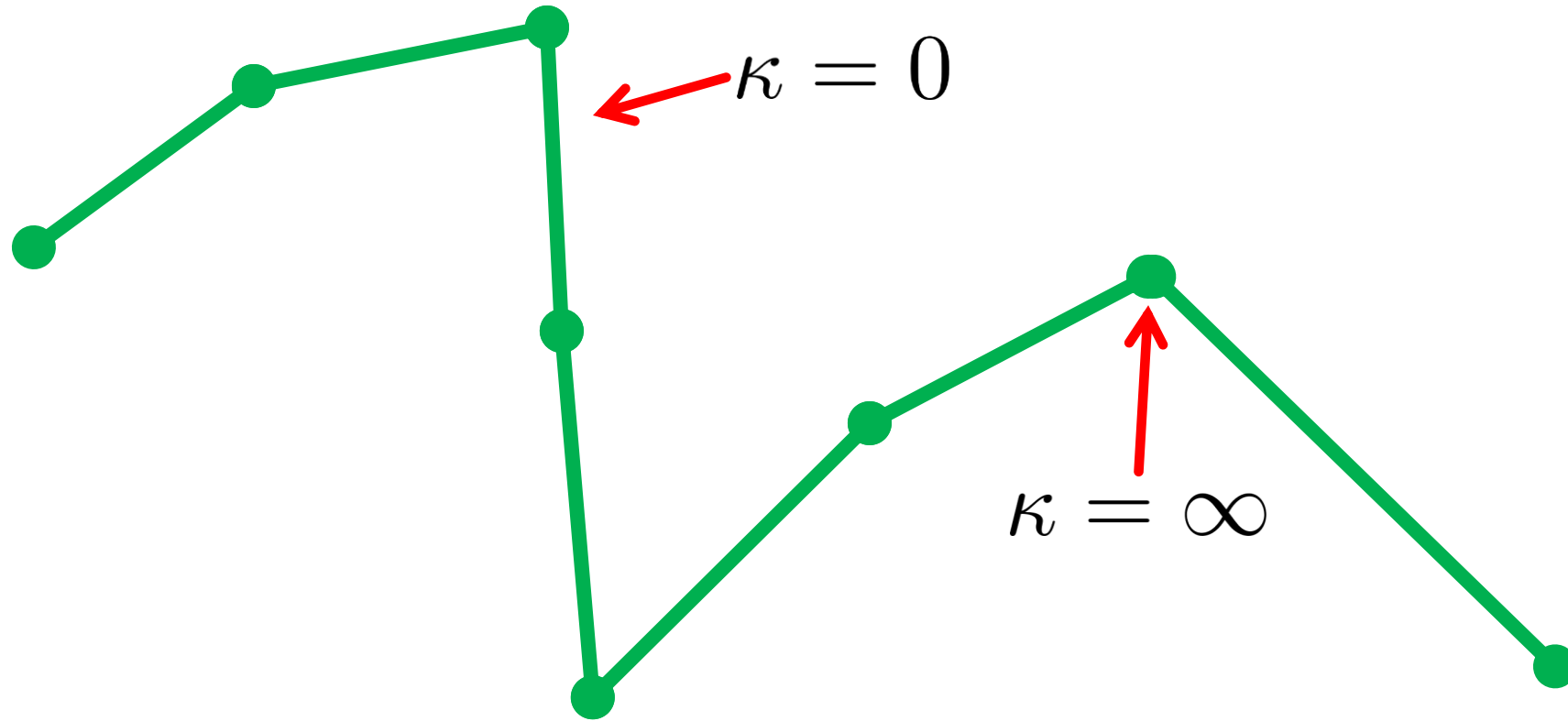
$$\{\text{Bézier curves}\} \subsetneq \{\gamma : \mathbb{R} \rightarrow \mathbb{R}^3\}$$

# Simpler Approximation



**Piecewise linear: Poly-line**

# Big Problem



**Boring differential structure**

# Finite Difference Approach

$$f'(x) \approx \frac{1}{h} [f(x + h) - f(x)]$$

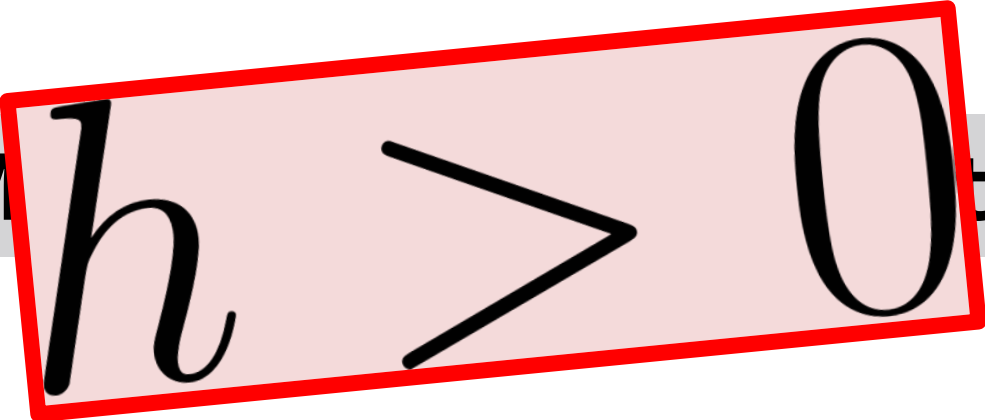
**THEOREM:** As  $\Delta h \rightarrow 0$ , [insert statement].



# Reality Check

$$f'(x) \approx \frac{1}{h} [f(x+h) - f(x)]$$

THEOREM


$$h > 0$$

statement].

# Two Key Considerations

- **Convergence** to continuous theory
- Discrete **behavior**

# Goal

**Examine discrete theories  
of differentiable curves.**

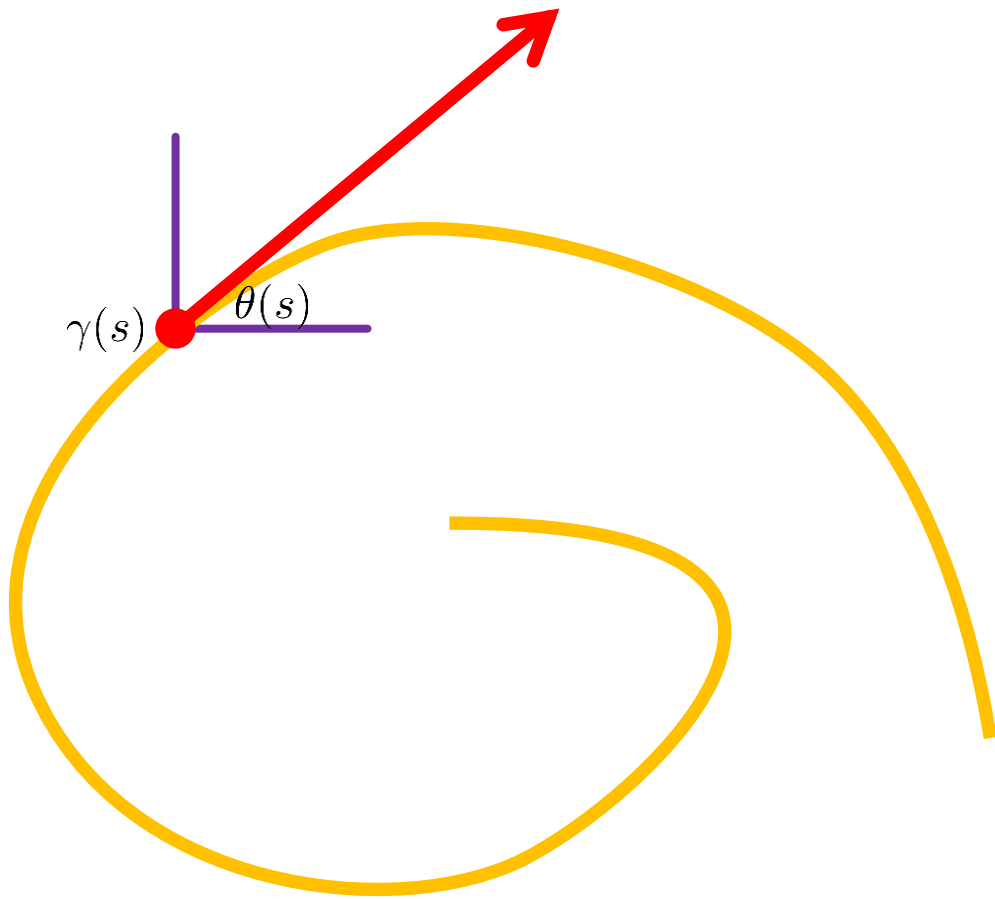
# Goal

**Examine discrete theories  
of differentiable curves.**

Recall:

# Signed Curvature on Plane Curves

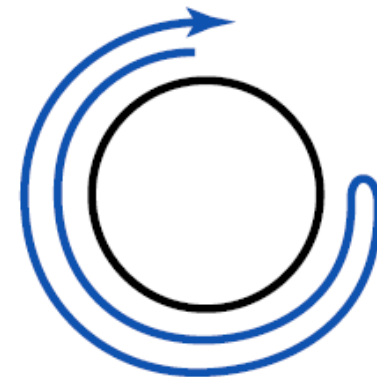
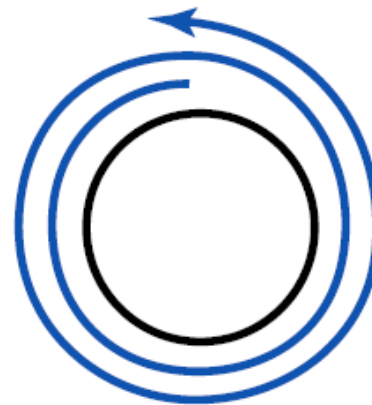
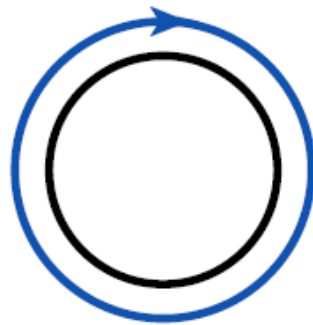
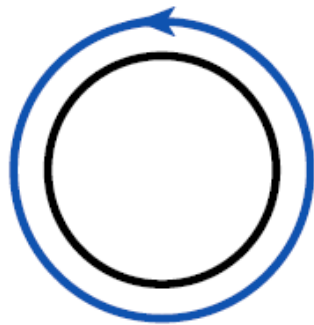
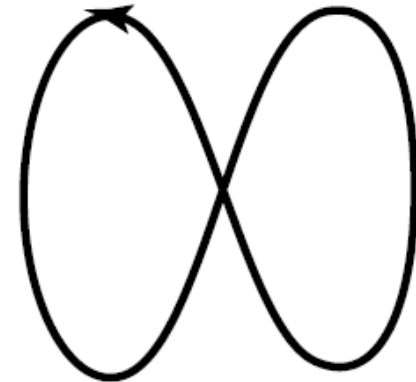
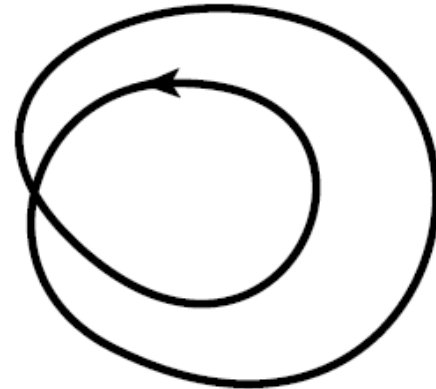
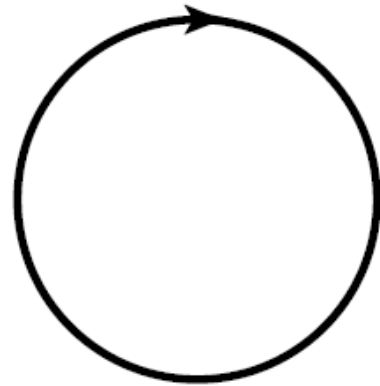
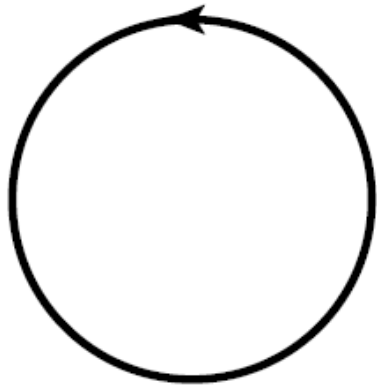
$$\mathbf{T}(s) = (\cos \theta(s), \sin \theta(s))$$



Gauss map:  
Map from curve to its normals.

$$\begin{aligned}\mathbf{T}'(s) &= \theta'(s)(-\sin \theta(s), \cos \theta(s)) \\ &:= \kappa(s)\mathbf{N}(s)\end{aligned}$$

# Turning Numbers



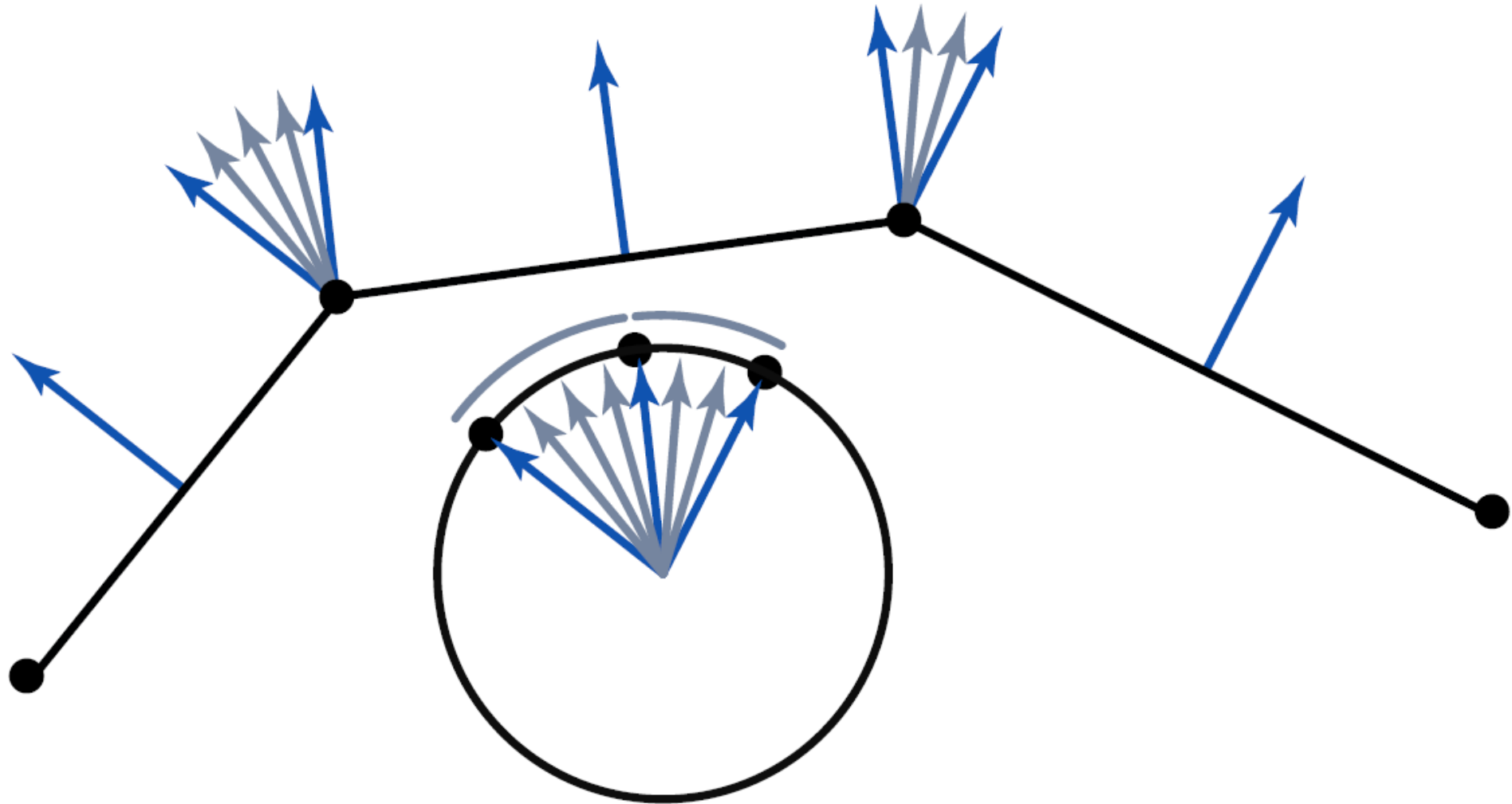
+1

-1

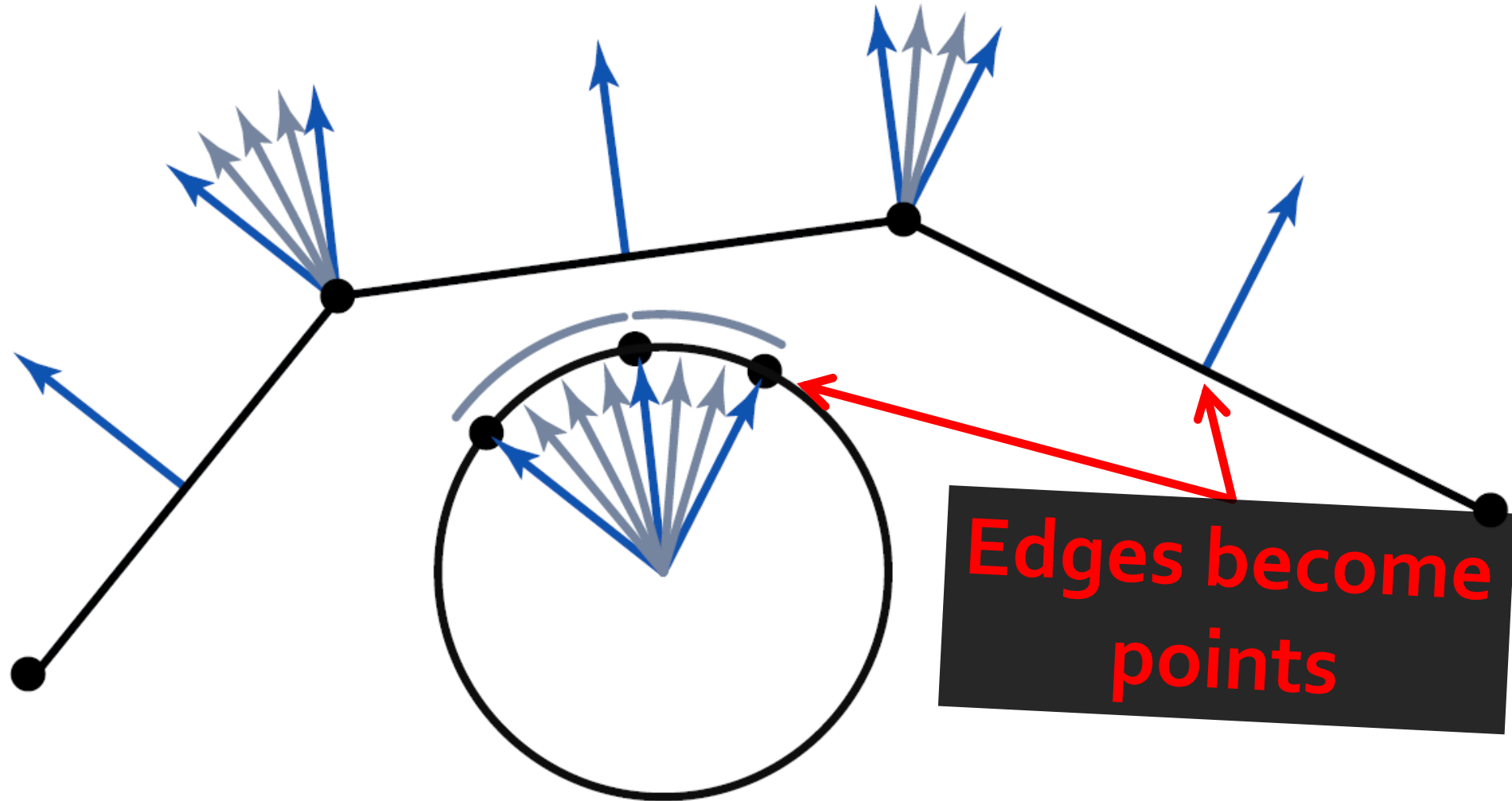
+2

0

# Discrete Gauss Map

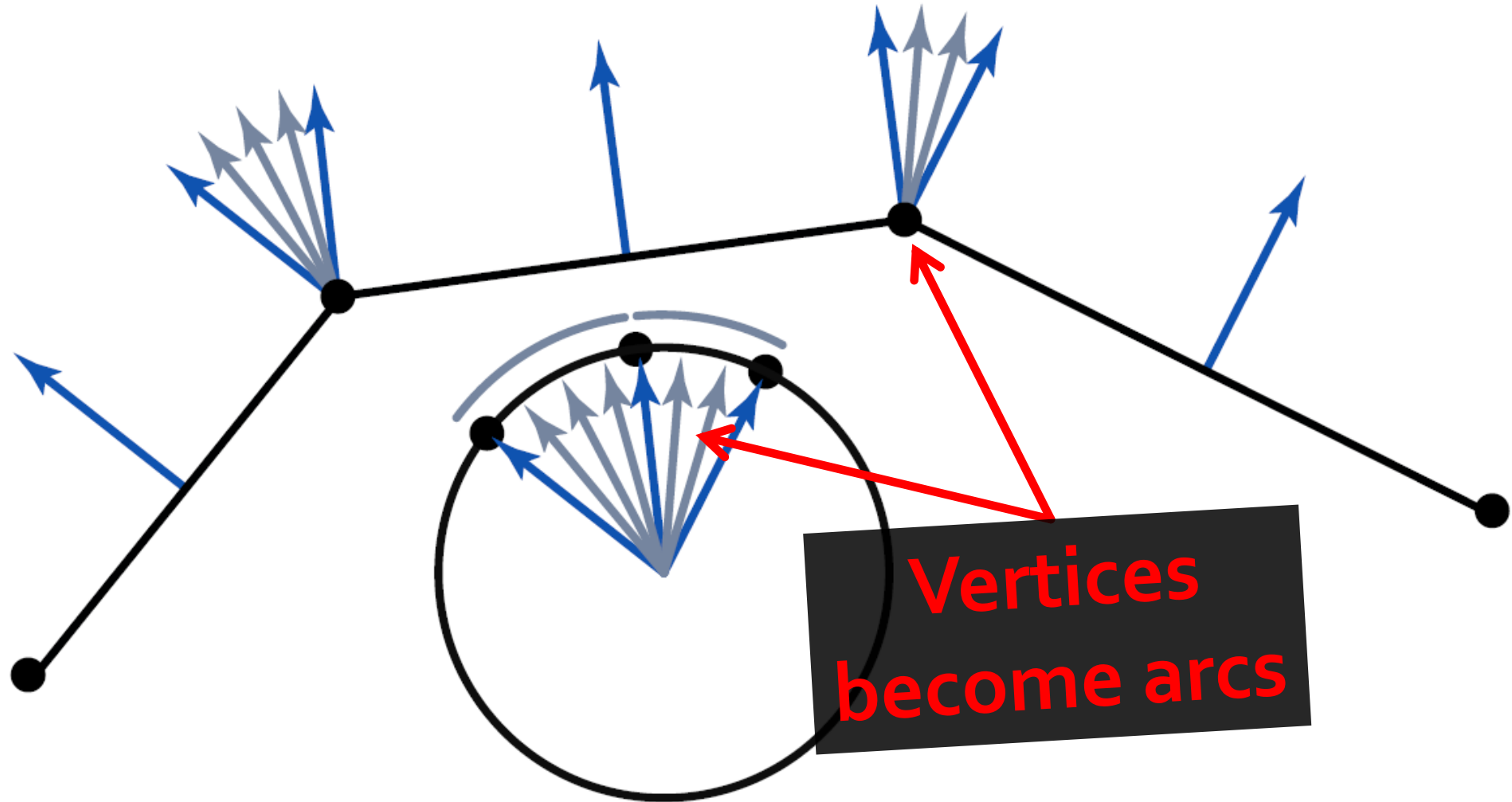


# Discrete Gauss Map

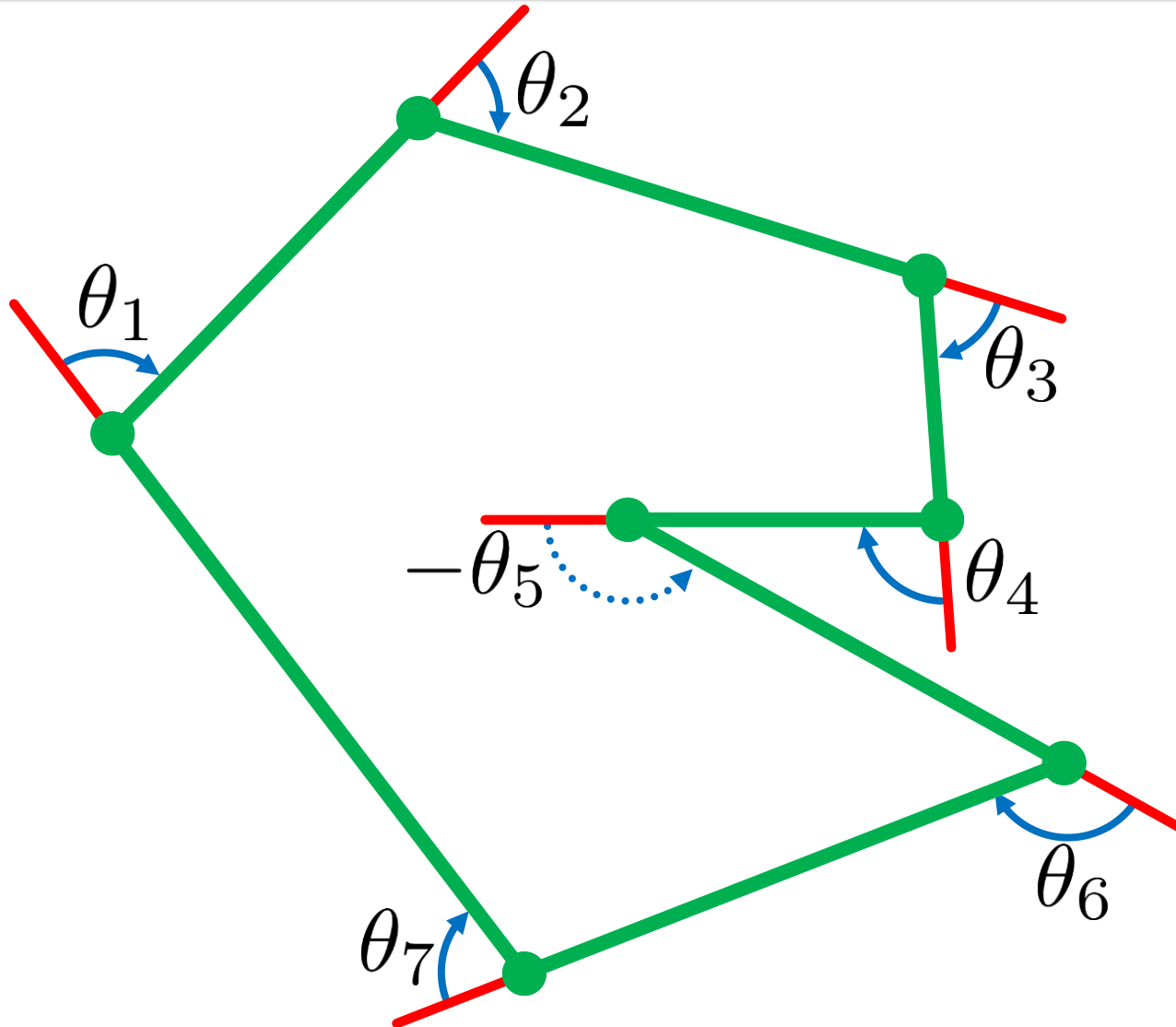




# Discrete Gauss Map



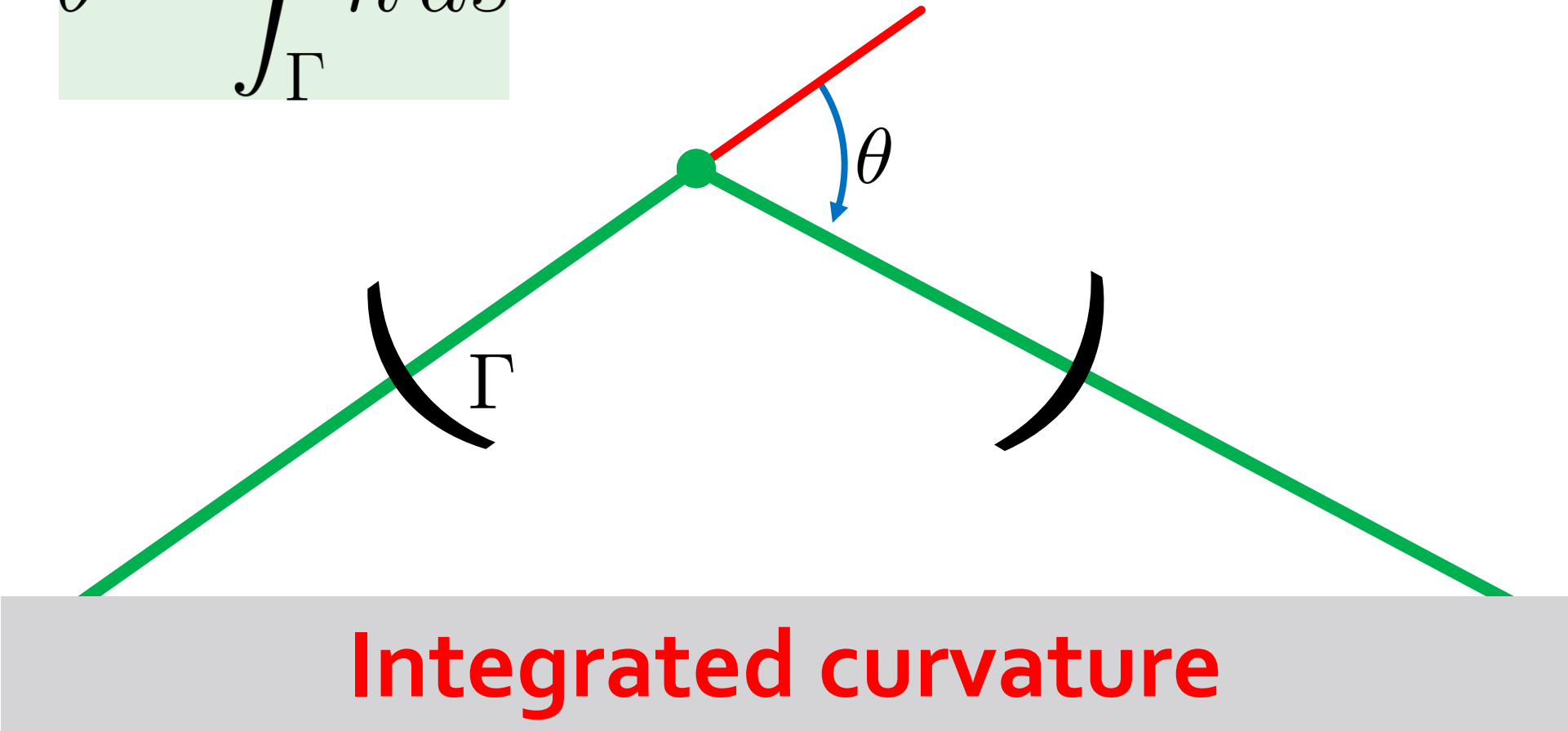
# Key Observation



$$\sum_i \theta_i = 2\pi k$$

# What's Going On?

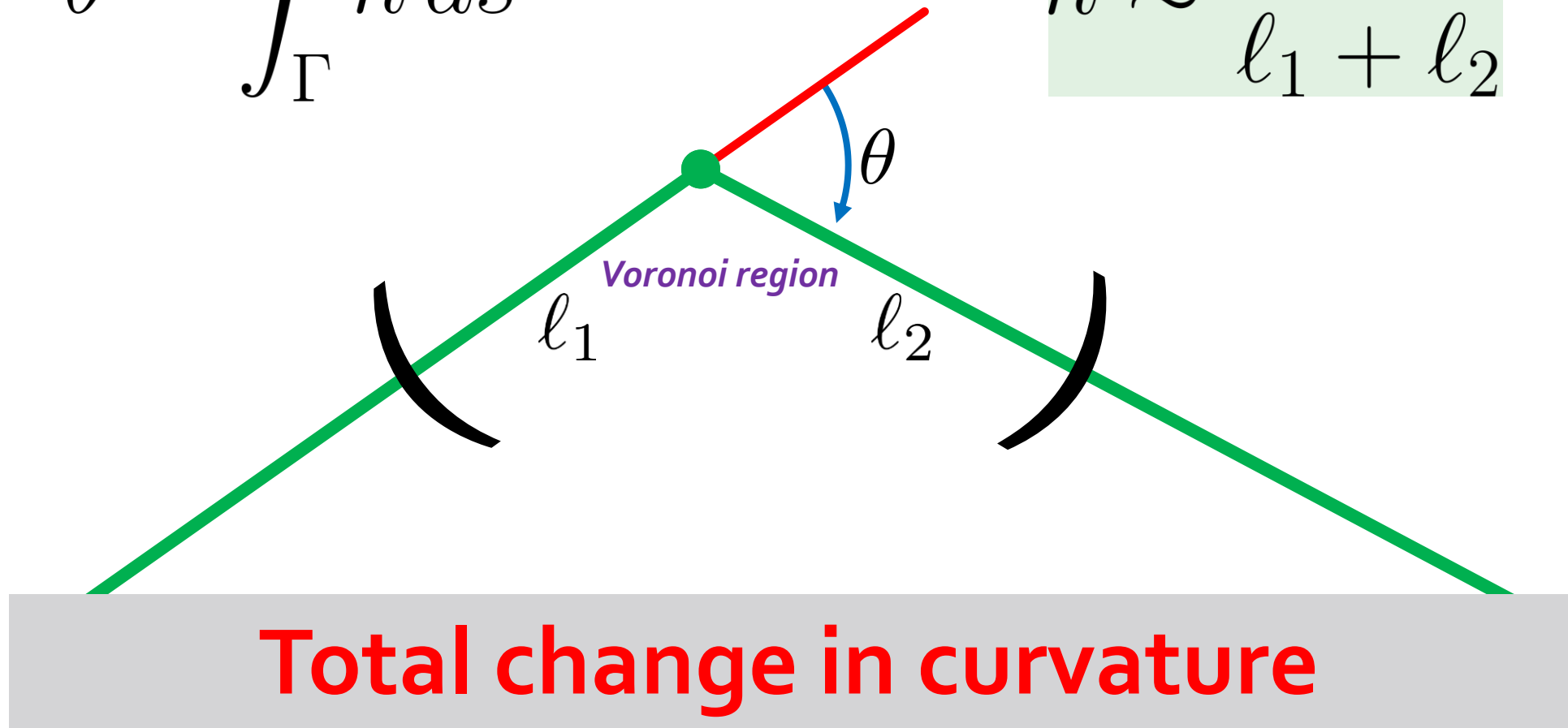
$$\theta = \int_{\Gamma} \kappa \, ds$$



# What's Going On?

$$\theta = \int_{\Gamma} \kappa \, ds$$

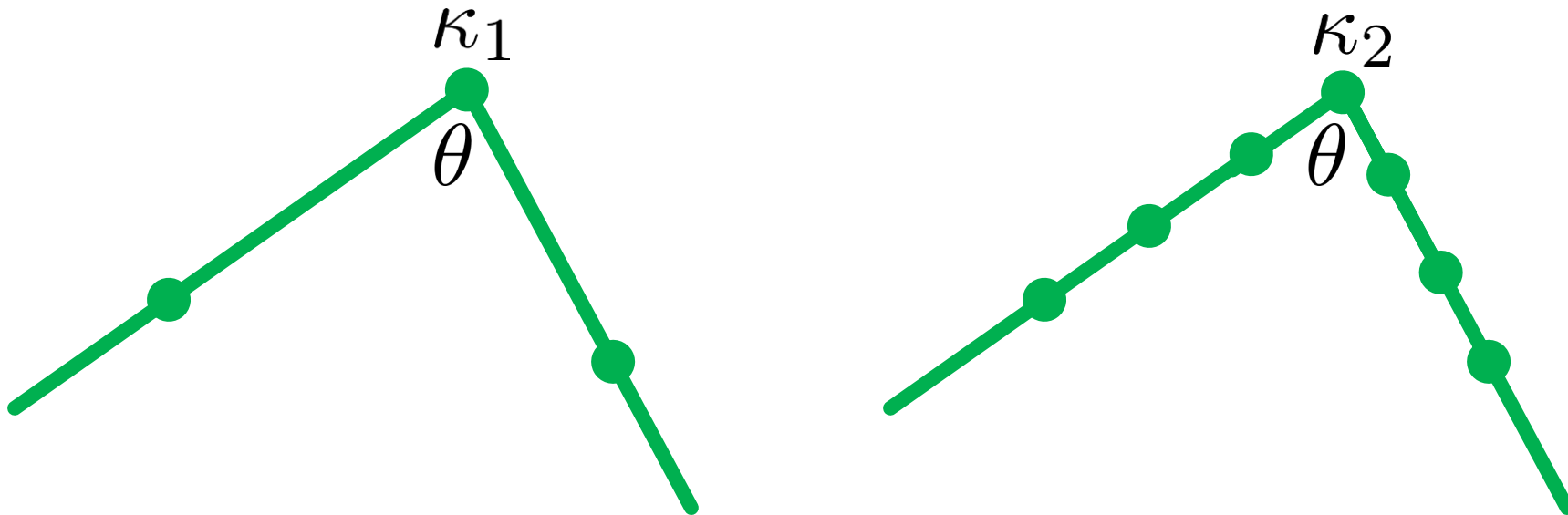
$$\kappa \approx \frac{\theta}{\ell_1 + \ell_2}$$



**Total change in curvature**

# Interesting Distinction

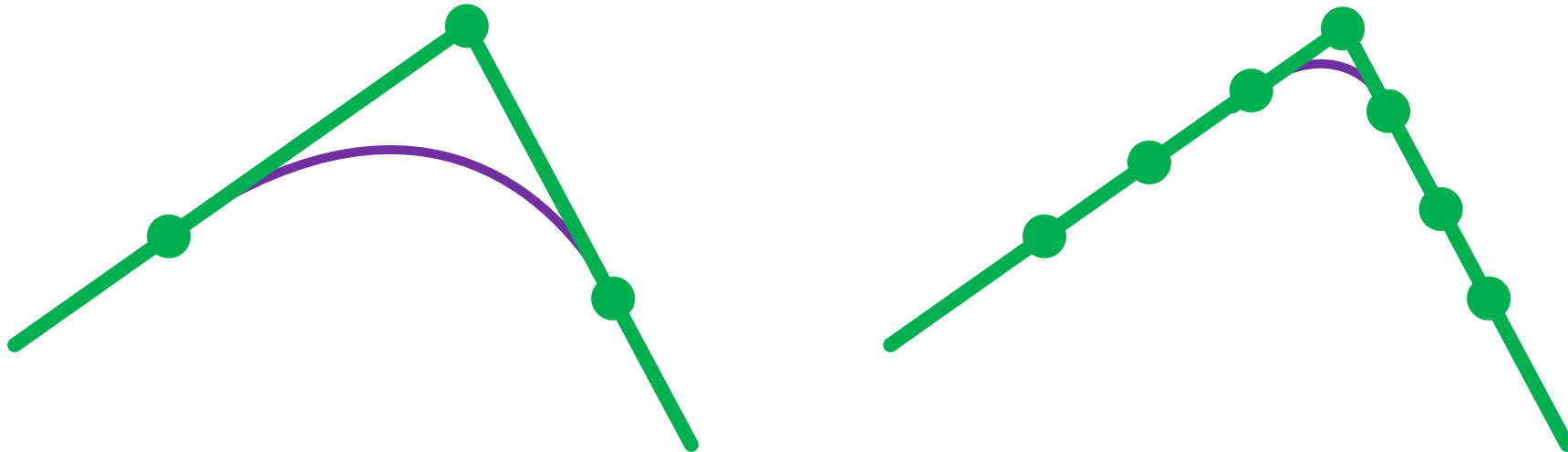
$$\kappa_1 \neq \kappa_2$$



Same integrated curvature

# Interesting Distinction

$$\kappa_1 \neq \kappa_2$$



Same integrated curvature

# What's Going On?

$$\theta = \int_{\Gamma} \kappa \, ds$$

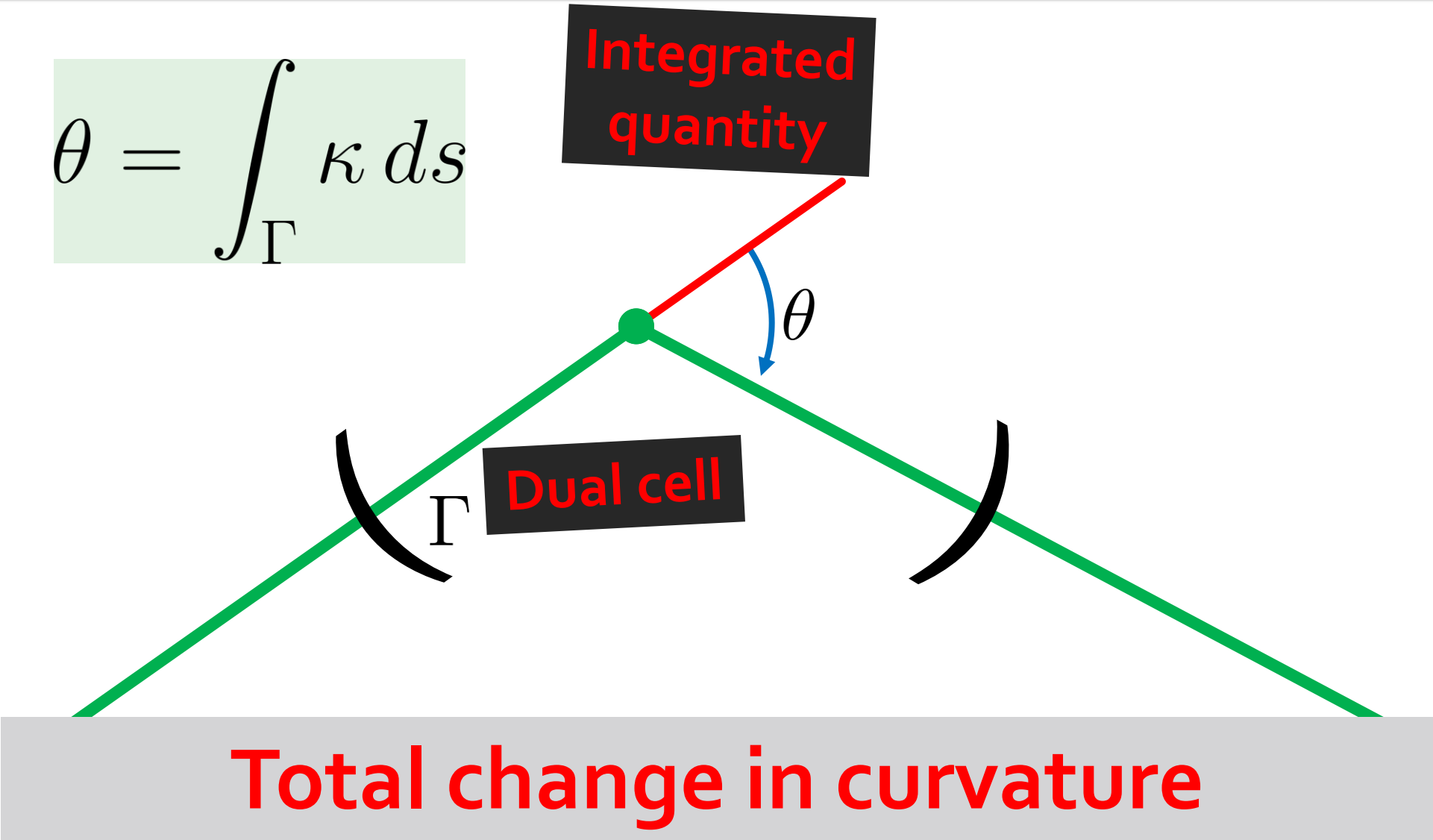
Integrated  
quantity

$\theta$

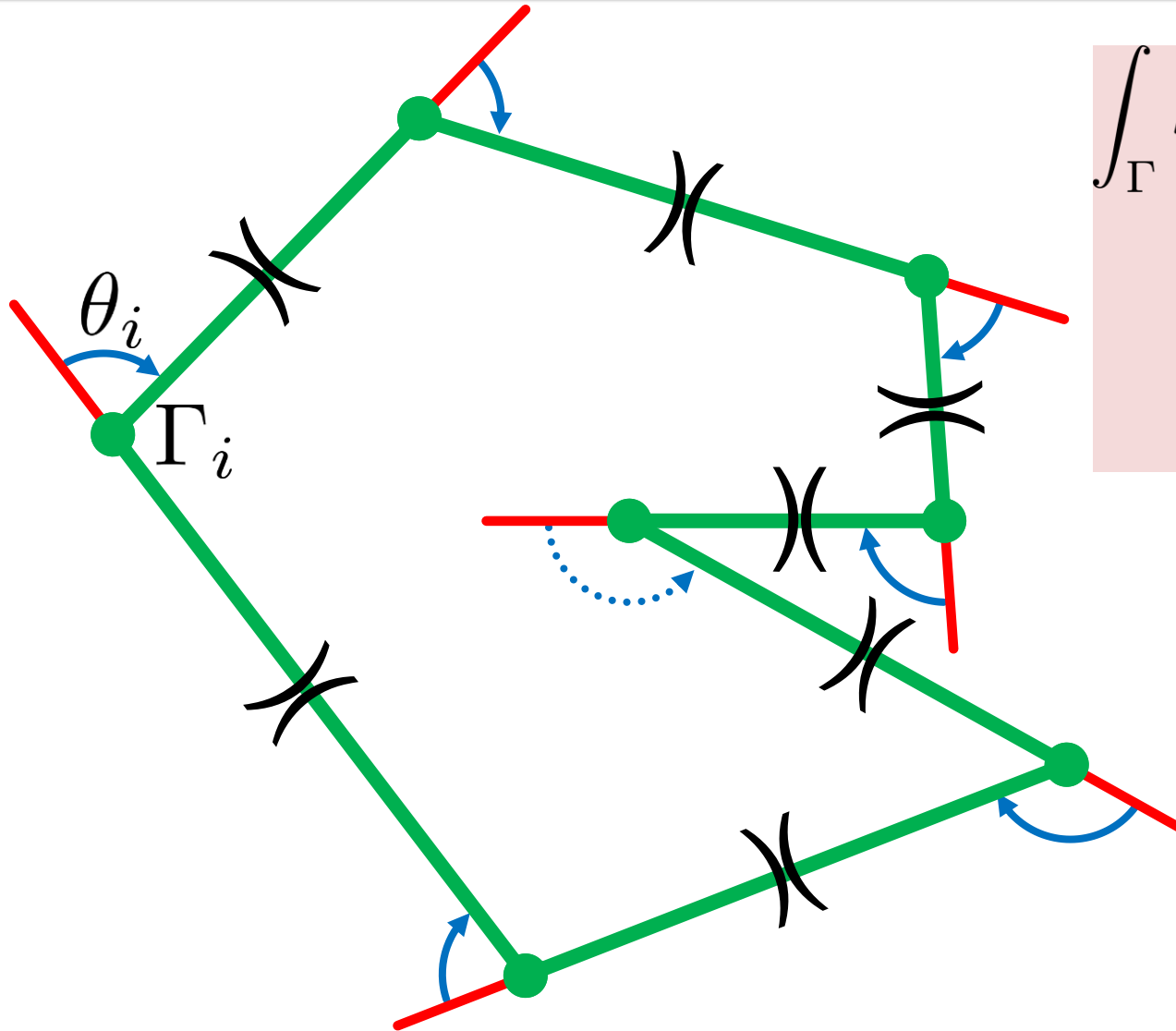
Dual cell

$\Gamma$

Total change in curvature



# Discrete Turning Angle Theorem

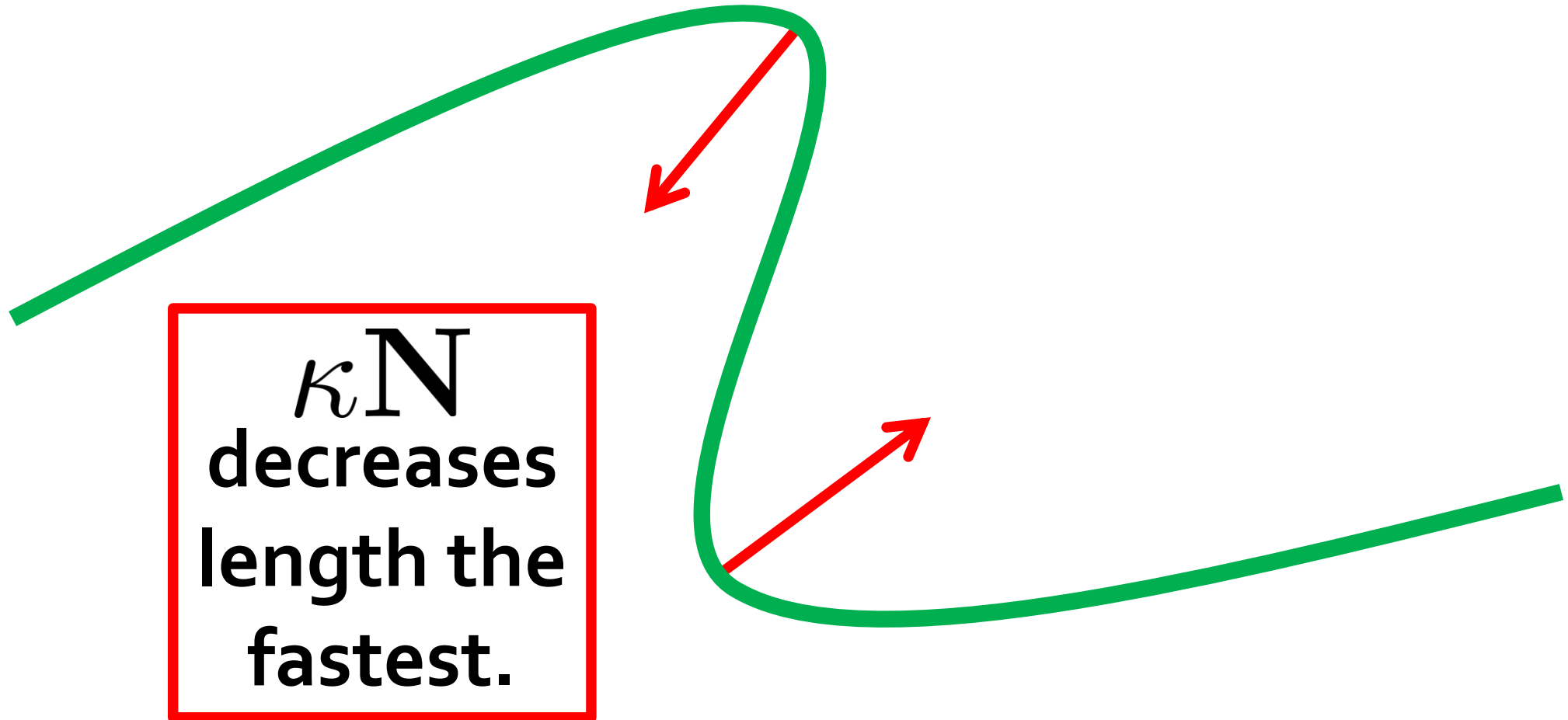


$$\begin{aligned}\int_{\Gamma} \kappa \, ds &= \sum_i \int_{\Gamma_i} \kappa \, ds \\ &= \sum_i \theta_i \\ &= 2\pi k\end{aligned}$$

**Preserved  
structure!**

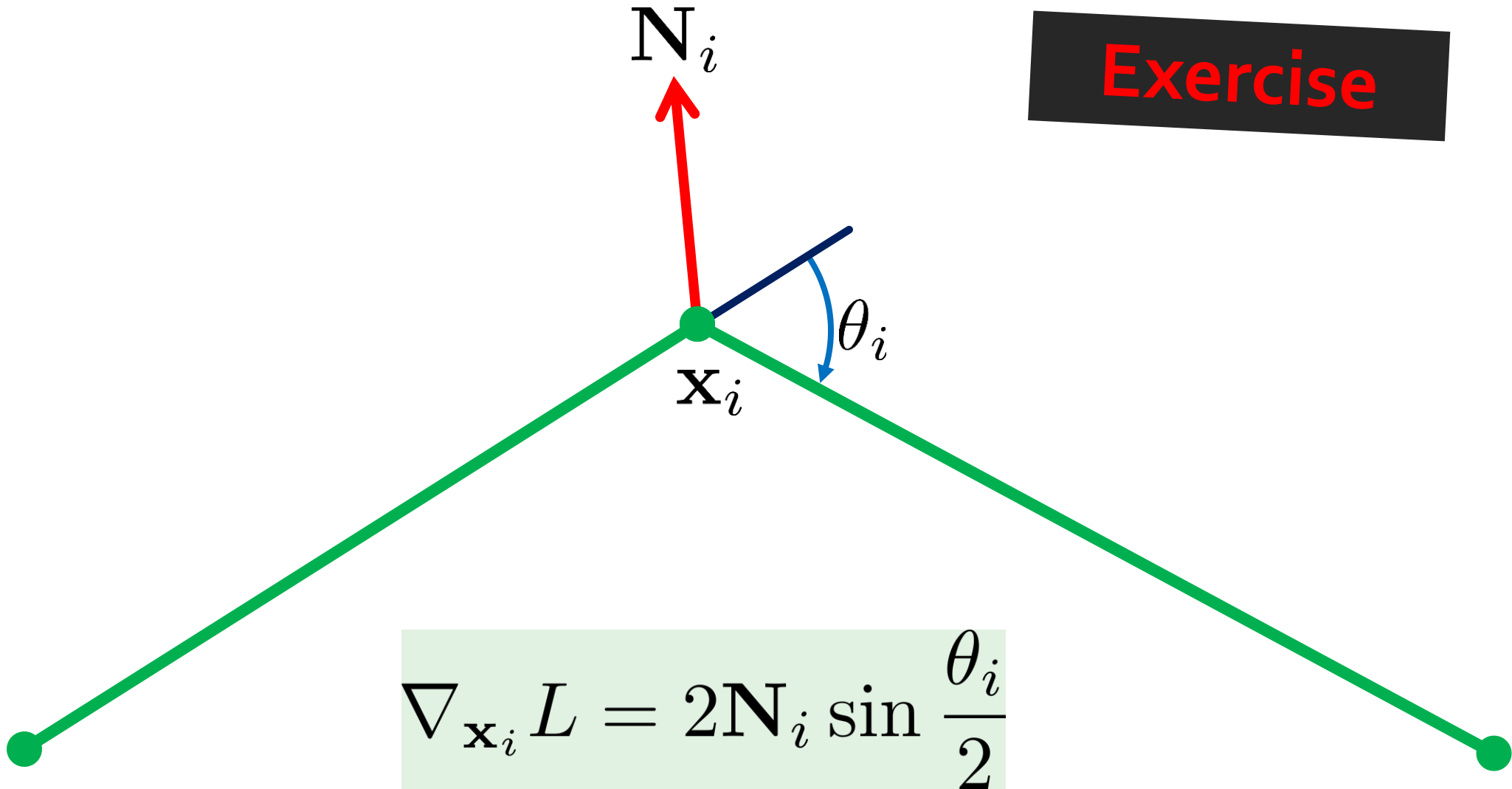


# First Variation Formula

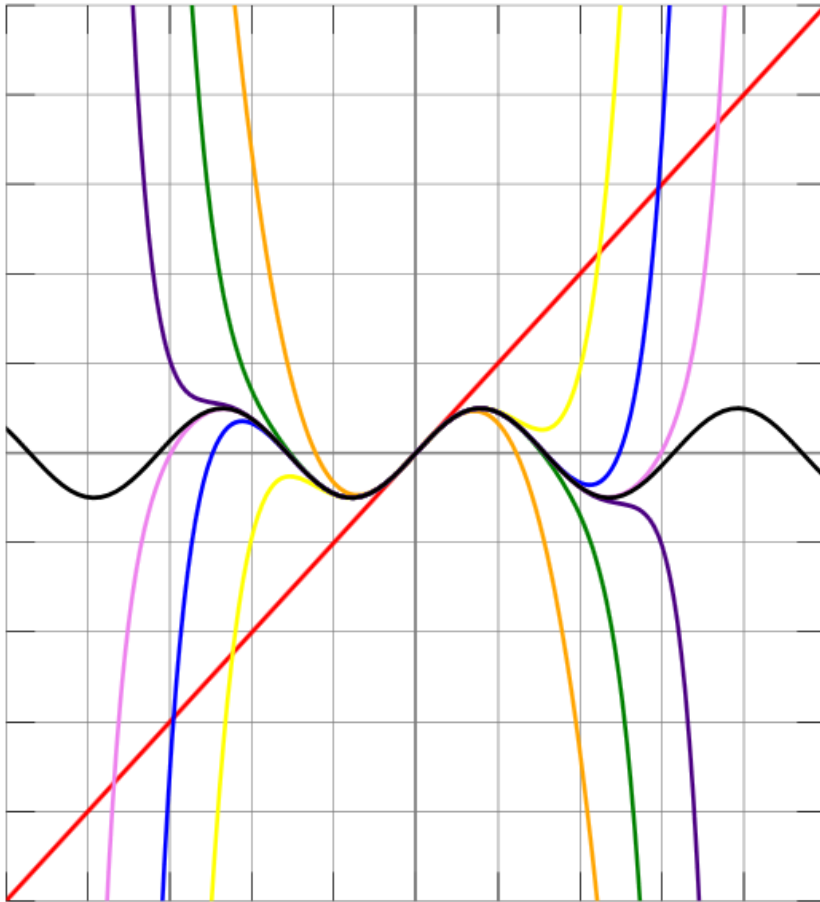


# Discrete Case

Exercise



# For Small $\theta$



[http://en.wikipedia.org/wiki/Taylor\\_series](http://en.wikipedia.org/wiki/Taylor_series)

$$2 \sin \frac{\theta}{2} \approx 2 \cdot \frac{\theta}{2} \\ = \theta$$

**Same behavior in the limit**

# No Free Lunch

*Choose one:*

- Discrete curvature with  
**turning angle theorem**
- Discrete curvature from  
**gradient of arc length**



# Remaining Question

**Does discrete curvature  
converge in limit?**

*Yes!*  
*Under some assumptions!*

# Remaining Question

**Does discrete curvature  
converge in limit?**

Questions:

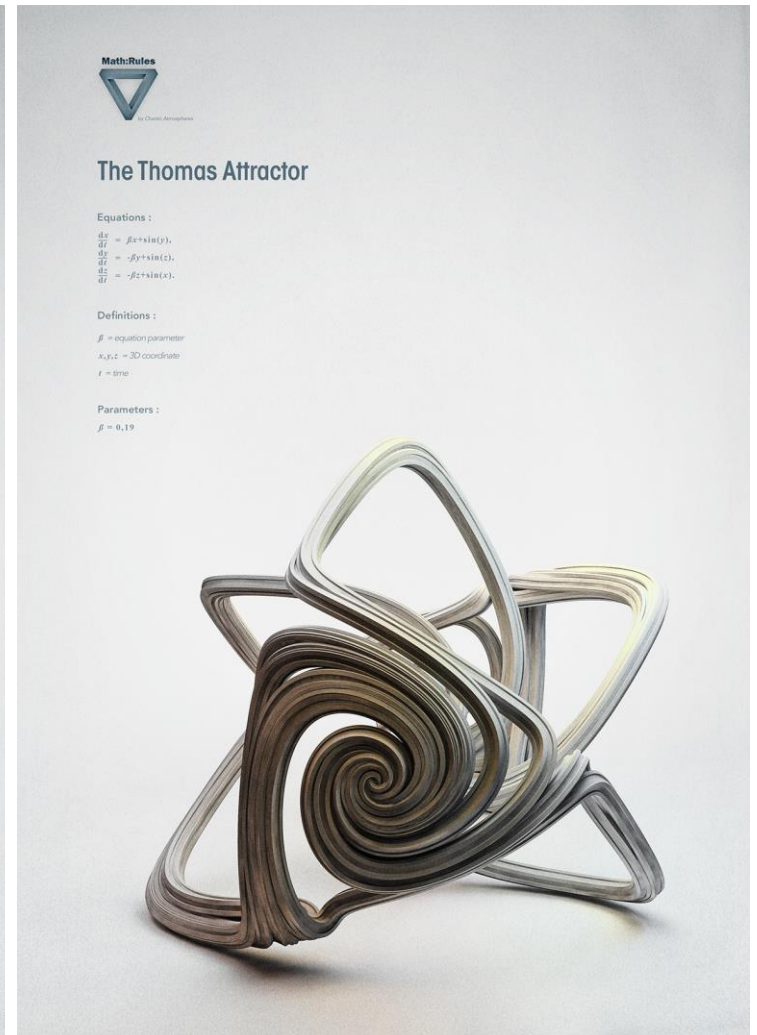
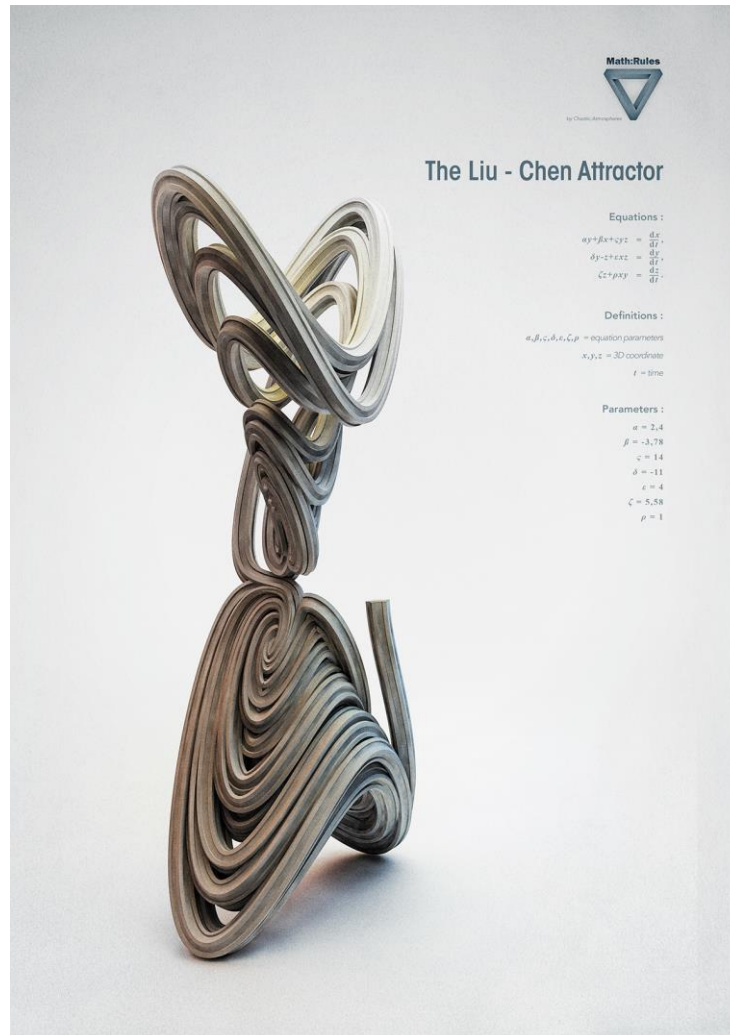
- Type of convergence?
- Sampling?
- Class of curves?

*Yes!*  
*Under some assumptions!*

# Discrete Differential Geometry

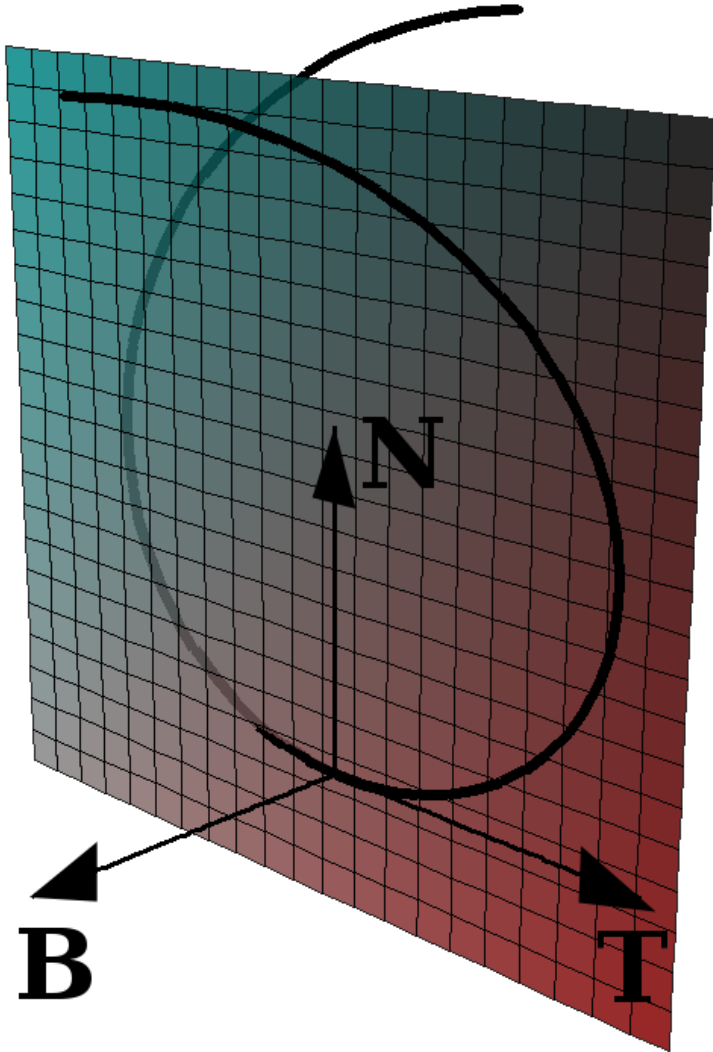
- **Different** discrete behavior
- **Same** convergence

# Curves in 3D?





# Frenet Frame

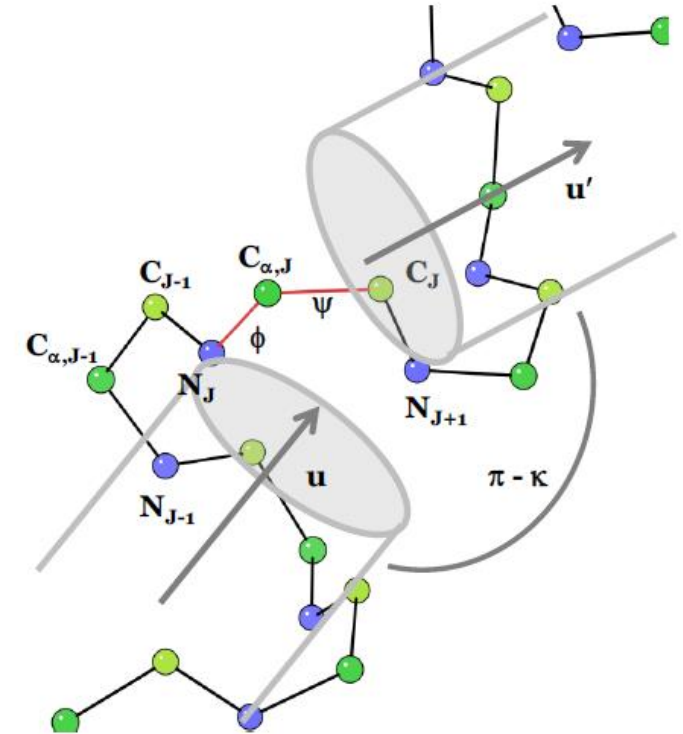
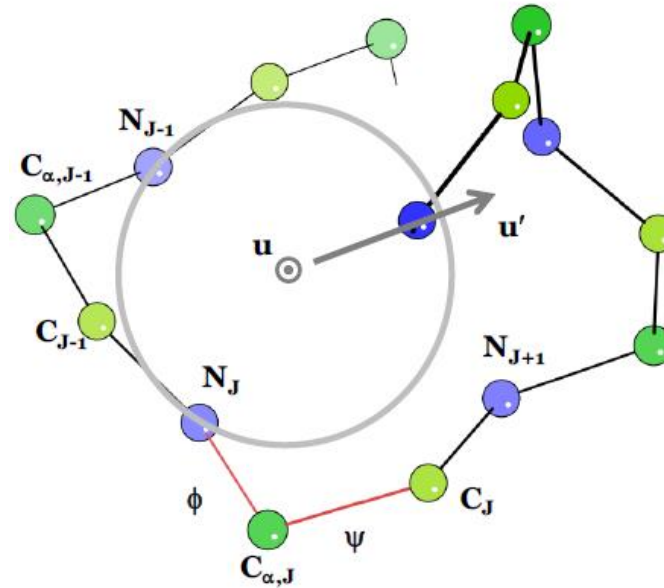


$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

# Application



**NMR scanner**



**Kinked alpha helix**

Structure Determination of Membrane Proteins Using Discrete Frenet Frame and Solid State NMR Restraints

Achuthan and Quine

*Discrete Mathematics and its Applications*, ed. M. Sethumadhavan (2006)

# Potential Discretization

$$\begin{aligned}\mathbf{T}_j &= \frac{\mathbf{p}_{j+1} - \mathbf{p}_j}{\|\mathbf{p}_{j+1} - \mathbf{p}_j\|_2} \\ \mathbf{B}_j &= \mathbf{T}_{j-1} \times \mathbf{T}_j \\ \mathbf{N}_j &= \mathbf{B}_j \times \mathbf{T}_j\end{aligned}$$

**Discrete Frenet frame**

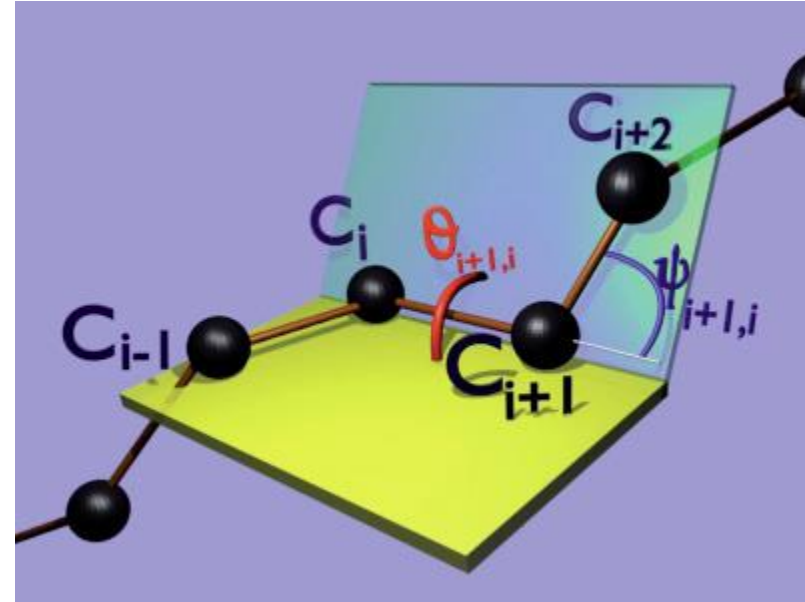
$$\begin{aligned}\mathbf{T}_k &= R(\mathbf{B}_k, \theta_k) \mathbf{T}_{k-1} \\ \mathbf{B}_{k+1} &= R(\mathbf{T}_k, \phi_k) \mathbf{B}_k\end{aligned}$$

**“Bond and torsion angles”**  
(derivatives converge to  $\kappa$   
and  $\tau$ , resp.)

*Discrete frame introduced in:*  
The resultant electric moment of complex molecules  
Eyring, Physical Review, 39(4):746—748, 1932.

# Transfer Matrix

$$\begin{pmatrix} \mathbf{T}_{i+1} \\ \mathbf{N}_{i+1} \\ \mathbf{B}_{i+1} \end{pmatrix} = R_{i+1,i} \begin{pmatrix} \mathbf{T}_i \\ \mathbf{N}_i \\ \mathbf{B}_i \end{pmatrix}$$

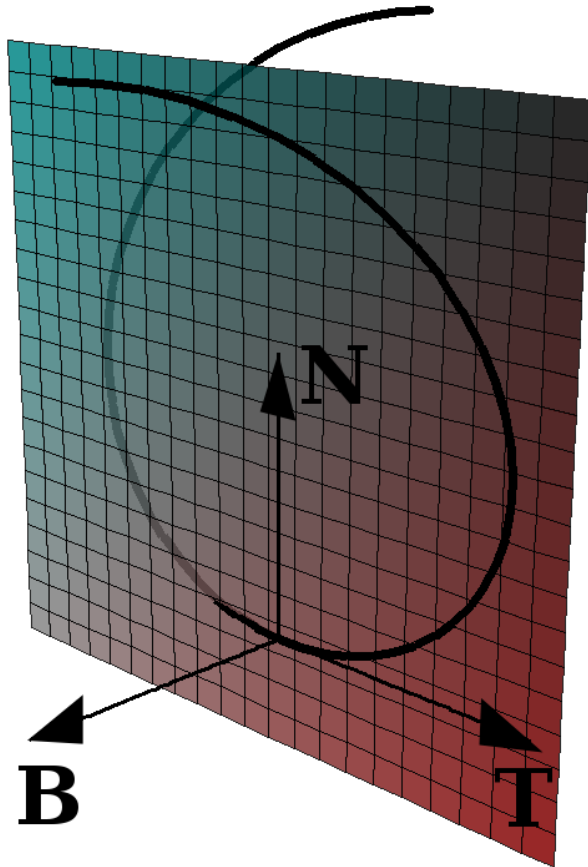


**Discrete construction that works for fractal curves  
and converges in continuum limit.**

Discrete Frenet Frame, Inflection Point Solitons, and Curve Visualization  
with Applications to Folded Proteins

Hu, Lundgren, and Niemi  
*Physical Review E* 83 (2011)

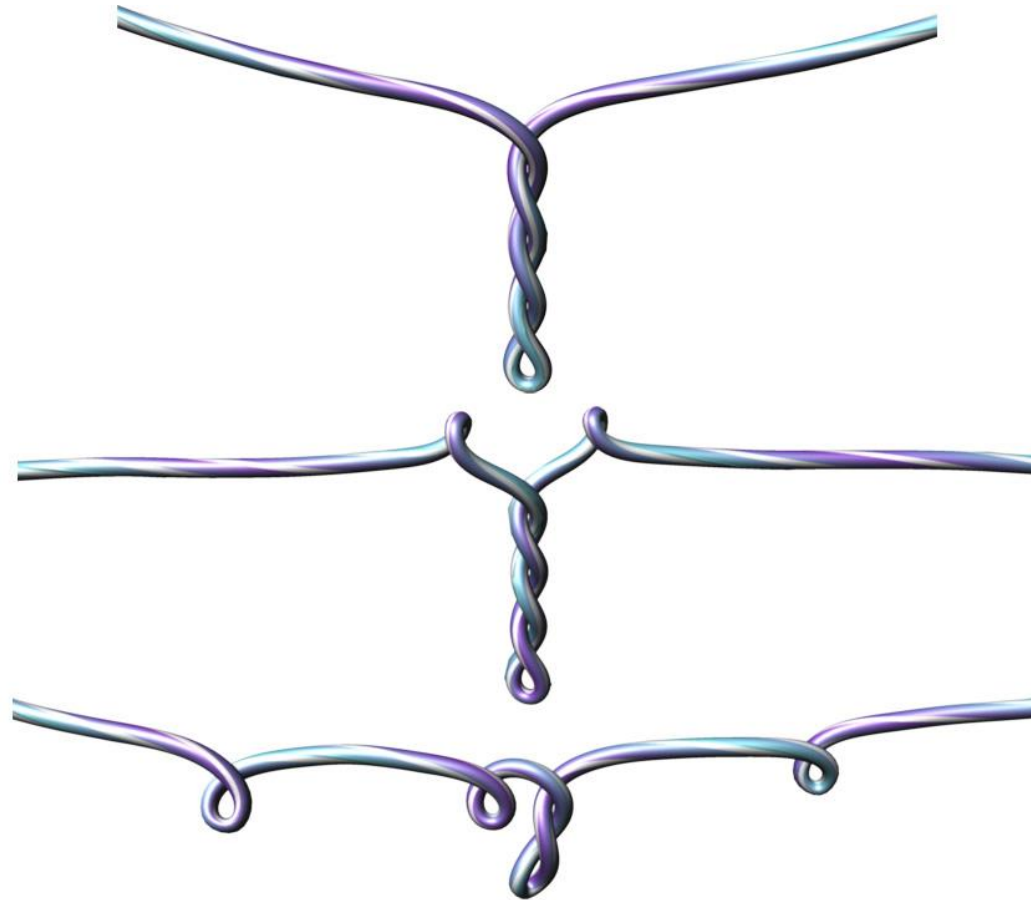
# Frenet Frame: Issue



$$\kappa = 0?$$

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \boxed{\kappa(s)} & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

# Segments Not Always Enough

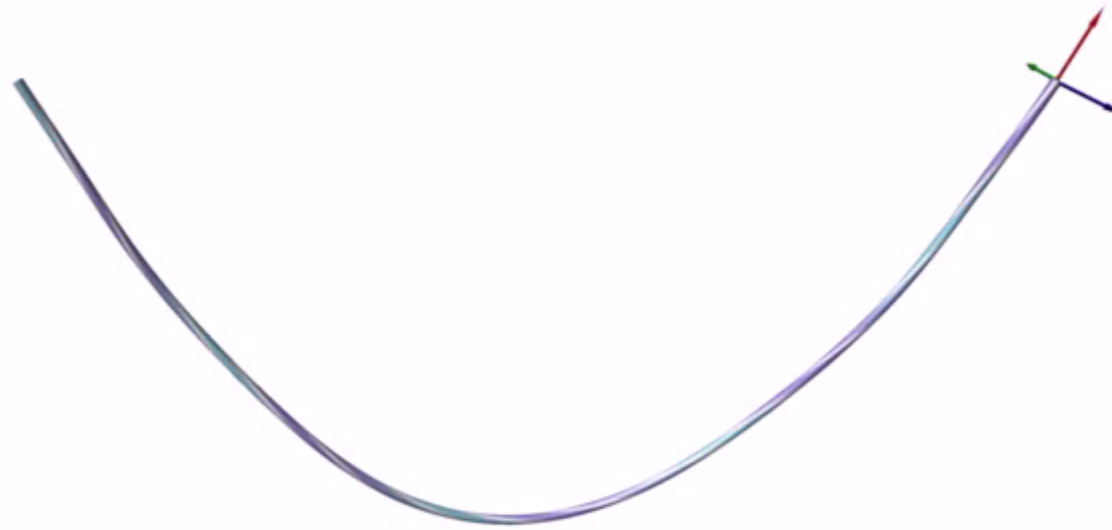


## Discrete Elastic Rods

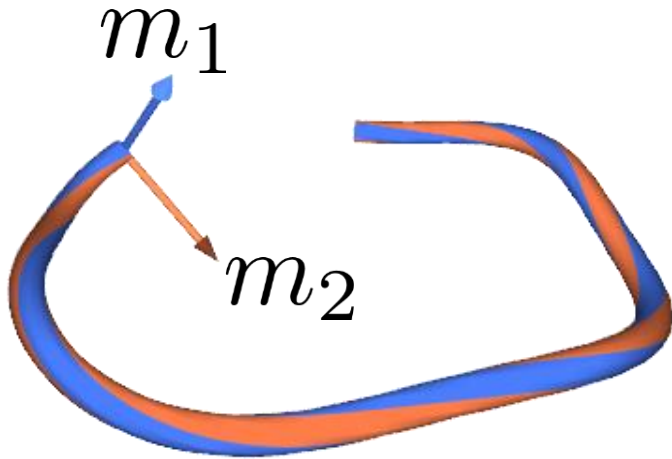
Bergou, Wardetzky, Robinson, Audoly, and Grinspun

*SIGGRAPH* 2008

# Simulation Goal



# Adapted Framed Curve



$$\Gamma = \{\gamma(s); \mathbf{T}, \mathbf{m}_1, \mathbf{m}_2\}$$

**Material frame**

**Normal part encodes twist**



# Bending Energy

$$E_{\text{bend}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \alpha \kappa^2 ds$$

Penalize turning the steering wheel

---

$$\begin{aligned} \kappa \mathbf{N} &= \mathbf{T}' \\ &= (\mathbf{T}' \cdot \mathbf{T})\mathbf{T} + (\mathbf{T}' \cdot \mathbf{m}_1)\mathbf{m}_1 + (\mathbf{T}' \cdot \mathbf{m}_2)\mathbf{m}_2 \\ &= (\mathbf{T}' \cdot \mathbf{m}_1)\mathbf{m}_1 + (\mathbf{T}' \cdot \mathbf{m}_2)\mathbf{m}_2 \\ &:= \omega_1 \mathbf{m}_1 + \omega_2 \mathbf{m}_2 \end{aligned}$$

# Bending Energy

$$E_{\text{bend}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \alpha(\omega_1^2 + \omega_2^2) ds$$

Penalize turning the steering wheel

---

$$\begin{aligned} \kappa \mathbf{N} &= \mathbf{T}' \\ &= (\mathbf{T}' \cdot \mathbf{T})\mathbf{T} + (\mathbf{T}' \cdot \mathbf{m}_1)\mathbf{m}_1 + (\mathbf{T}' \cdot \mathbf{m}_2)\mathbf{m}_2 \\ &= (\mathbf{T}' \cdot \mathbf{m}_1)\mathbf{m}_1 + (\mathbf{T}' \cdot \mathbf{m}_2)\mathbf{m}_2 \\ &:= \omega_1 \mathbf{m}_1 + \omega_2 \mathbf{m}_2 \end{aligned}$$

# Twisting Energy

$$E_{\text{twist}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \beta m^2 ds$$

Punish non-tangent change in material frame

---

$$m := \mathbf{m}'_1 \cdot \mathbf{m}_2$$

$$= \frac{d}{dt}(\mathbf{m}_1 \cdot \mathbf{m}_2) - \mathbf{m}_1 \cdot \mathbf{m}'_2$$

$$= -\mathbf{m}_1 \cdot \mathbf{m}'_2$$

← Swapping  $m_1$  and  $m_2$   
does not affect  $E_{\text{twist}}$ !

# Bishop Frame: The Hipster Framed Curve

## THERE IS MORE THAN ONE WAY TO FRAME A CURVE

RICHARD L. BISHOP

The Frenet frame of a 3-times continuously differentiable (that is,  $C^3$ ) non-degenerate curve in euclidean space has long been the standard vehicle for analysing properties of the curve invariant under euclidean motions. For arbitrary moving frames, that is, orthonormal basis fields, we can express the derivatives of the frame with respect to the curve parameter in terms of the frame itself, and due to orthonormality the coefficient matrix is always skew-symmetric. Thus it generally has three nonzero entries. The Frenet frame gains part of its special significance from the fact that one of the three derivatives is always zero. Another feature of the Frenet frame is that it is *adapted* to the curve: the members are either tangent to or perpendicular to the curve. It is the purpose of this paper to show that there are other frames which have these same advantages and to compare them with the Frenet frame.



**Relatively parallel fields.** We say that a normal vector field  $M$  along a curve is *relatively parallel* if its derivative is tangential. Such a field turns only whatever is necessary for it to remain normal, so it is as close to being parallel as possible without losing normality. Since its derivative is perpendicular to it, a relatively parallel normal field (couldn't decide on a meme) fields occur classically in



# Bishop Frame

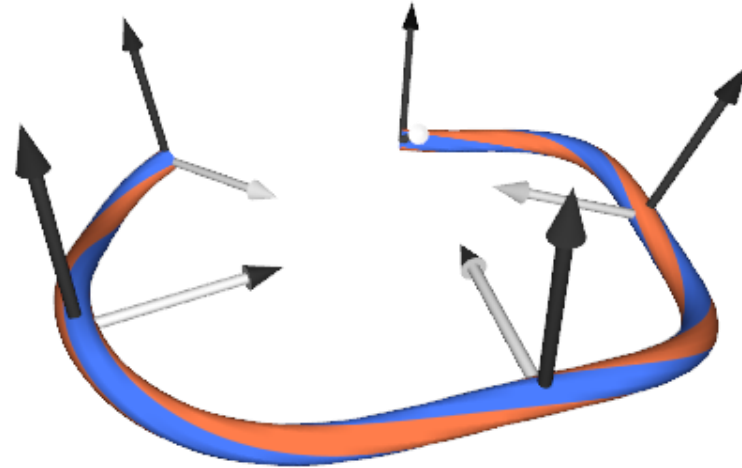
$$\mathbf{T}' = \boldsymbol{\Omega} \times \mathbf{T}$$

$$\mathbf{u}' = \boldsymbol{\Omega} \times \mathbf{u}$$

$$\mathbf{v}' = \boldsymbol{\Omega} \times \mathbf{v}$$

$$\boldsymbol{\Omega} := \kappa \mathbf{B} \text{ (“curvature binormal”)}$$

**Darboux vector**



**Most relaxed frame**

# Bishop Frame

$$\mathbf{T}' = \Omega \times \mathbf{T}$$

$$\mathbf{u}' = \Omega \times \mathbf{u}$$

$$\mathbf{v}' = \Omega \times \mathbf{v}$$

$$\mathbf{u}' \cdot \mathbf{v} \equiv 0$$

No twist  
("parallel transport")

$$\Omega := \kappa \mathbf{B} \text{ ("curvature binormal")}$$

Darboux vector

Most relaxed frame

# Curve-Angle Representation

$$\mathbf{m}_1 = \mathbf{u} \cos \theta + \mathbf{v} \sin \theta$$

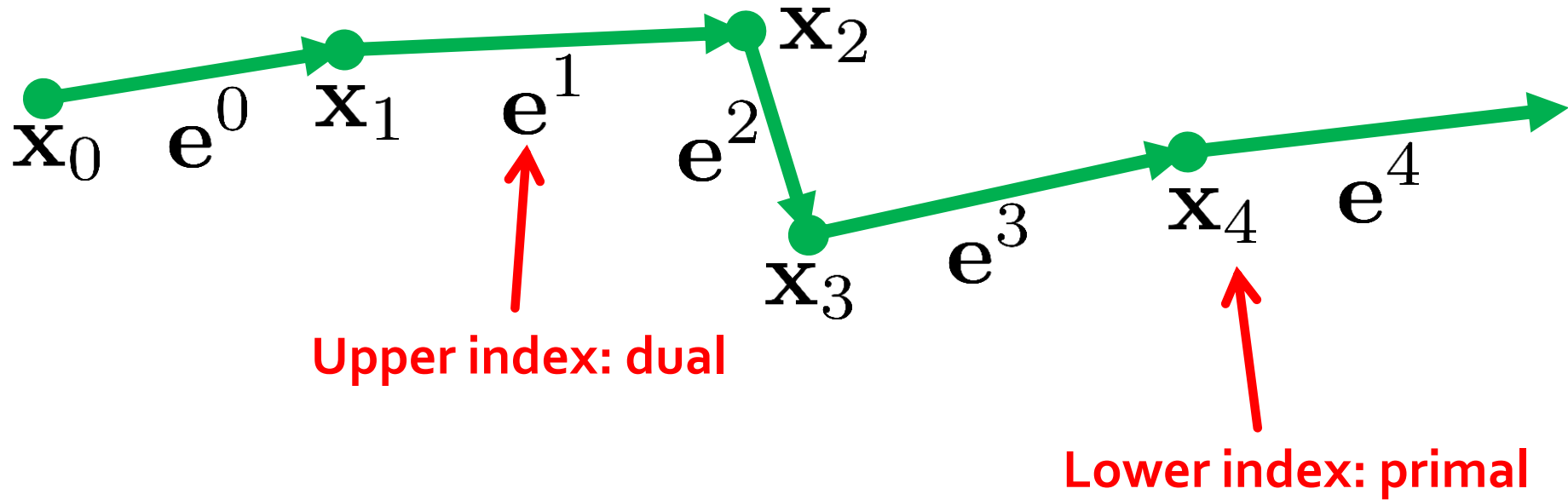
$$\mathbf{m}_2 = -\mathbf{u} \sin \theta + \mathbf{v} \cos \theta$$

$$E_{\text{twist}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \beta(\theta')^2 ds$$

**Degrees of freedom for elastic energy:**

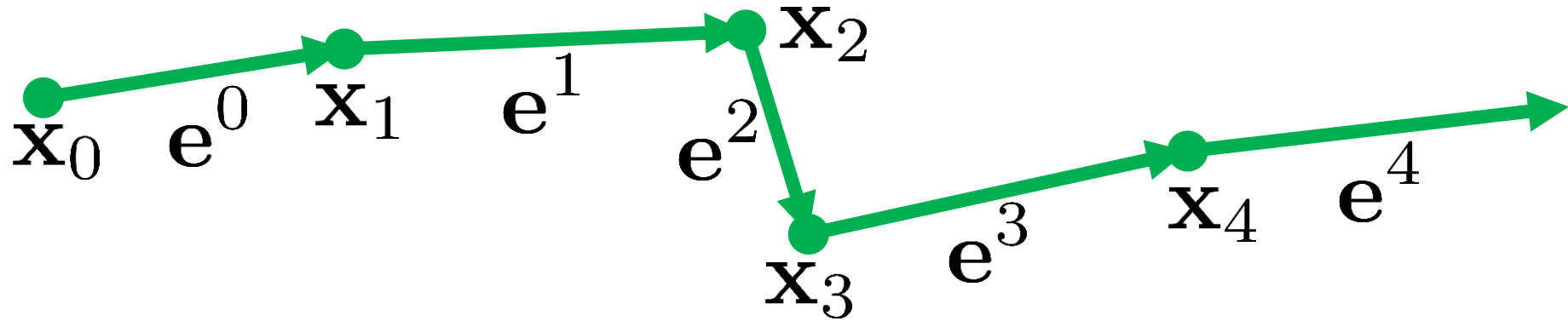
- Shape of curve
- Twist angle  $\theta$

# Discrete Kirchhoff Rods





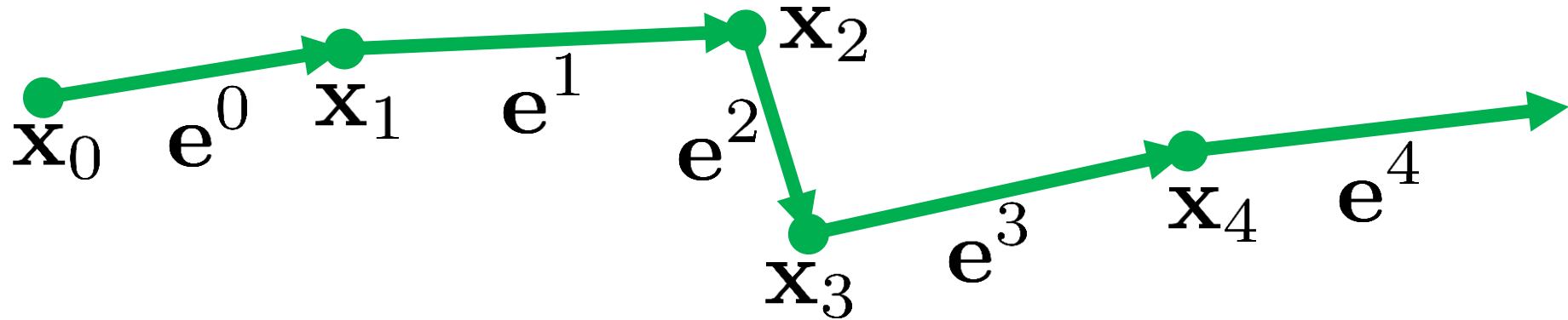
# Discrete Kirchhoff Rods



$$\mathbf{T}^i := \frac{\mathbf{e}^i}{\|\mathbf{e}^i\|_2}$$

Tangent unambiguous on edge

# Discrete Kirchhoff Rods



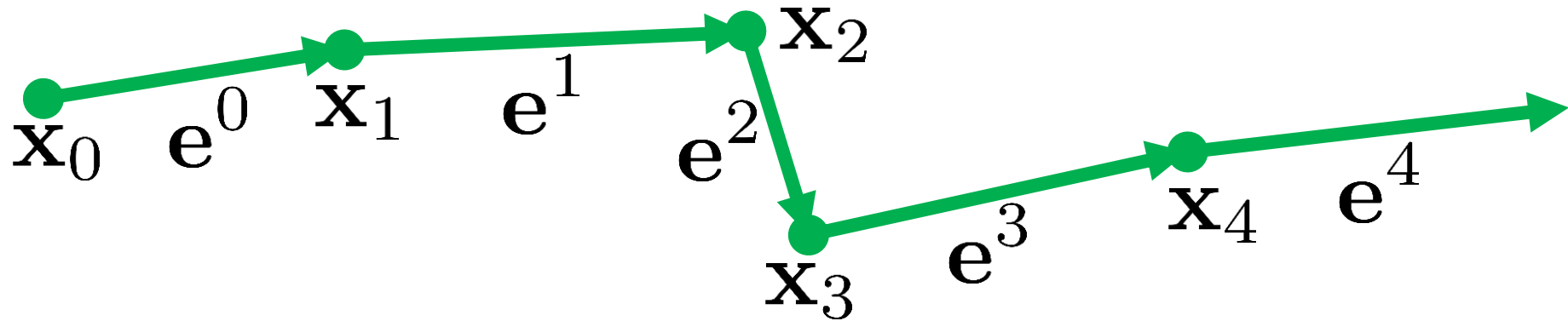
$$\kappa_i := 2 \tan \frac{\phi_i}{2}$$

Turning angle

Yet another curvature!

Integrated curvature

# Discrete Kirchhoff Rods



$$\kappa_i := 2 \tan \frac{\phi_i}{2}$$

Yet another curvature!

$$(\kappa \mathbf{B})_i := \frac{2\mathbf{e}^{i-1} \times \mathbf{e}^i}{\|\mathbf{e}^{i-1}\|_2 \|\mathbf{e}^i\|_2 + \mathbf{e}^{i-1} \cdot \mathbf{e}^i}$$

Orthogonal to osculating plane,  
norm  $\kappa_i$

**Darboux vector**

# Bending Energy

$$\begin{aligned} E_{\text{bend}}(\Gamma) &:= \frac{\alpha}{2} \sum_i \left( \frac{(\kappa \mathbf{B})_i}{\ell_i/2} \right)^2 \frac{\ell_i}{2} \\ &= \alpha \sum_i \frac{\|(\kappa \mathbf{B})_i\|_2^2}{\ell_i} \end{aligned}$$

Convert to pointwise and integrate

# Discrete Parallel Transport

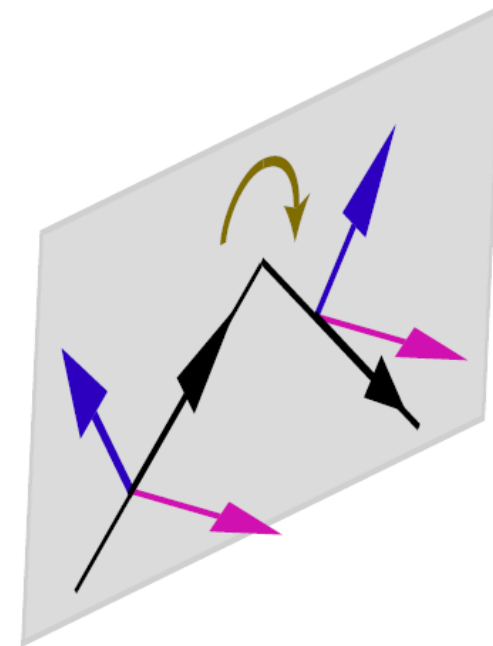
$$P_i(\mathbf{T}^{i-1}) = \mathbf{T}^i$$

$$P_i(\mathbf{T}^{i-1} \times \mathbf{T}^i) = \mathbf{T}^{i-1} \times \mathbf{T}^i$$

- Map tangent to tangent
- Preserve binormal
- Orthogonal

$$\mathbf{u}^i = P_i(\mathbf{u}^{i-1})$$

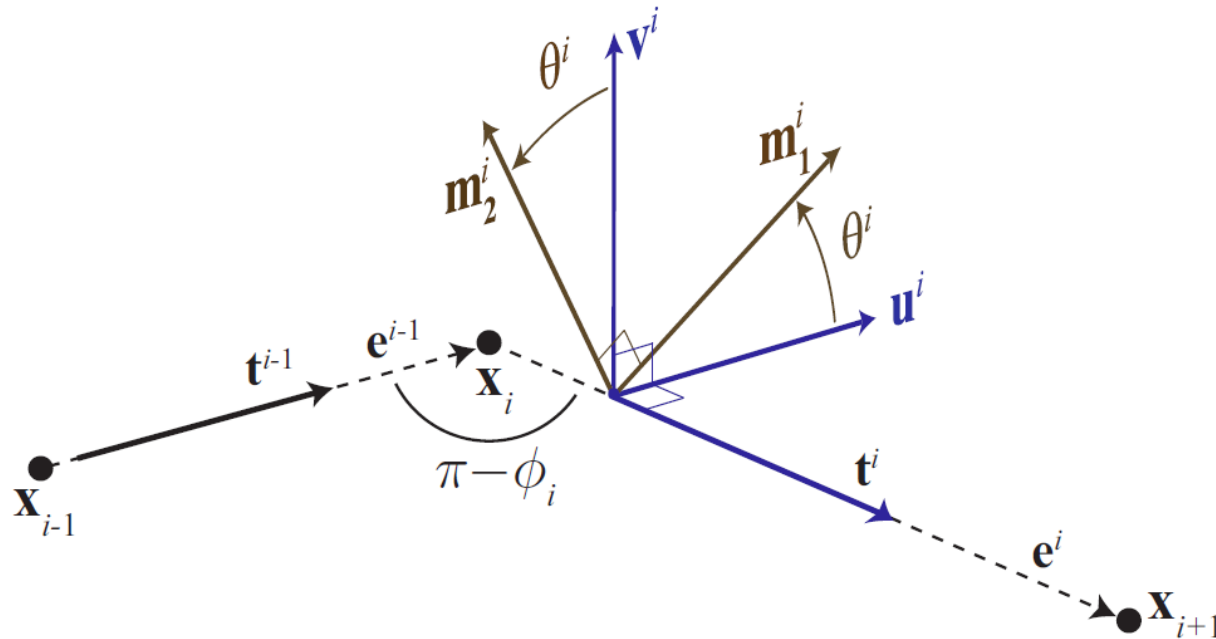
$$\mathbf{v}^i = \mathbf{T}^i \times \mathbf{u}^i$$




# Discrete Material Frame

$$\mathbf{m}_1^i = \mathbf{u}^i \cos \theta^i + \mathbf{v}^i \sin \theta^i$$

$$\mathbf{m}_2^i = -\mathbf{u}^i \sin \theta^i + \mathbf{v}^i \cos \theta^i$$



# Discrete Twisting Energy

$$E_{\text{twist}}(\Gamma) := \beta \sum_i \frac{(\theta^i - \theta^{i-1})^2}{\ell_i}$$


Note  $\theta_0$  can be arbitrary

# Simulation

`\omit{physics}`

*Worth reading!*



# Extension and Speedup

## Discrete Viscous Threads

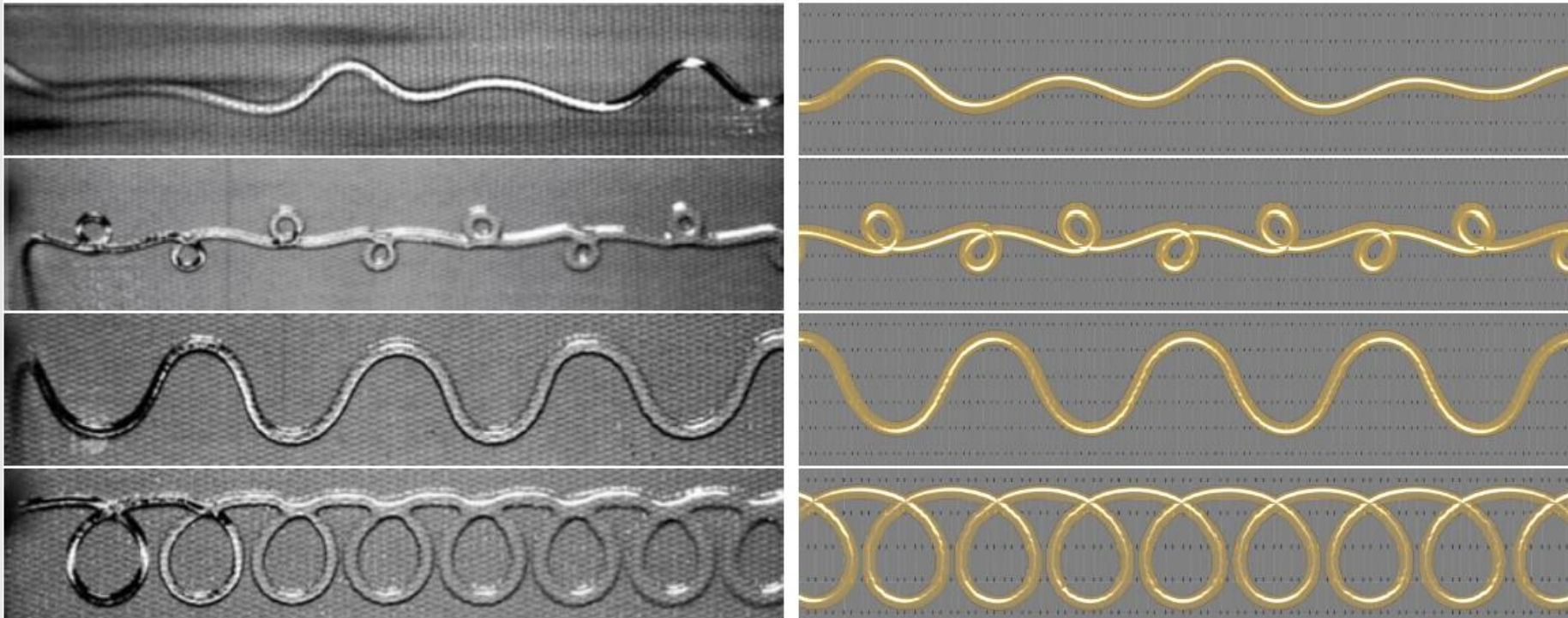
Miklós Bergou  
Columbia University

Basile Audoly  
UPMC Univ. Paris 06 & CNRS

Etienne Vouga  
Columbia University

Max Wardetzky  
Universität Göttingen

Eitan Grinspun  
Columbia University



# Extension and Speedup

## Discrete Viscous Threads

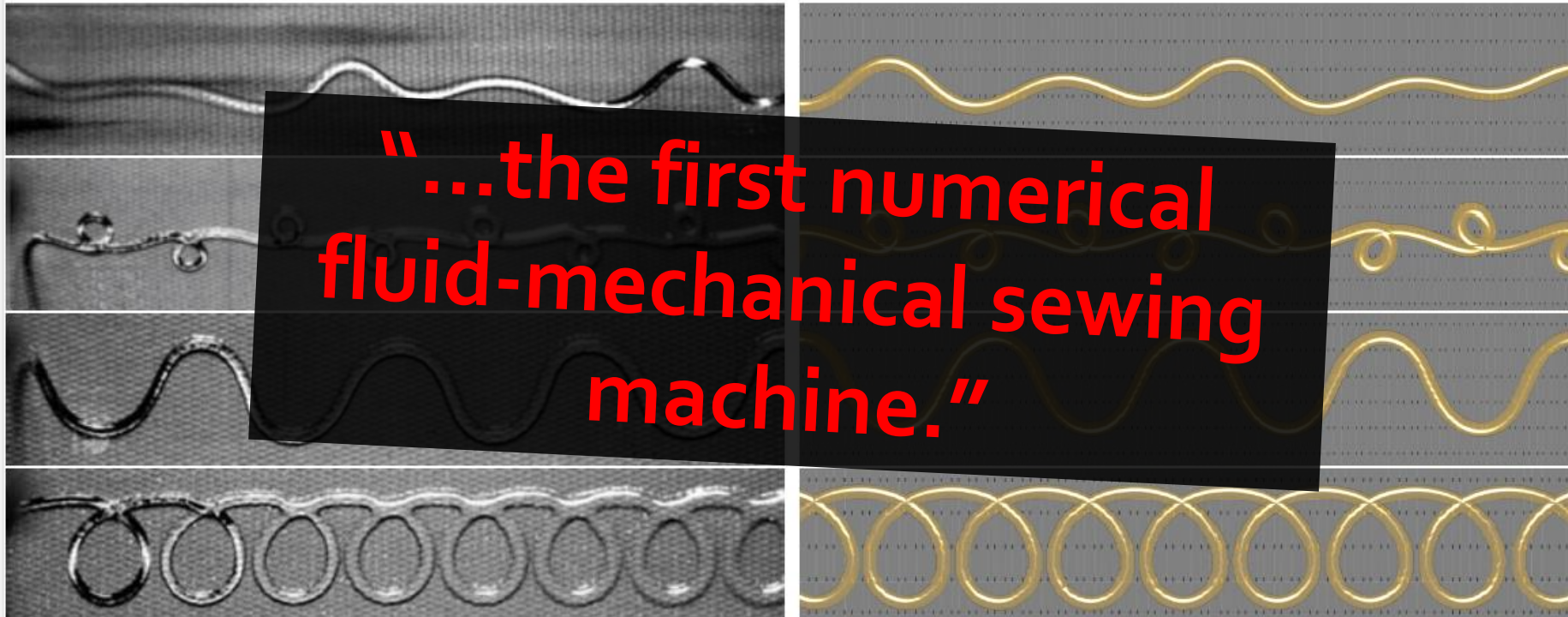
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Columbia University



# Morals

One curve,  
three curvatures.

$$\theta$$

$$2 \sin \frac{\theta}{2}$$

$$2 \tan \frac{\theta}{2}$$

# Morals

**Easy theoretical object,  
hard to use.**

$$\frac{d}{ds} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix} = \begin{pmatrix} 0 & \kappa(s) & 0 \\ -\kappa(s) & 0 & \tau(s) \\ 0 & -\tau(s) & 0 \end{pmatrix} \begin{pmatrix} \mathbf{T}(s) \\ \mathbf{N}(s) \\ \mathbf{B}(s) \end{pmatrix}$$

# Morals

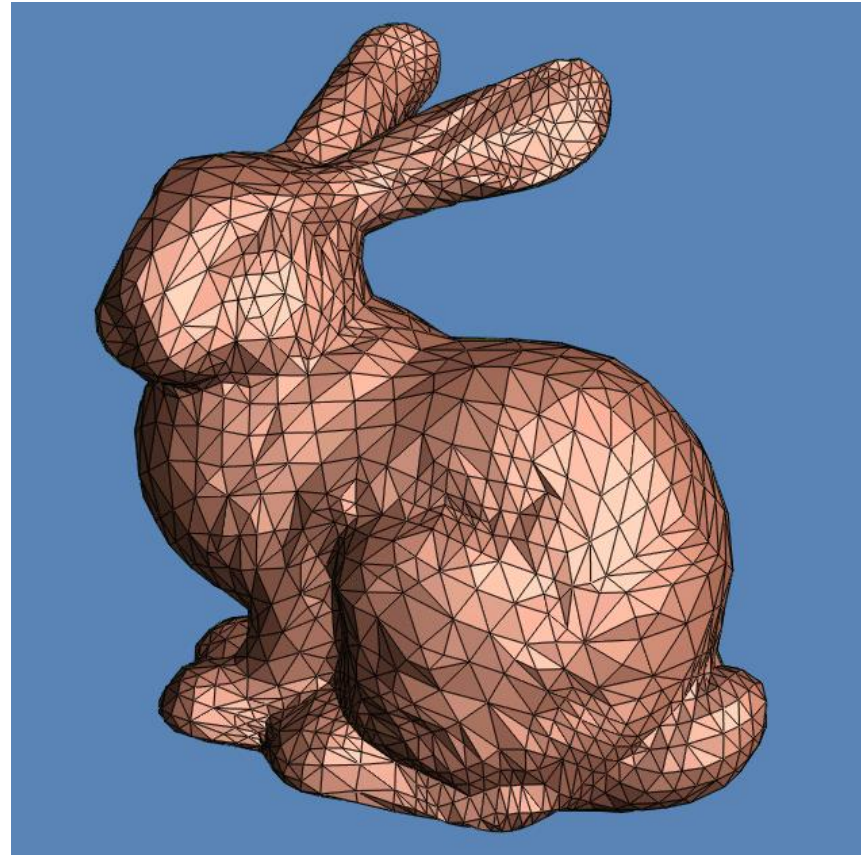
Proper frames and DOFs  
go a long way.

$$\mathbf{m}_1^i = \mathbf{u}^i \cos \theta^i + \mathbf{v}^i \sin \theta^i$$

$$\mathbf{m}_2^i = -\mathbf{u}^i \sin \theta^i + \mathbf{v}^i \cos \theta^i$$



# Next



<http://graphics.stanford.edu/data/3Dscanrep/stanford-bunny-cebal-ssh.jpg>  
<http://www.stat.washington.edu/wxs/images/BUNMID.gif>

# Surfaces

# Discrete Curves

Justin Solomon

6.838: Shape Analysis

Spring 2021

