



# Curves: Continuous and Discrete

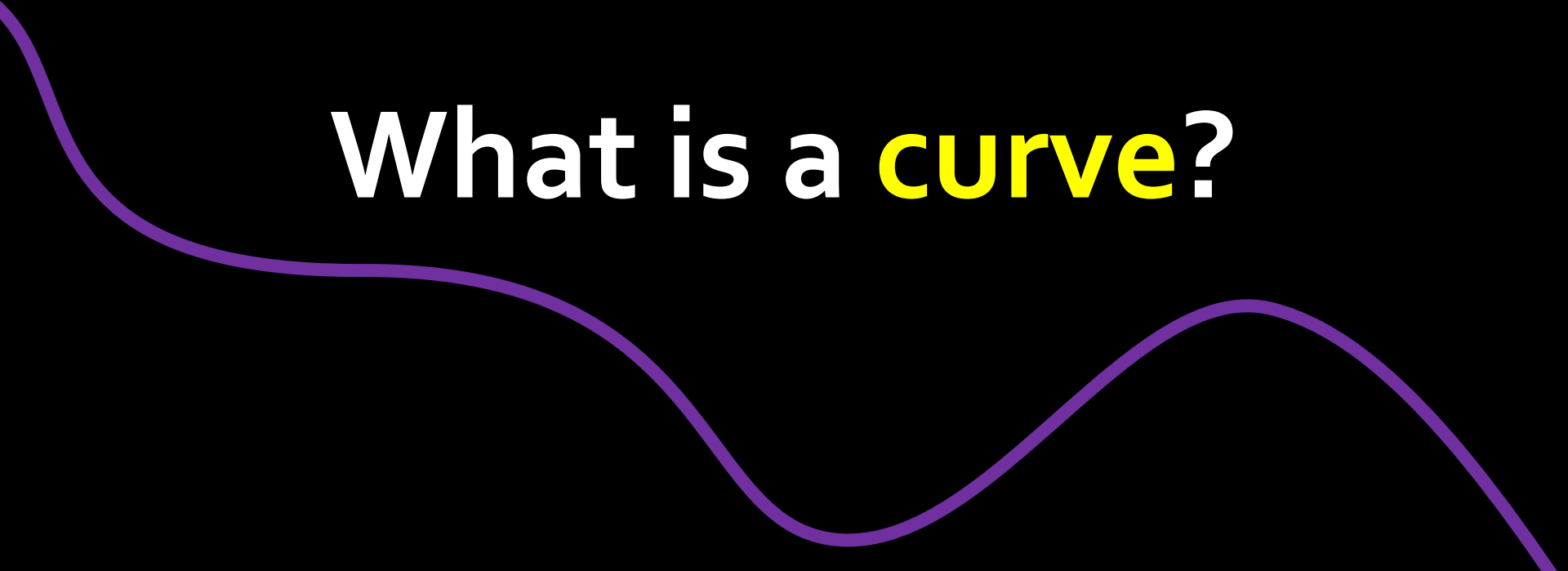
Justin Solomon

MIT, Spring 2017

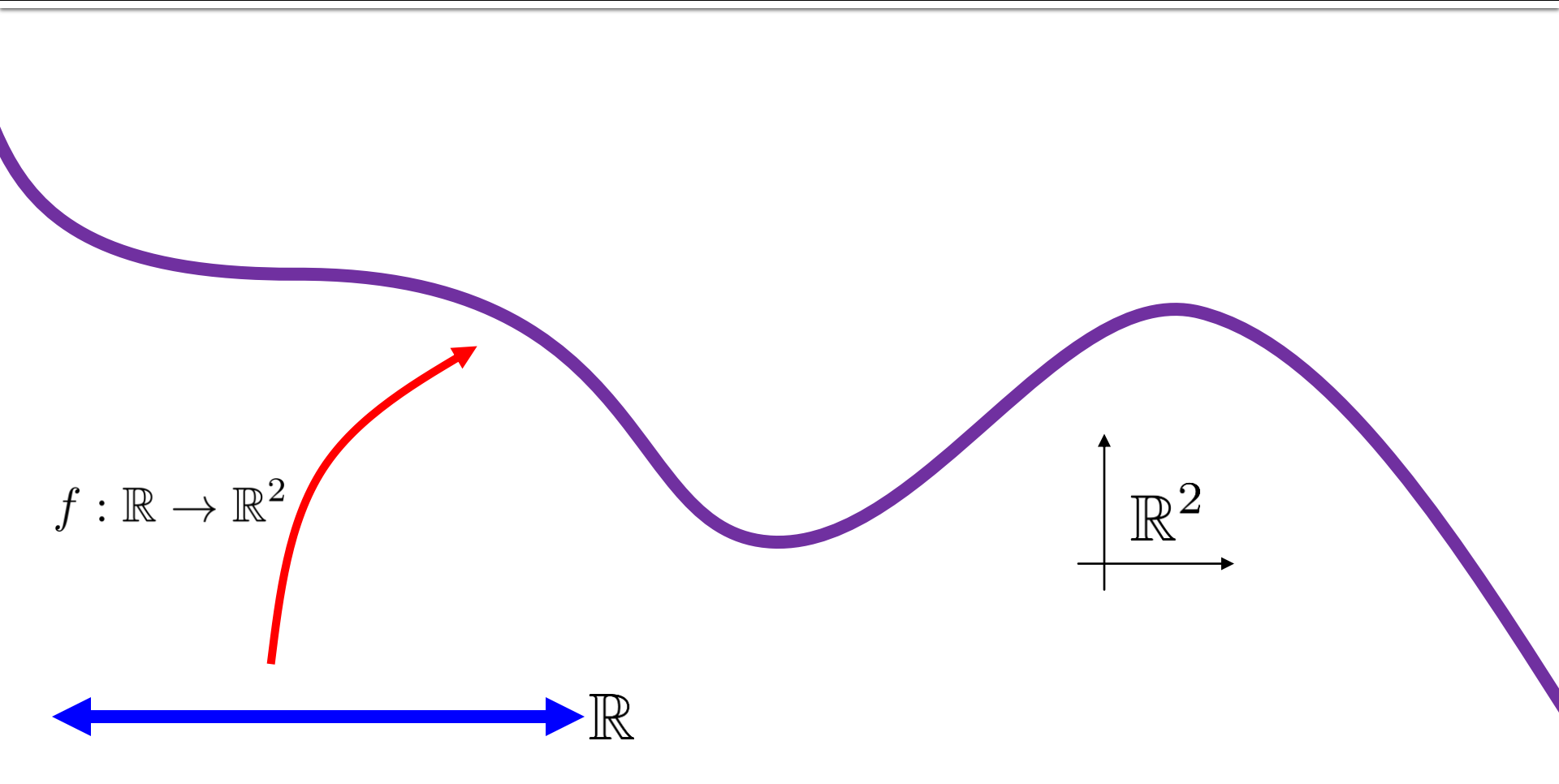




What is a **curve**?



# Defining "Curve"



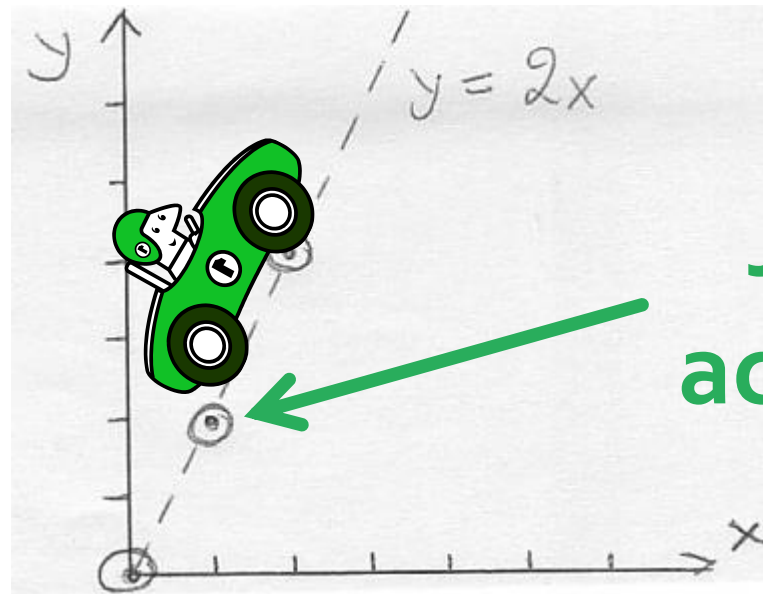
**A function?**

# Subtlety

$$\gamma_3(t) := (0, 0)$$

**Not a curve**

# Different from Calculus

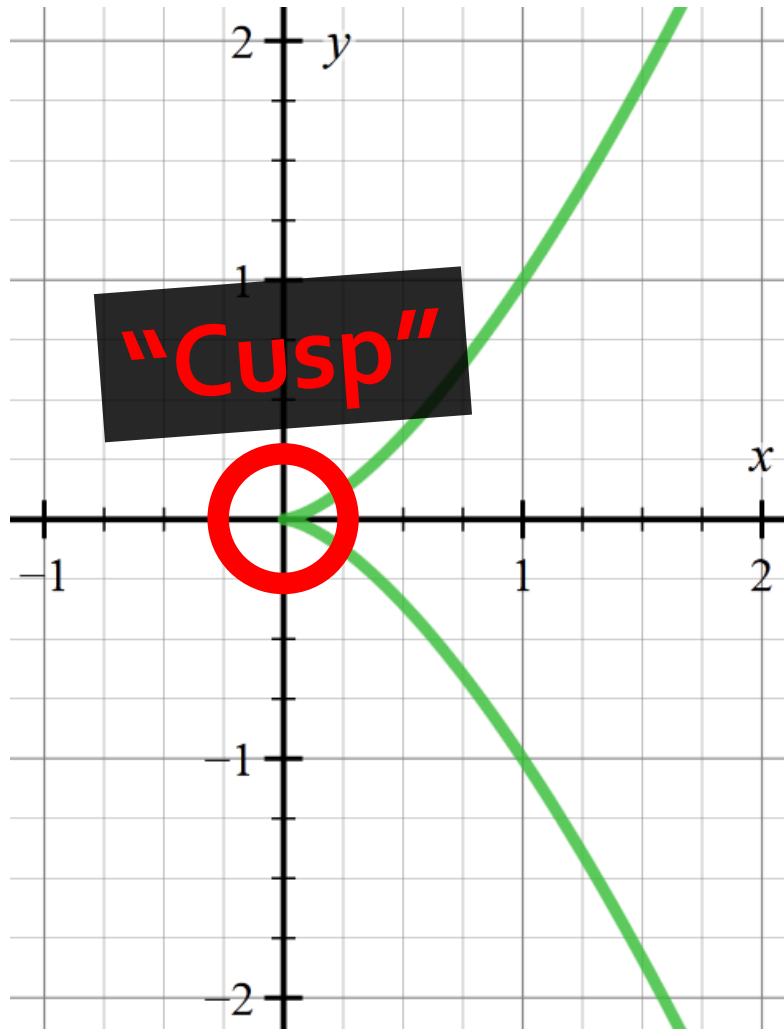


Jams on  
accelerator

$$f_1(t) = (t, 2t)$$

$$f_2(t) = \begin{cases} (t, 2t) & t \leq 1 \\ (2(t - \frac{1}{2}), 4(t - \frac{1}{2})) & t > 1 \end{cases}$$

# Graphs of Smooth Functions



$$f(t) = (t^2, t^3)$$

# Geometry of a Curve

A curve is a  
**set of points**  
with certain properties.

It is not a function.

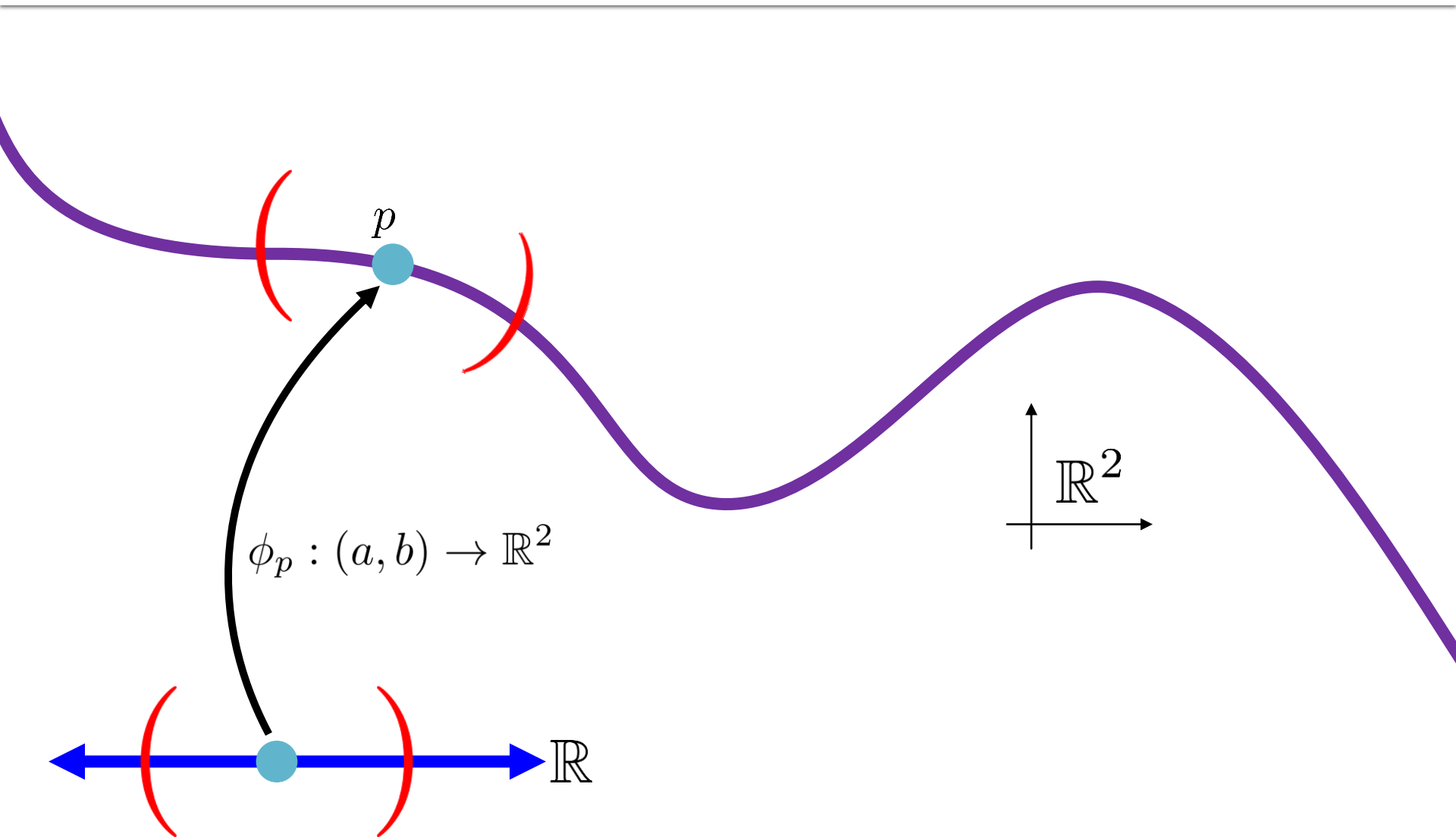
# Geometric Definition



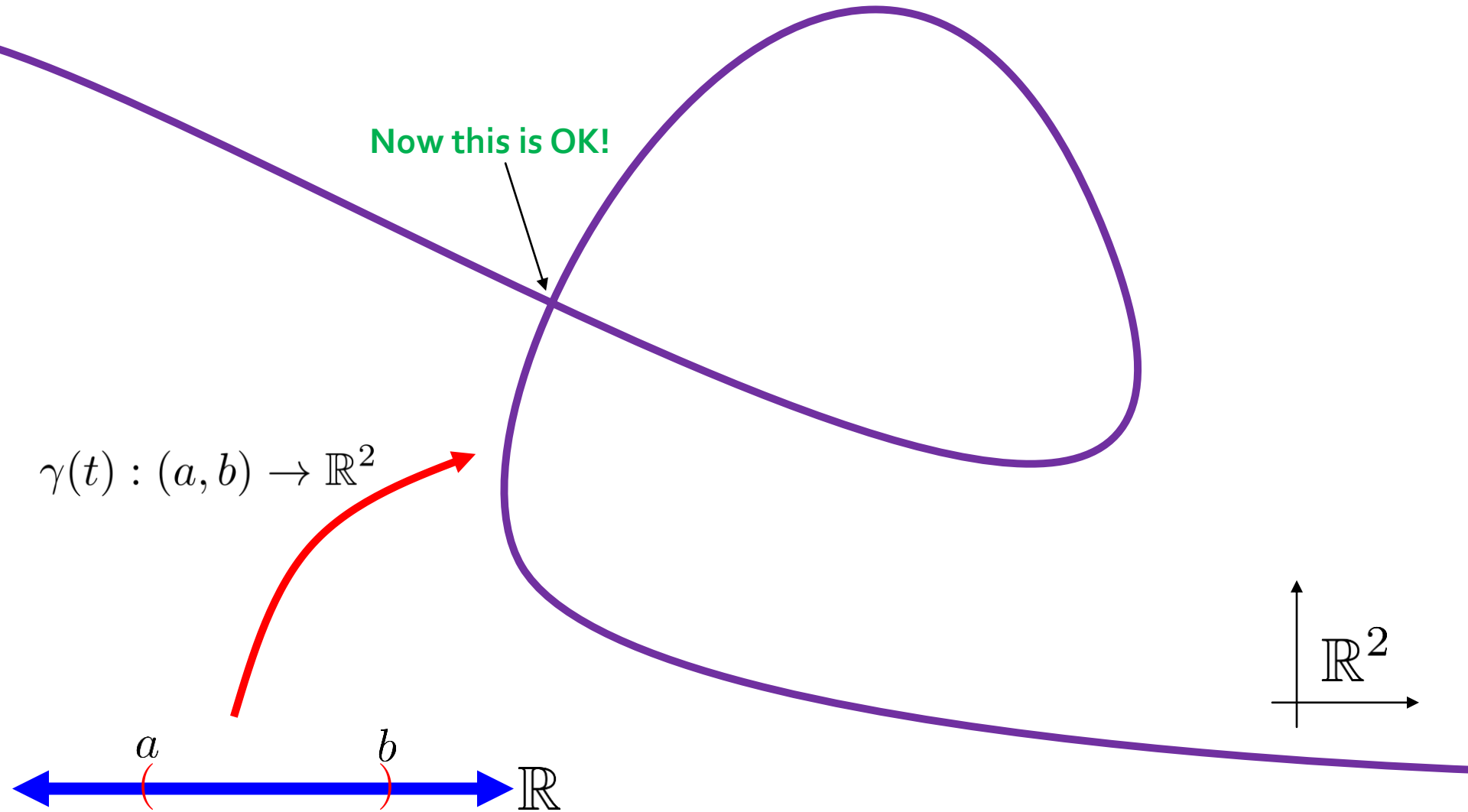
Set of points that locally looks like a line.



# Differential Geometry Definition



# Parameterized Curve



# Some Vocabulary

- **Trace** of parameterized curve

$$\{\gamma(t) : t \in (a, b)\}$$

- **Component** functions

$$\gamma(t) = (x(t), y(t), z(t))$$

# Change of Parameter

$$\bar{t} \mapsto \gamma(g(\bar{t})) = \gamma \circ g(\bar{t})$$

Geometric measurements should be  
**invariant**  
to changes of parameter.



# Dependence of Velocity

$$\tilde{\gamma}(s) := \gamma(\phi(s))$$

*On the board:*

Effect on velocity and acceleration.

# Arc Length

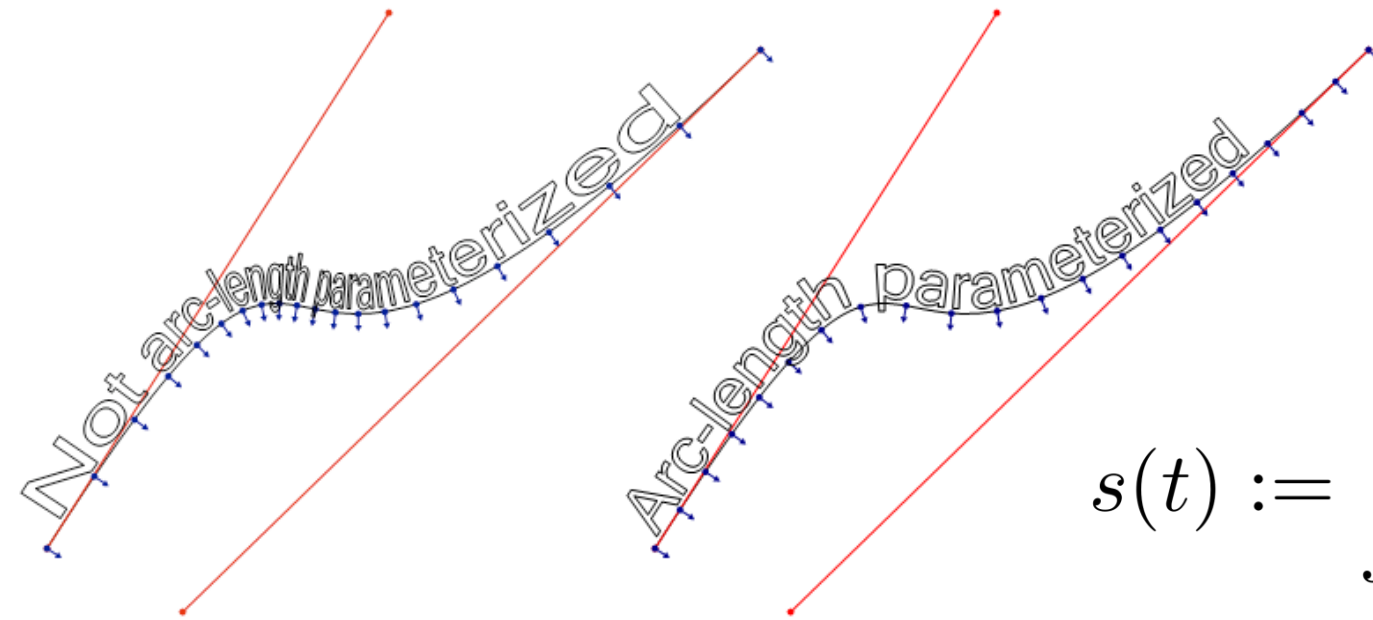
$$\int_a^b \|\gamma'(t)\| dt$$

*On the board:*

Independence of parameter

# Parameterization by Arc Length

<http://www.planetclegg.com/projects/WarpingTextToSplines.html>



$$s(t) := \int_{t_0}^t \|\gamma'(t)\| dt$$

$$t(s) := \text{inverse of } s(t)$$

$$\gamma(s) := \gamma(s(t))$$

**Constant-speed parameterization**

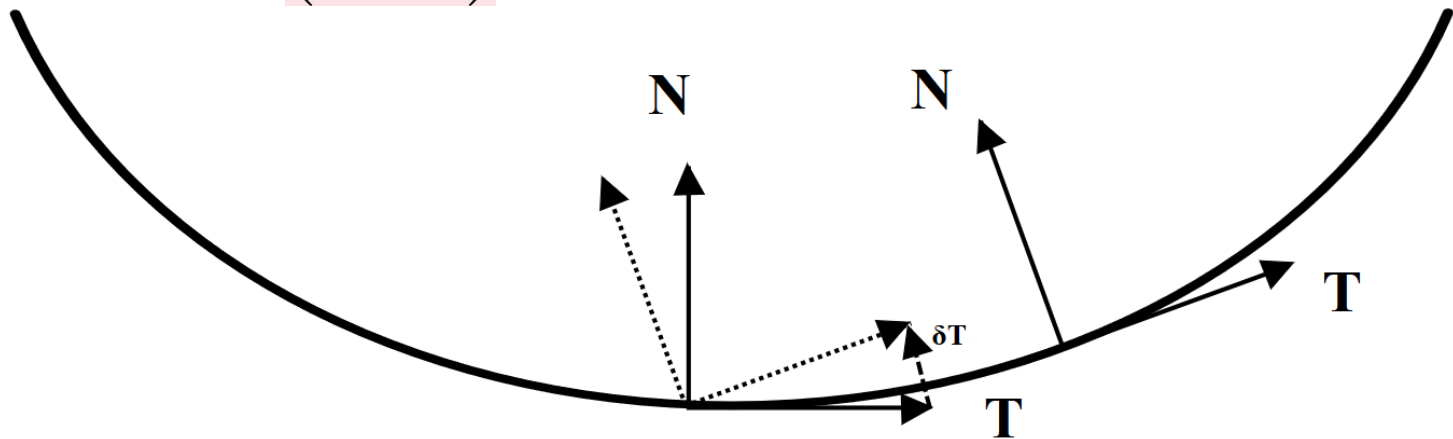
# Moving Frame in 2D

$$T(s) := \gamma'(s)$$

$$\implies \text{(on board)} \quad \|T(s)\| \equiv 1$$

$$N(s) := JT(s)$$

$$\begin{pmatrix} 0 & -1 \\ 1 & 0 \end{pmatrix}$$





# Philosophical Point

Differential geometry “should” be  
**coordinate-invariant.**

Referring to  $x$  and  $y$  is a hack!  
*(but sometimes convenient...)*

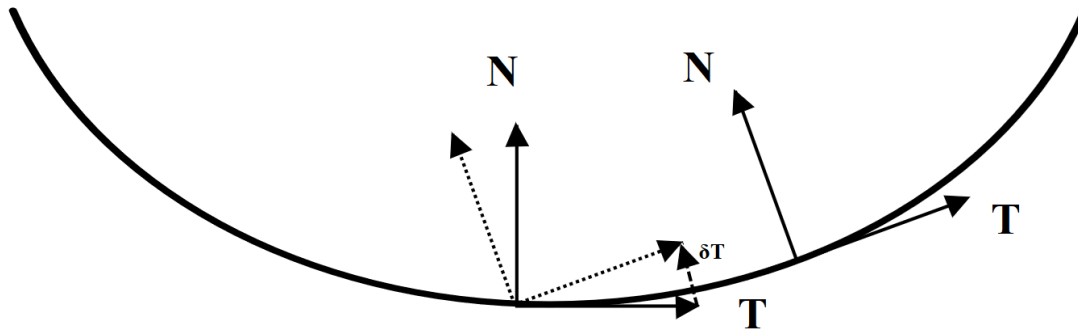


How do you  
characterize shape  
**without coordinates?**

# Turtles All The Way Down

On the board:

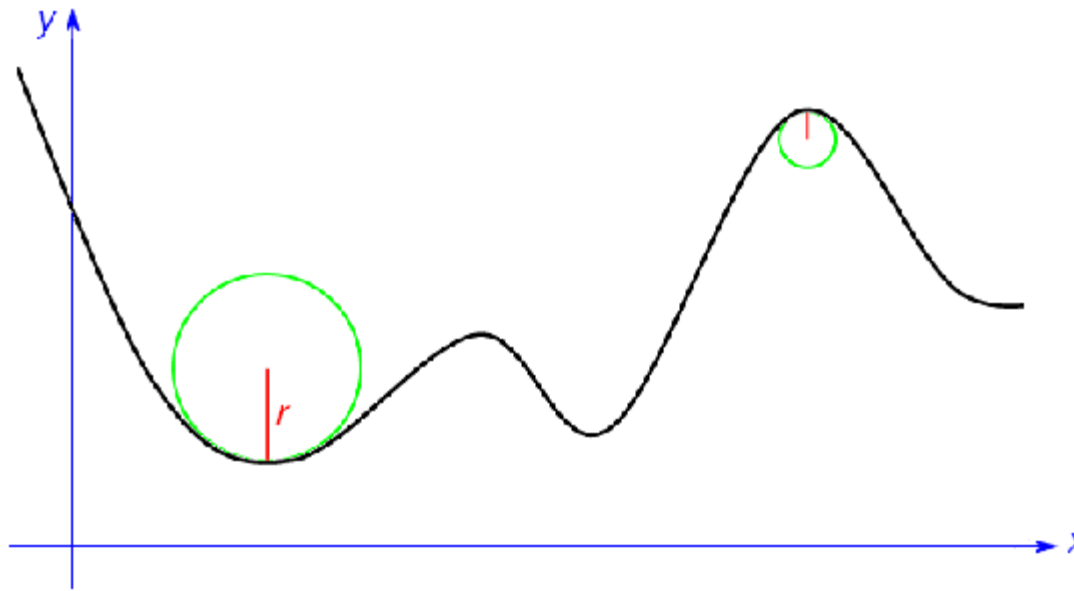
$$\frac{d}{ds} \begin{pmatrix} T(s) \\ N(s) \end{pmatrix} := \begin{pmatrix} 0 & k(s) \\ -k(s) & 0 \end{pmatrix} \begin{pmatrix} T(s) \\ N(s) \end{pmatrix}$$



[https://en.wikipedia.org/wiki/Frenet%E2%80%93Serret\\_formulas](https://en.wikipedia.org/wiki/Frenet%E2%80%93Serret_formulas)

Use coordinates *from* the curve to  
express its shape!

# Radius of Curvature



$$r(s) := \frac{1}{\kappa(s)}$$

# Fundamental theorem of the local theory of plane curves:

$k(s)$  characterizes a planar curve up to rigid motion.

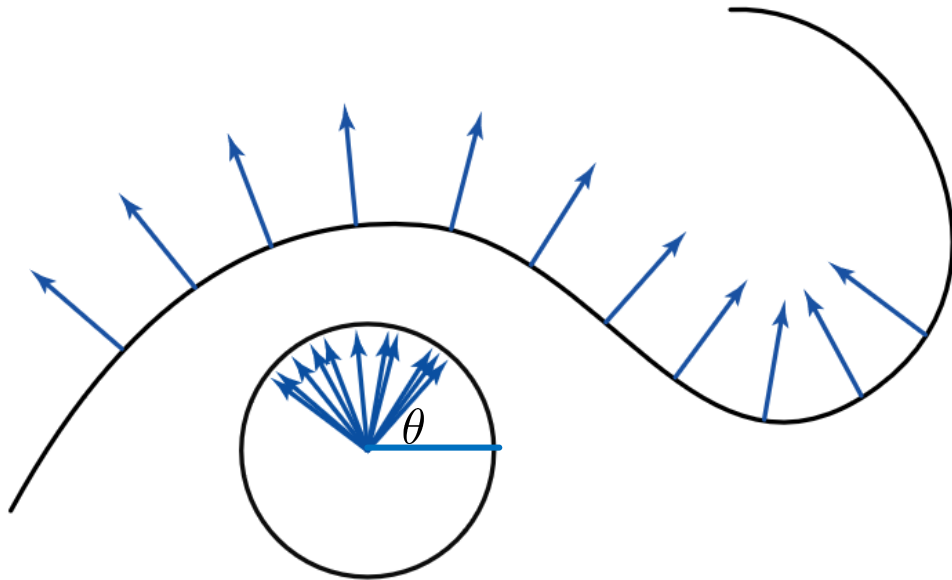
# Fundamental theorem of the local theory of plane curves:

$k(s)$  characterizes a planar curve up to rigid motion.



*Statement shorter than the name!*

# Idea of Proof



$$T(s) := (\cos \theta(s), \sin \theta(s))$$
$$\implies k(s) := \theta'(s)$$

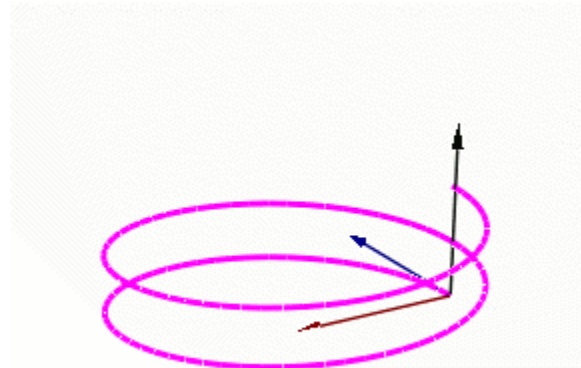
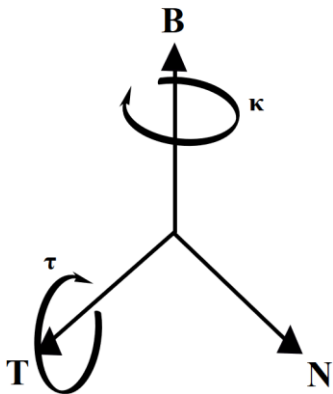
Image from DDG course notes by E. Grinspun

**Provides intuition for curvature**

# Frenet Frame: Curves in $\mathbb{R}^3$

$$\frac{d}{ds} \begin{pmatrix} T \\ N \\ B \end{pmatrix} = \begin{pmatrix} 0 & \kappa & 0 \\ -\kappa & 0 & \tau \\ 0 & -\tau & 0 \end{pmatrix} \begin{pmatrix} T \\ N \\ B \end{pmatrix}$$

- **Binormal:**  $T \times N$
- **Curvature:** In-plane motion
- **Torsion:** Out-of-plane motion





# **Fundamental theorem of the local theory of space curves:**

**Curvature and torsion  
characterize a 3D curve up to  
rigid motion.**

# Aside: Generalized Frenet Frame

$$\gamma(s) : \mathbb{R} \rightarrow \mathbb{R}^n$$

$$\frac{d}{ds} \begin{pmatrix} e_1(s) \\ e_2(s) \\ \vdots \\ e_n(s) \end{pmatrix} = \begin{pmatrix} 0 & \chi_1(s) & & 0 \\ -\chi_1(s) & \ddots & \ddots & \\ & \ddots & 0 & \chi_{n-1}(s) \\ 0 & & -\chi_{n-1}(s) & 0 \end{pmatrix} \begin{pmatrix} e_1(s) \\ e_2(s) \\ \vdots \\ e_n(s) \end{pmatrix}$$

*Suspicion: Application to time series analysis? ML?*

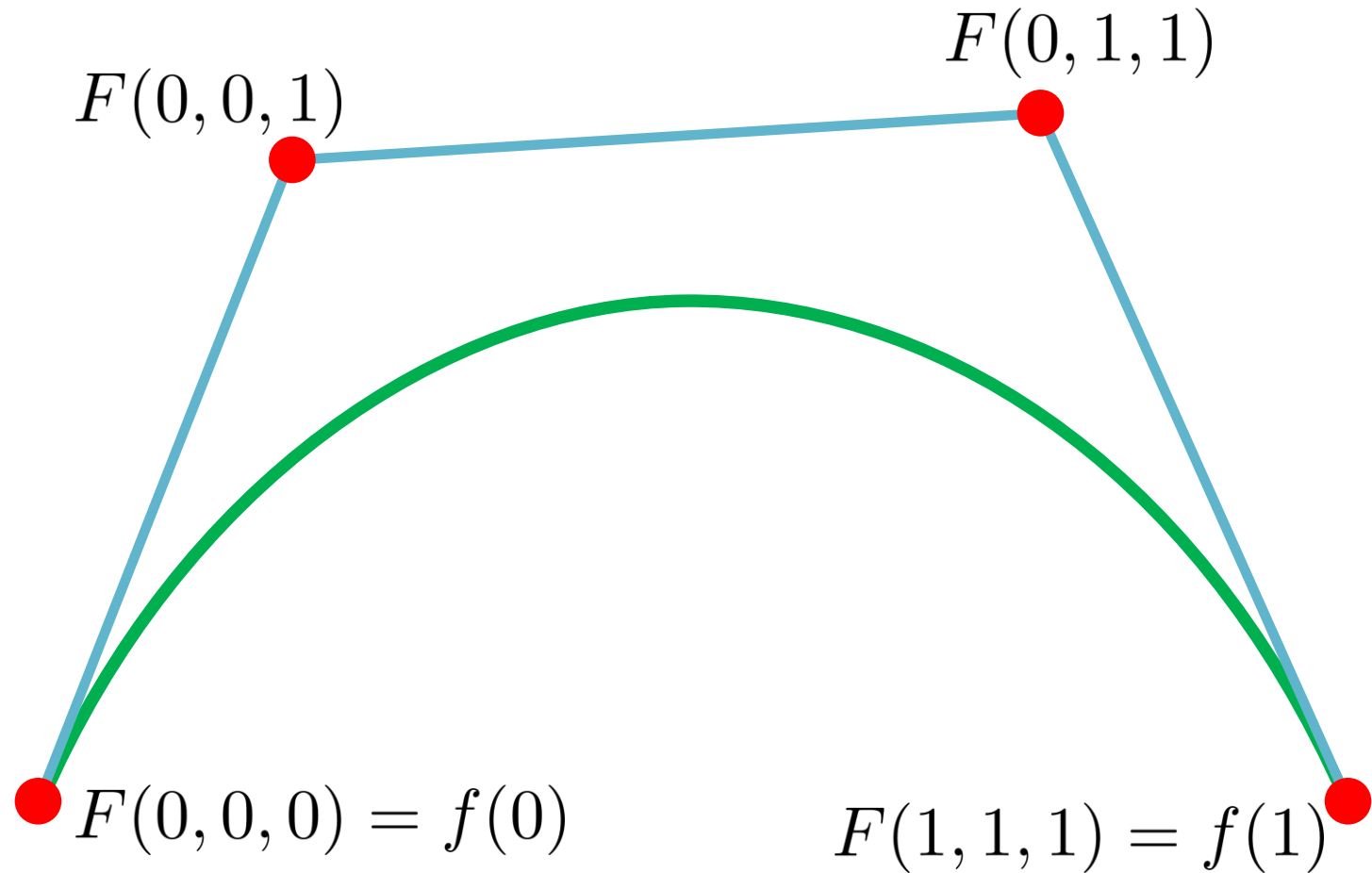
C. Jordan, 1874

**Gram-Schmidt on first  $n$  derivatives**



What do these  
calculations look like  
**in software?**

# Old-School Approach



**Piecewise smooth approximations**

# Question

What is the arc length of a cubic Bézier curve?

$$\int_a^b \|\gamma'(t)\| dt$$

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What is the arc length of a cubic Bézier curve?

$$\int_a^b \|\gamma'(t)\| dt$$

Not known in closed form.

*Sad fact:*

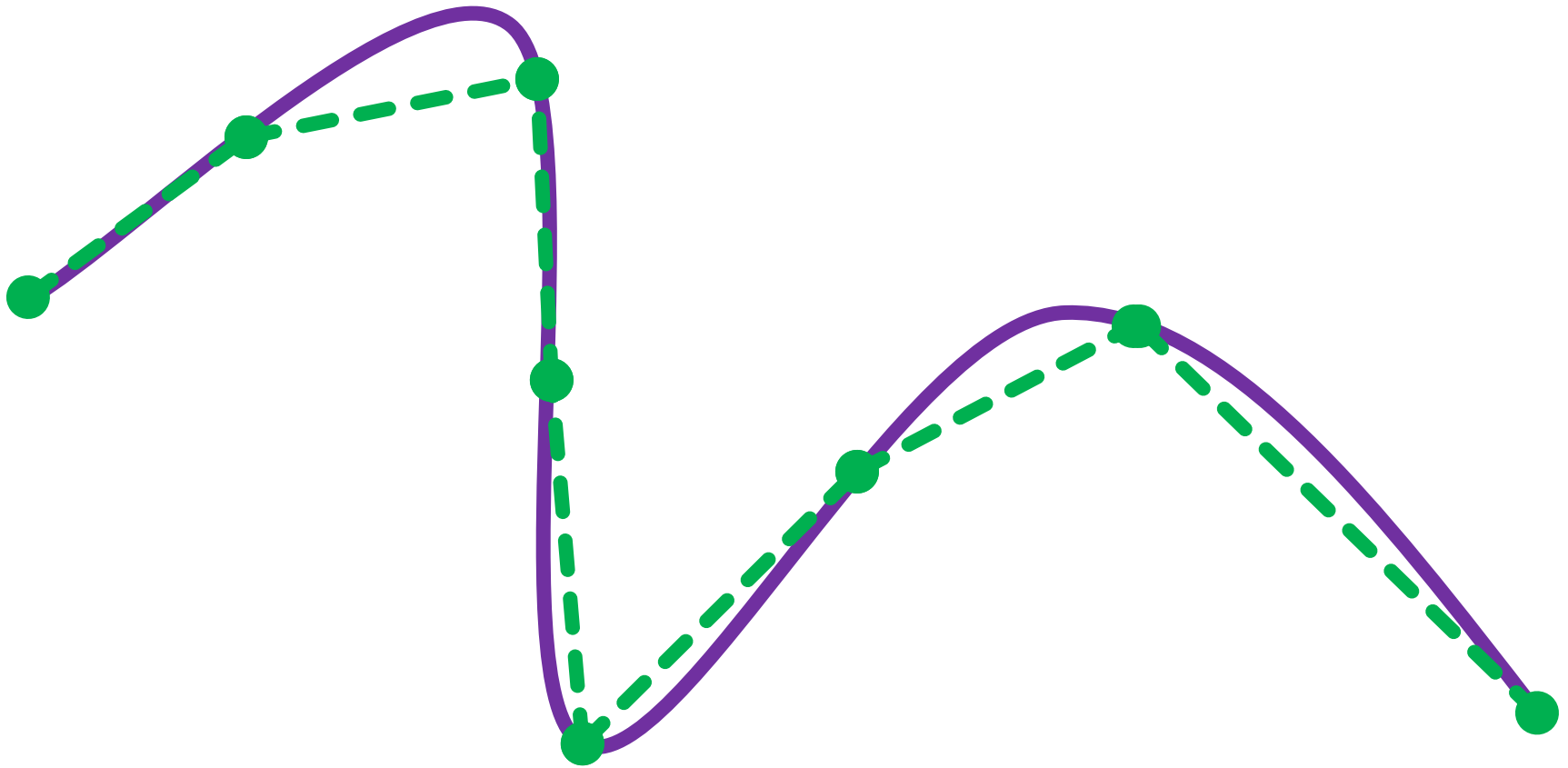
Closed-form  
expressions **rarely exist**.  
When they do exist, they  
usually are **messy**.

# Only Approximations Anyway

$$\{\text{Bézier curves}\} \subsetneq \{\gamma : \mathbb{R} \rightarrow \mathbb{R}^3\}$$

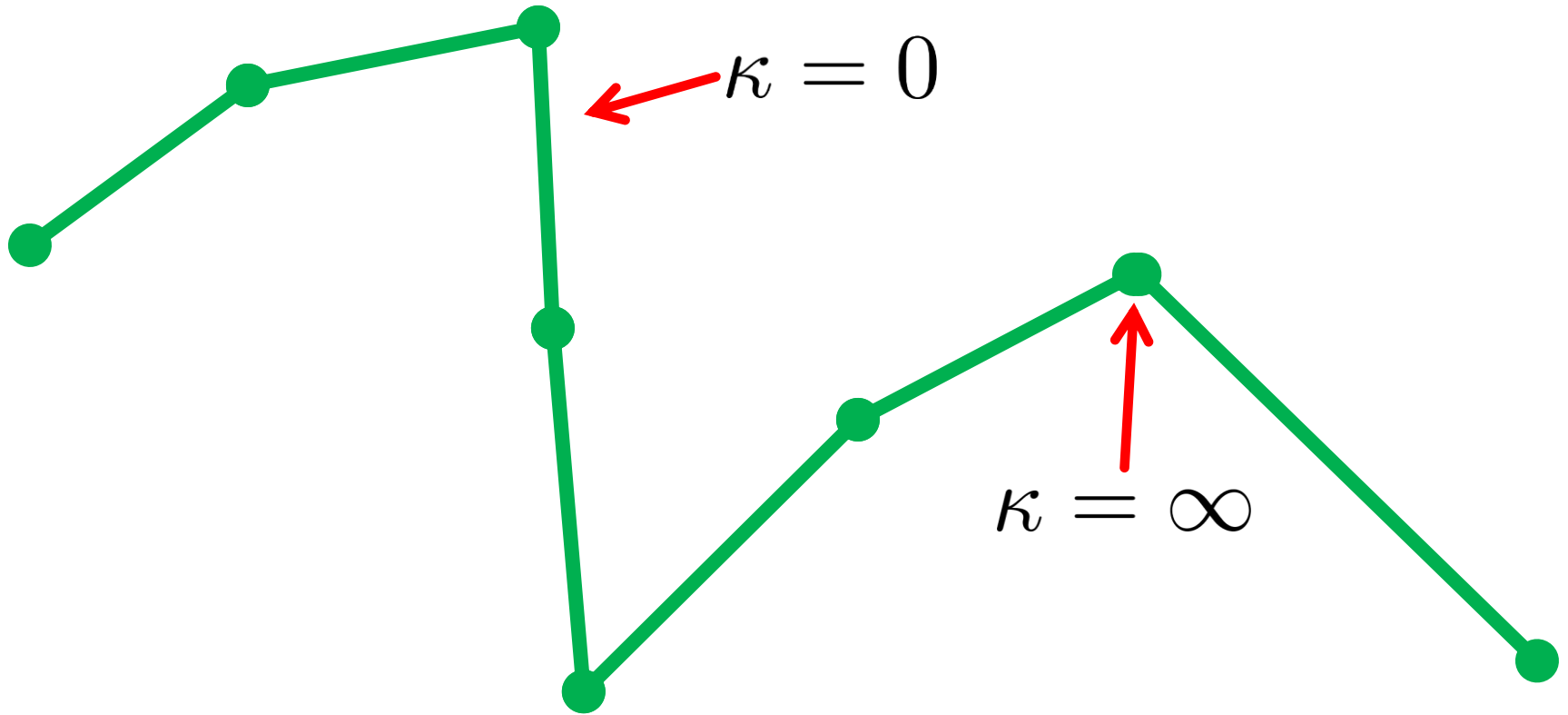


# Equally Reasonable Approximation



**Piecewise linear**

# Big Problem



**Boring differential structure**

# Finite Difference Approach

$$f'(x) \approx \frac{1}{h} [f(x+h) - f(x)]$$

**THEOREM: As  $\Delta h \rightarrow 0$ , [insert statement].**

# Reality Check

$$f'(x) \approx \frac{1}{h} [f(x+h) - f(x)]$$

THEOREM

$$h > 0$$

statement].

# Two Key Considerations

- **Convergence** to continuous theory
- **Discrete behavior**

# Goal

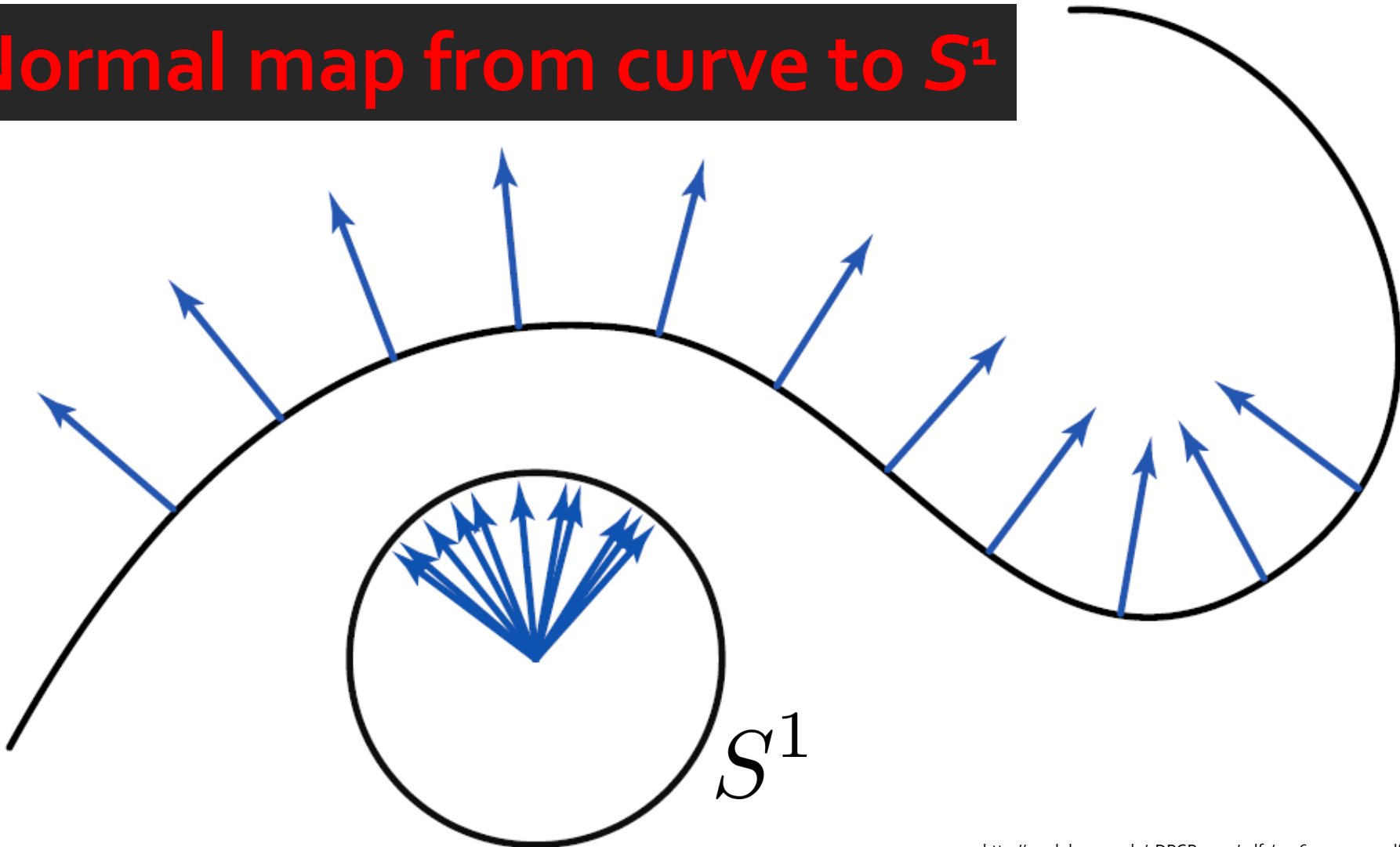
**Examine discrete theories  
of differentiable curves.**

# Goal

**Examine discrete theories  
of differentiable curves.**

# Gauss Map

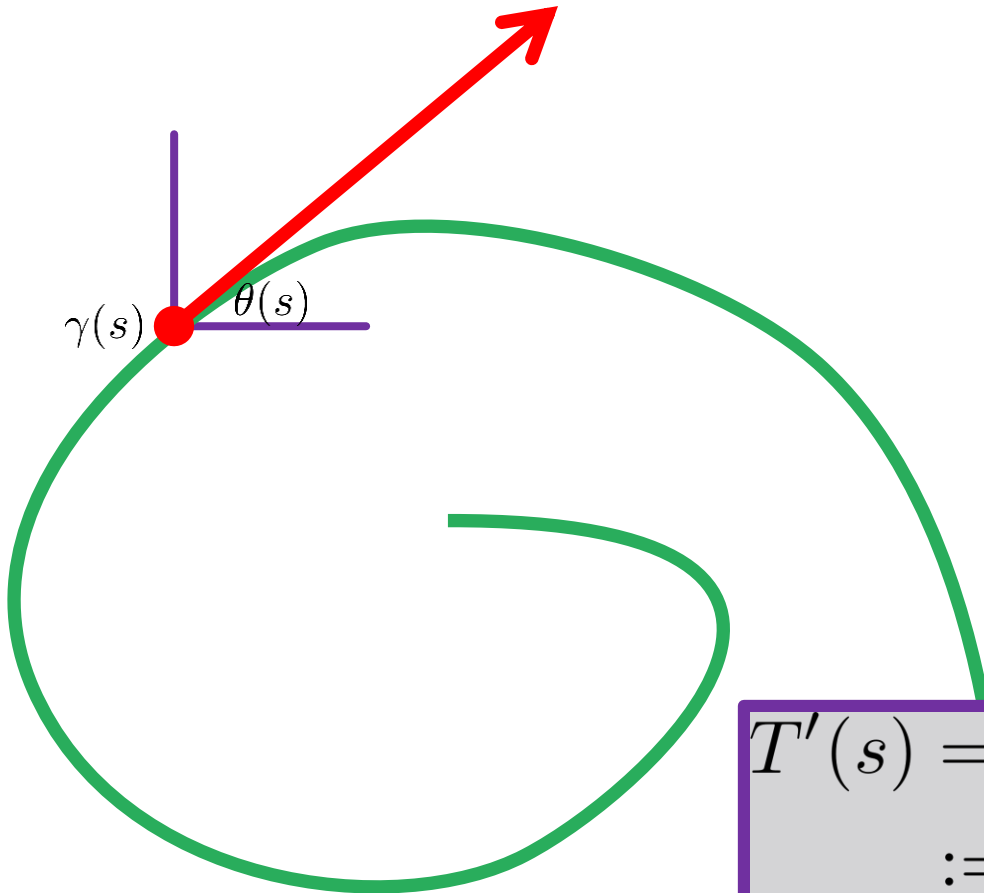
Normal map from curve to  $S^1$





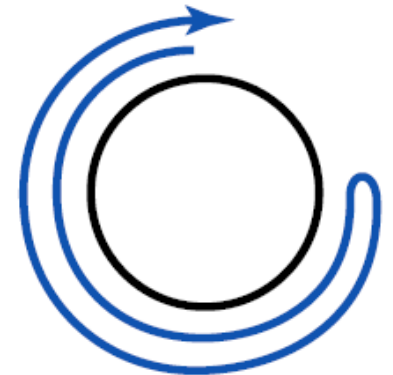
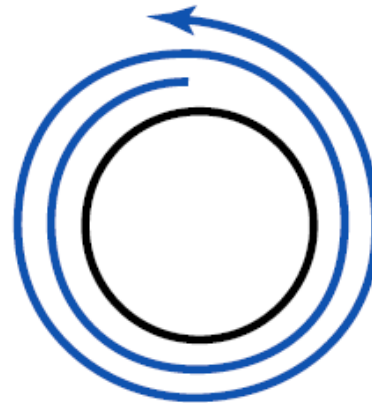
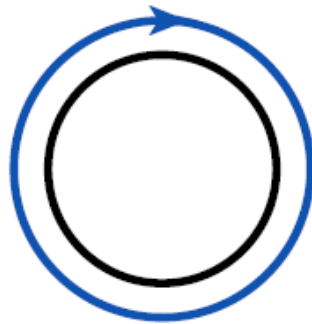
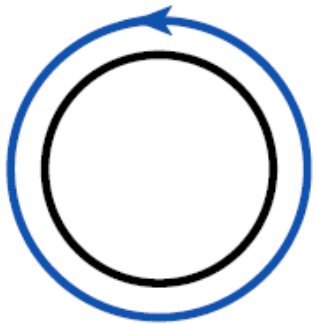
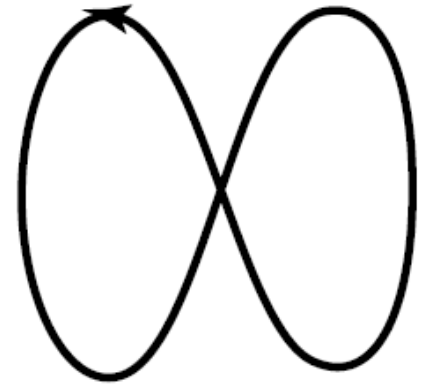
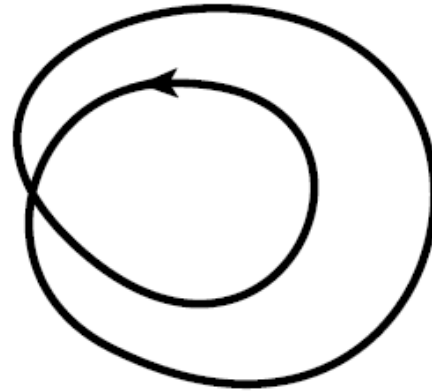
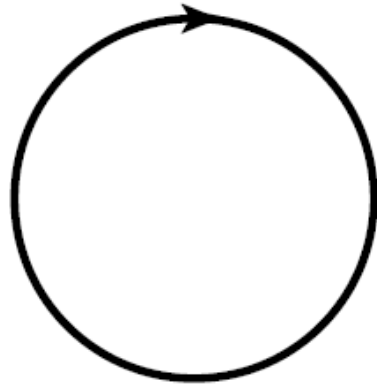
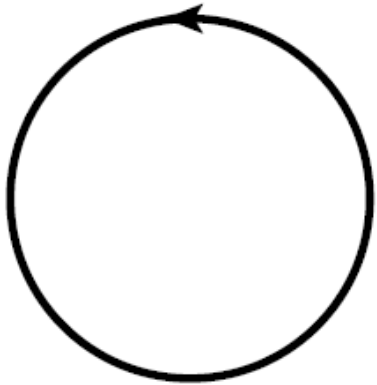
# Signed Curvature on Plane Curves

$$T(s) = (\cos \theta(s), \sin \theta(s))$$



$$\begin{aligned} T'(s) &= \theta'(s)(-\sin \theta(s), \cos \theta(s)) \\ &:= \kappa(s)N(s) \end{aligned}$$

# Turning Numbers



+1

-1

+2

0

# Recovering Theta

$$\theta'(s) = \kappa(s)$$



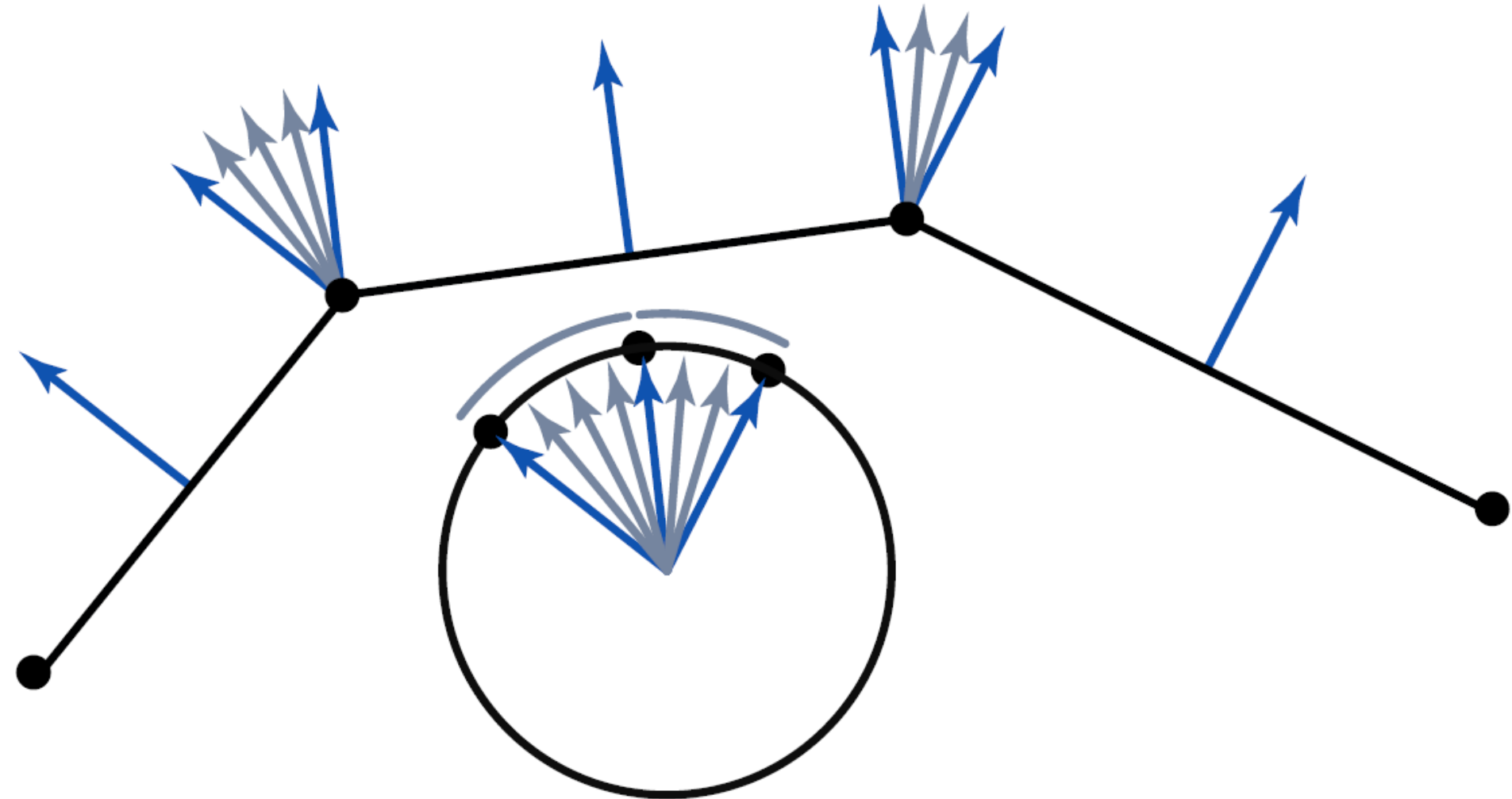
$$\Delta\theta = \int_{s_0}^{s_1} \kappa(s) ds$$

# Turning Number Theorem

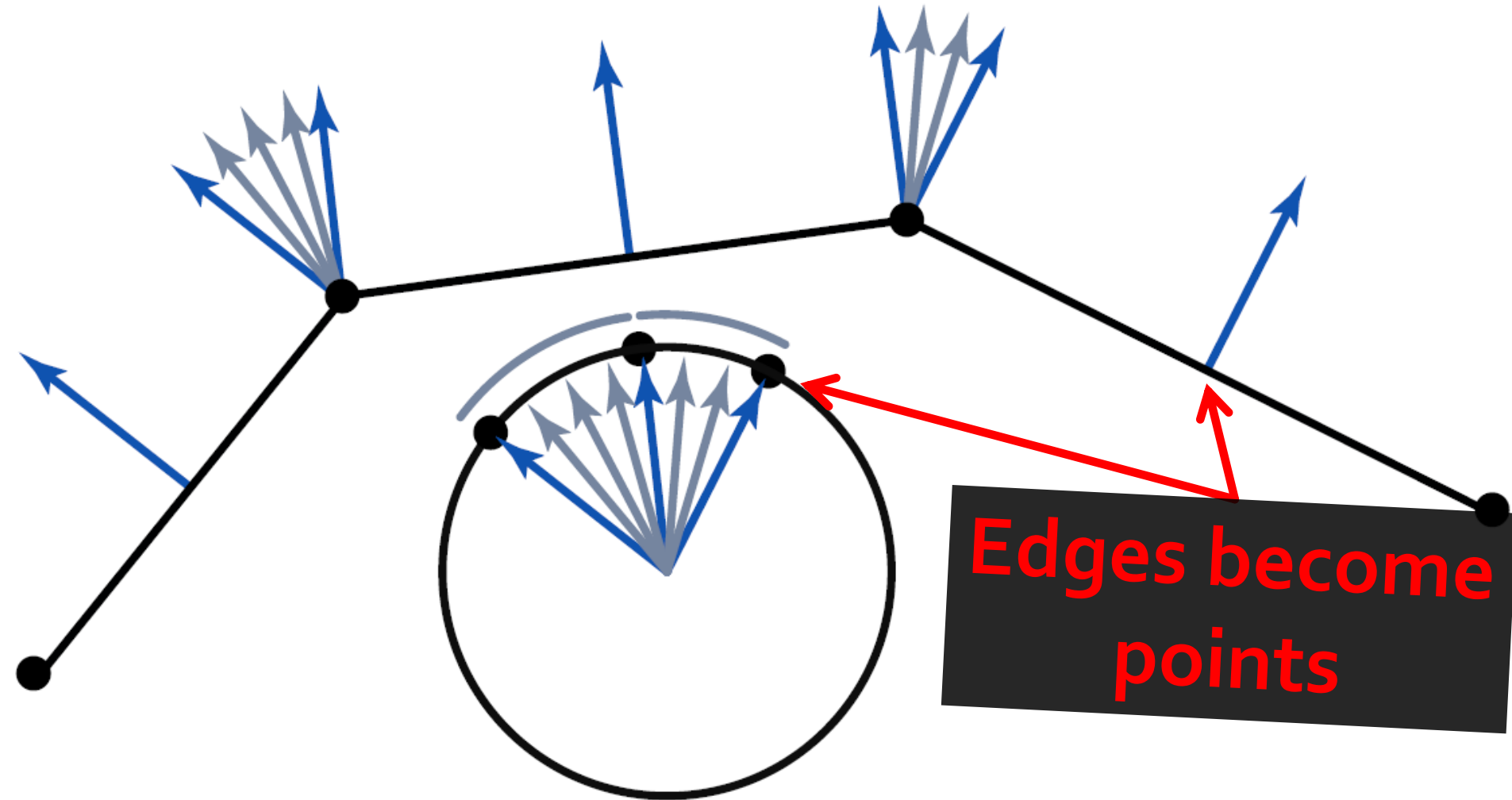
$$\int_{\Omega} \kappa(s) ds = 2\pi k$$

A “global” theorem!

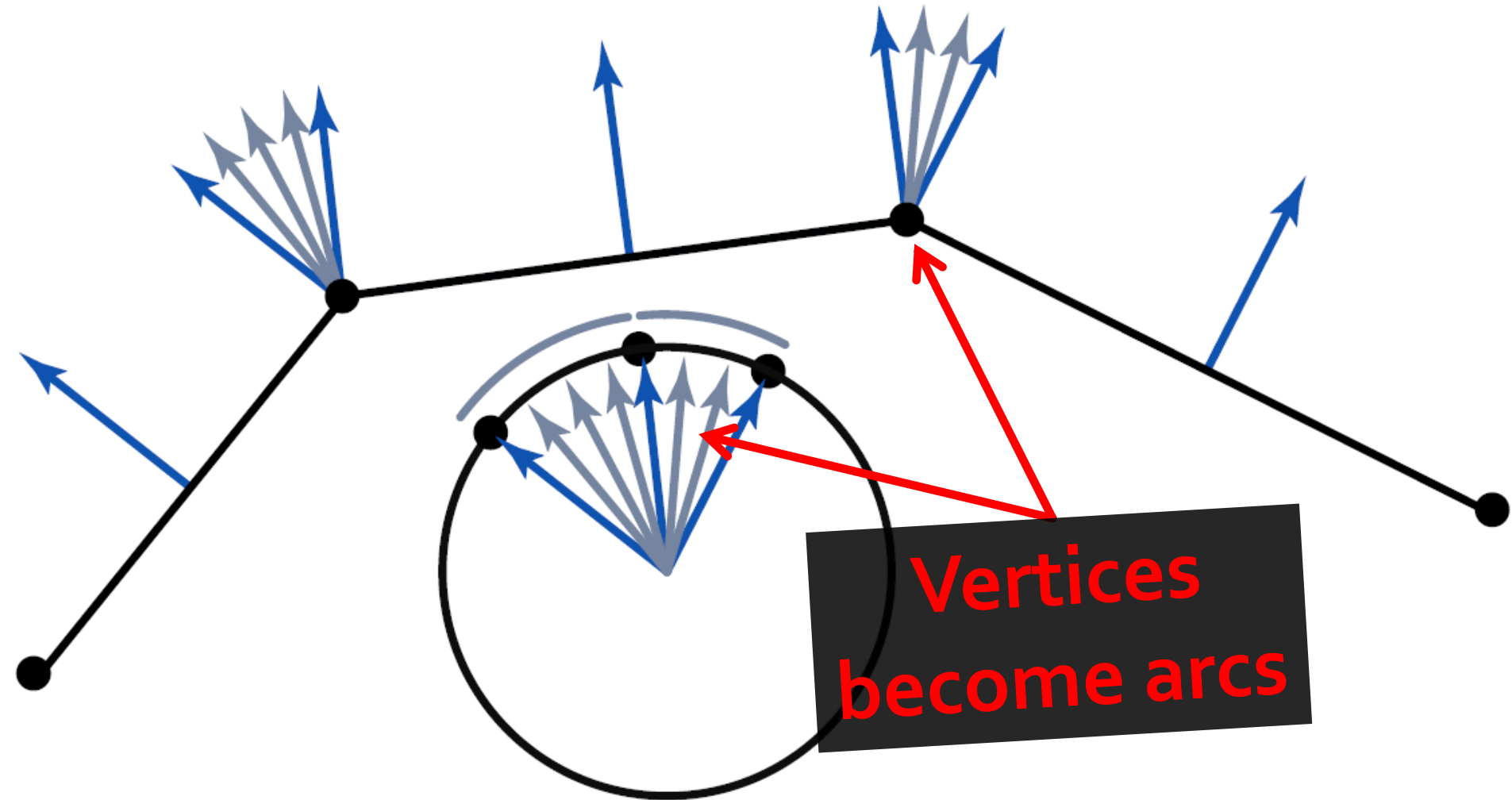
# Discrete Gauss Map



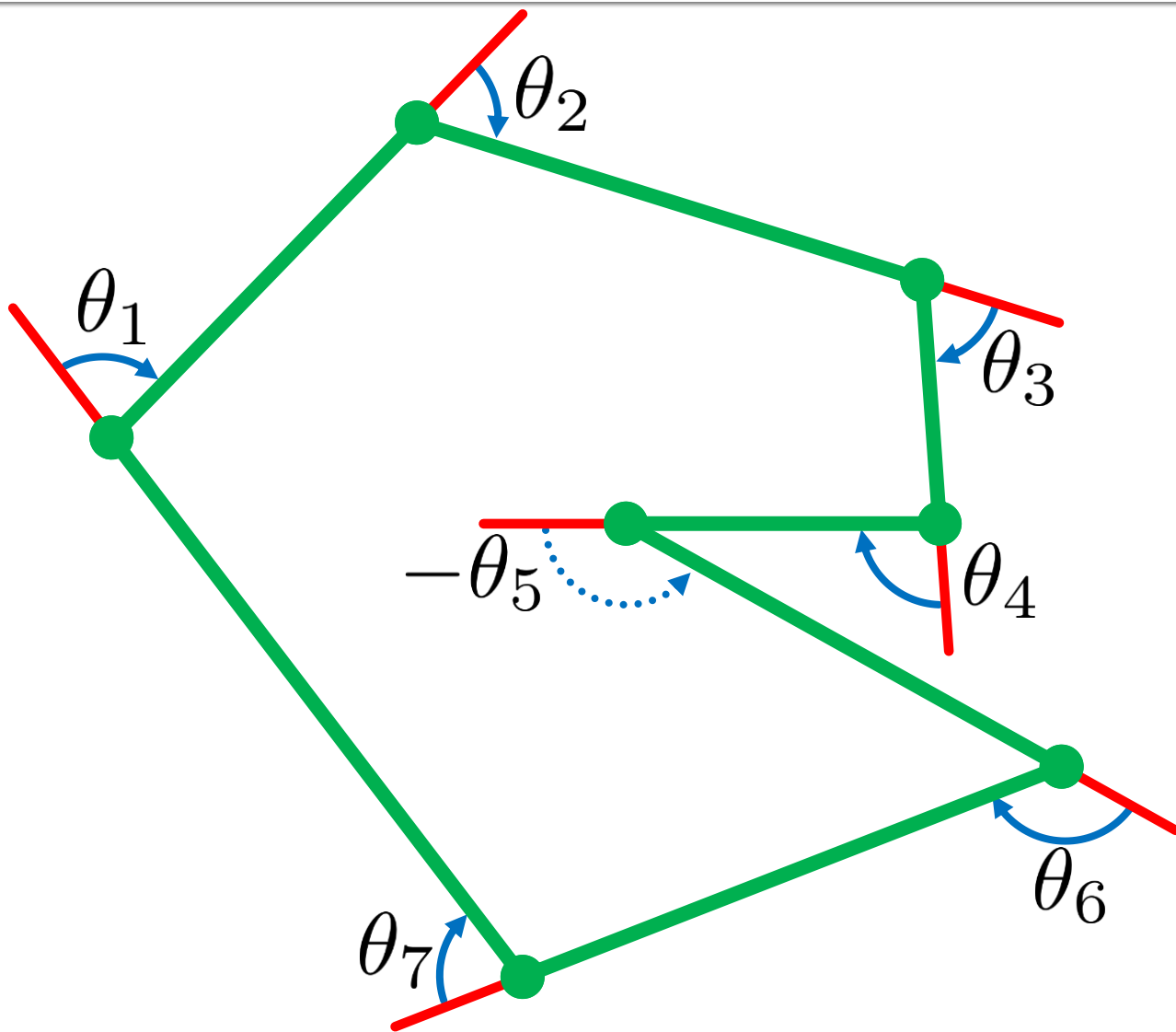
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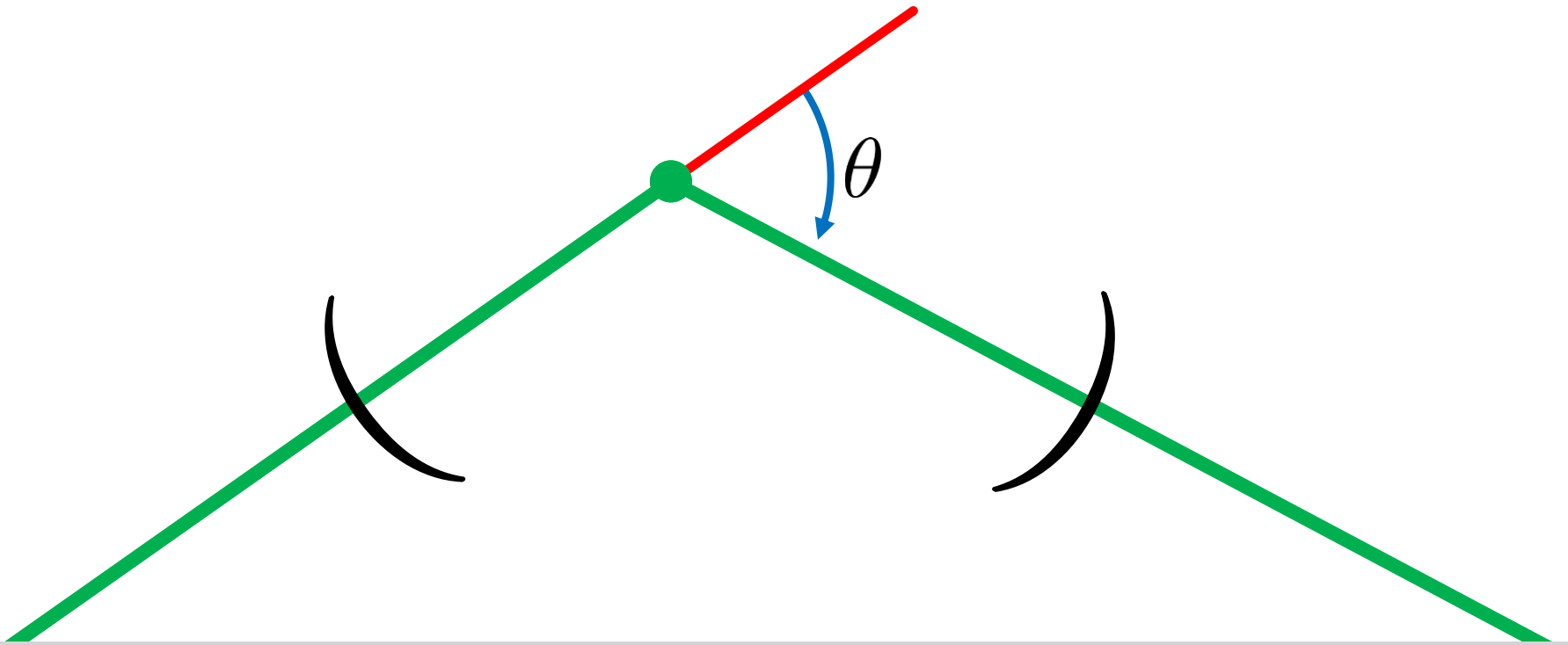
# Key Observation



$$\sum_i \theta_i = 2\pi k$$



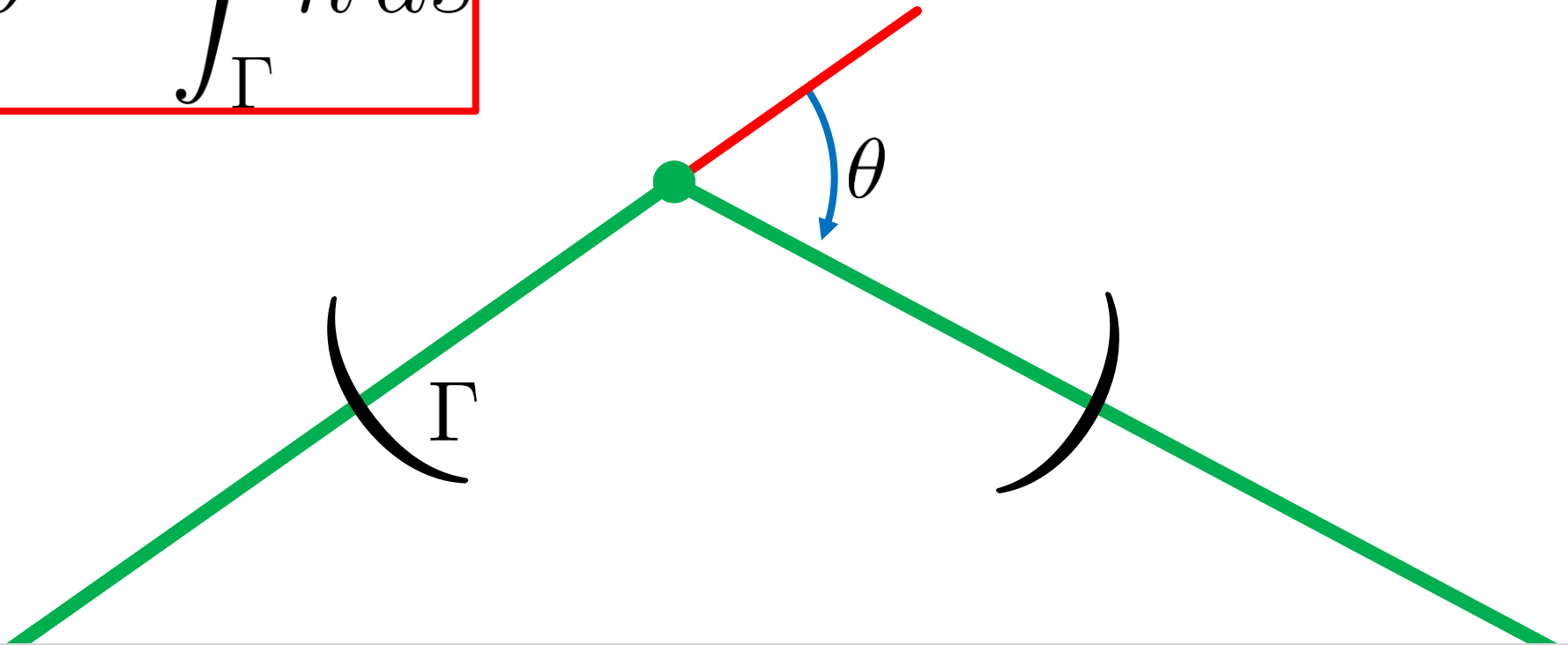
# What's Going On?



**Total change in curvature**

# What's Going On?

$$\theta = \int_{\Gamma} \kappa ds$$

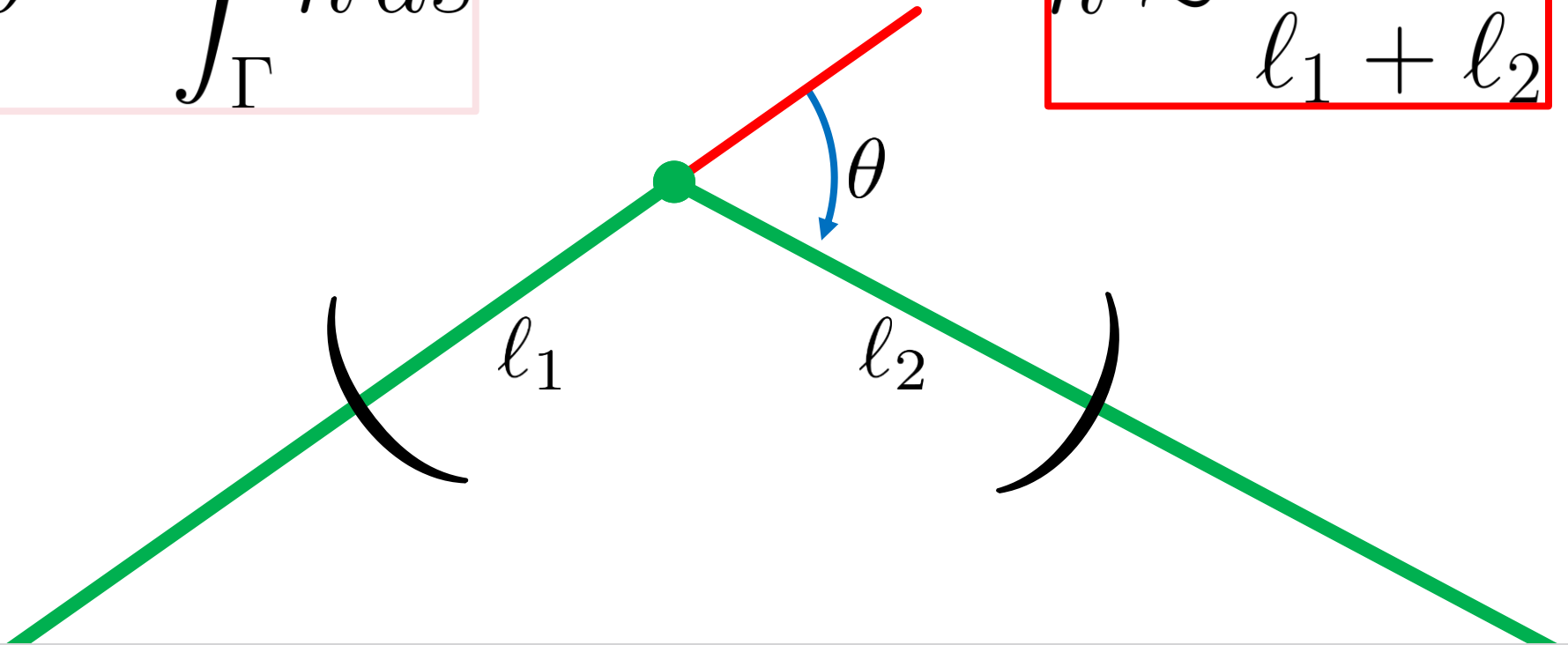


**Total change in curvature**

# What's Going On?

$$\theta = \int_{\Gamma} \kappa ds$$

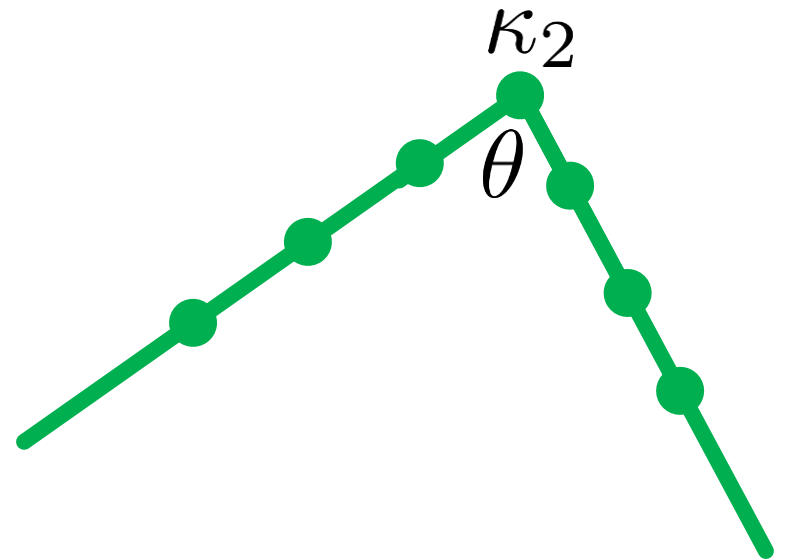
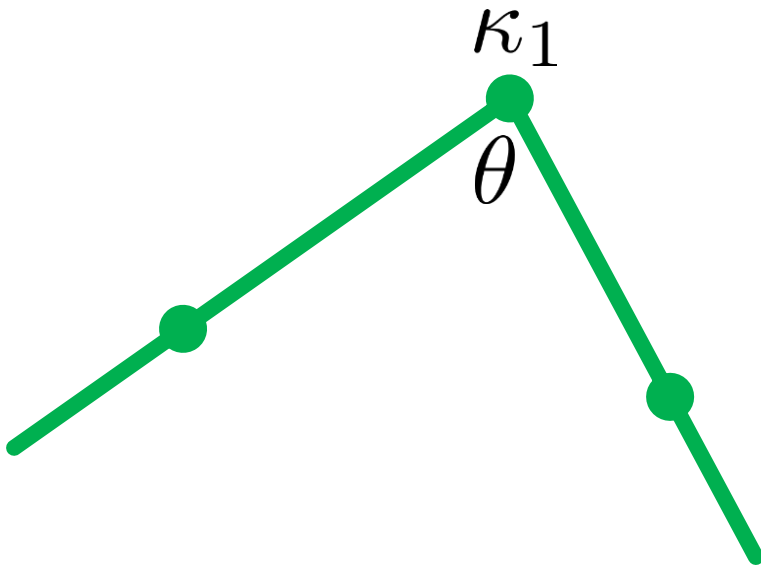
$$\kappa \approx \frac{\theta}{l_1 + l_2}$$



**Total change in curvature**

# Interesting Distinction

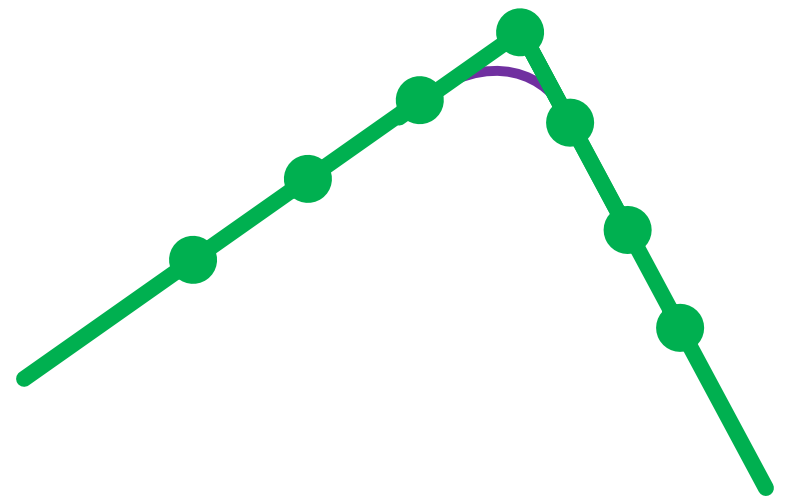
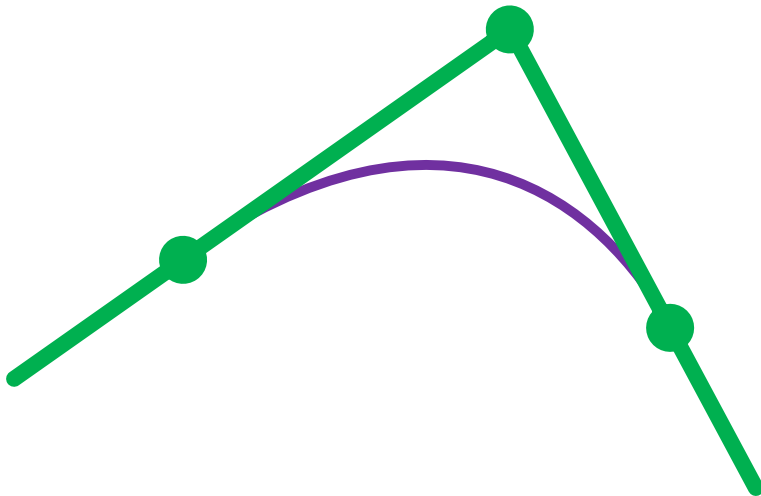
$$\kappa_1 \neq \kappa_2$$



Same integrated curvature

# Interesting Distinction

$$\kappa_1 \neq \kappa_2$$

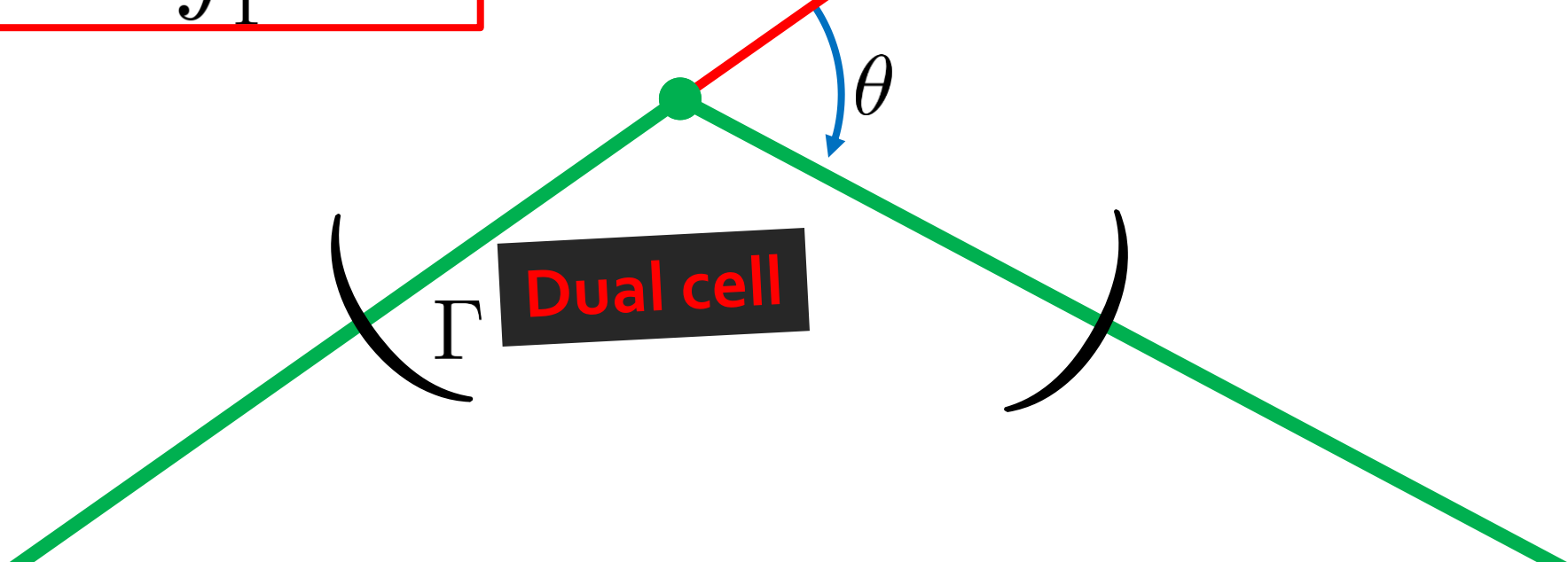


Same integrated curvature

# What's Going On?

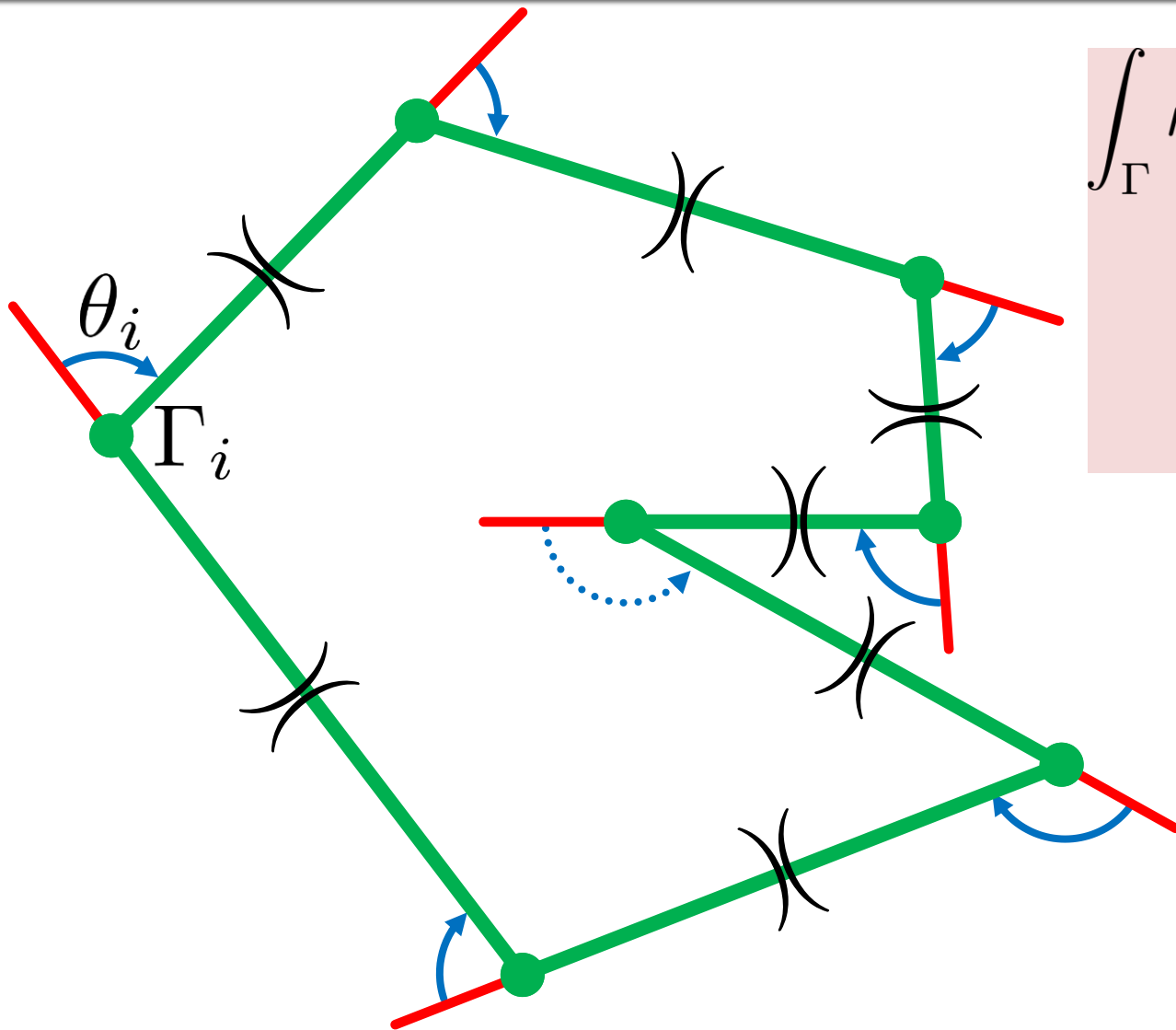
$$\theta = \int_{\Gamma} \kappa ds$$

Integrated quantity



Total change in curvature

# Discrete Turning Angle Theorem



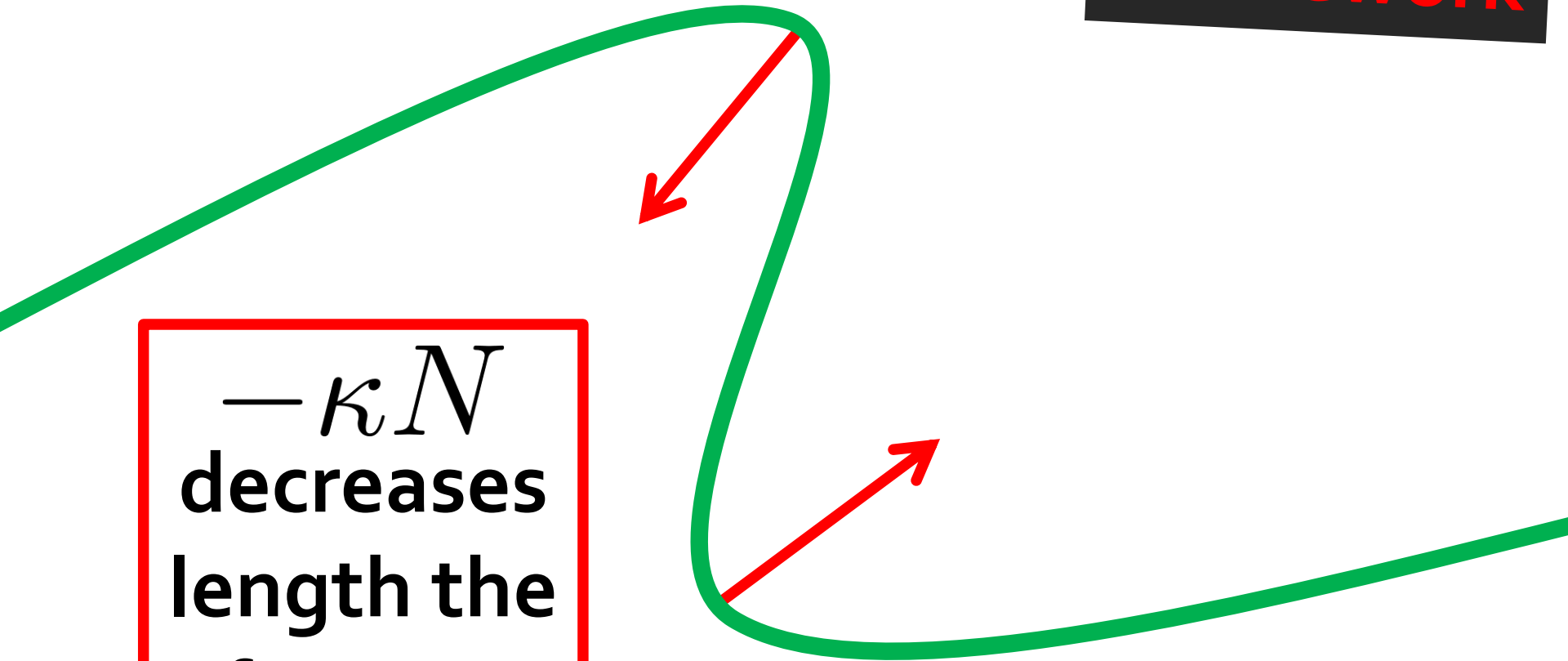
$$\begin{aligned}\int_{\Gamma} \kappa ds &= \sum_i \int_{\Gamma_i} \kappa ds \\ &= \sum_i \theta_i \\ &= 2\pi k\end{aligned}$$

**Preserved  
structure!**

# Alternative Definition

Homework

$-\kappa N$   
decreases  
length the  
fastest.

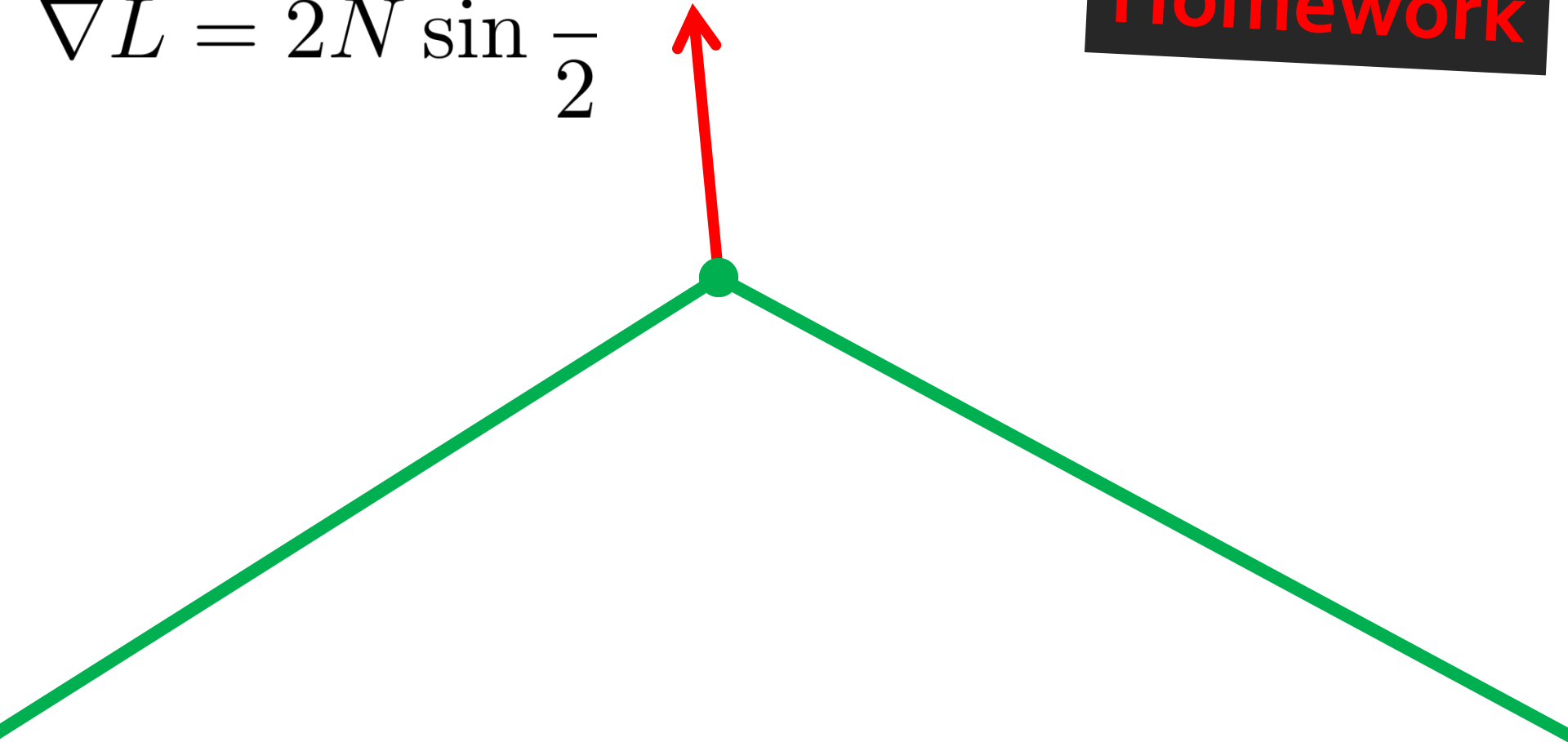




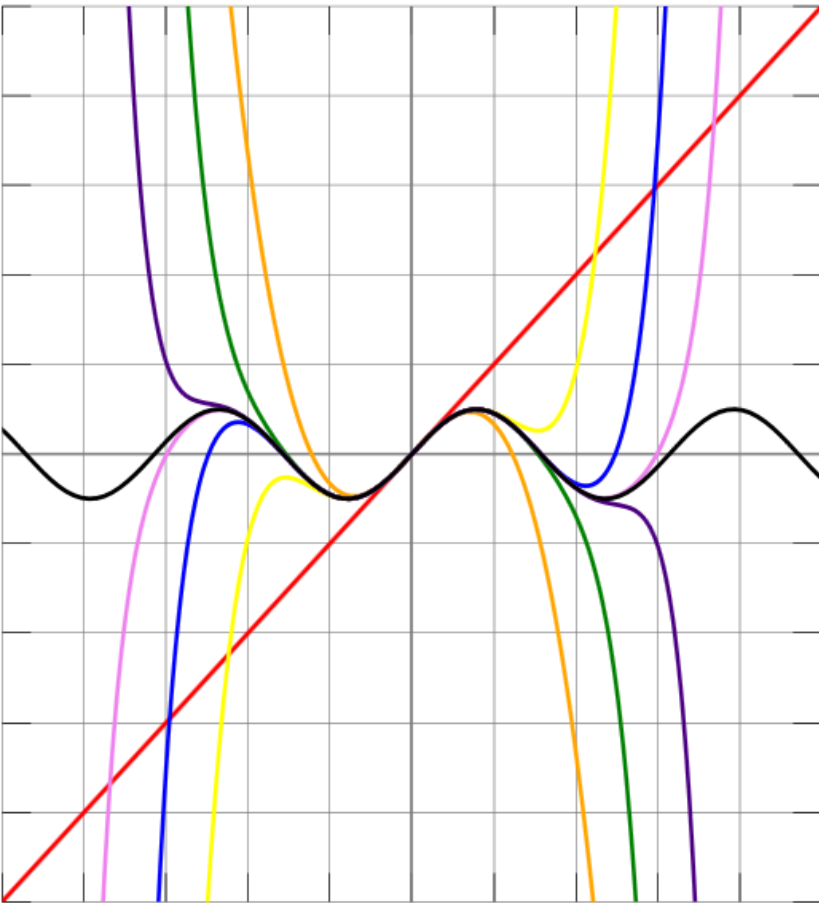
# Discrete Case

$$\nabla L = 2N \sin \frac{\theta}{2}$$

**Homework**



# For Small $\theta$



$$2 \sin \frac{\theta}{2} \approx 2 \cdot \frac{\theta}{2} \\ = \theta$$

**Same behavior in the limit**

# Remaining Question

**Does discrete curvature  
converge in limit?**

*Yes!*

# Remaining Question

Does discrete curvature  
converge in limit?

Questions:

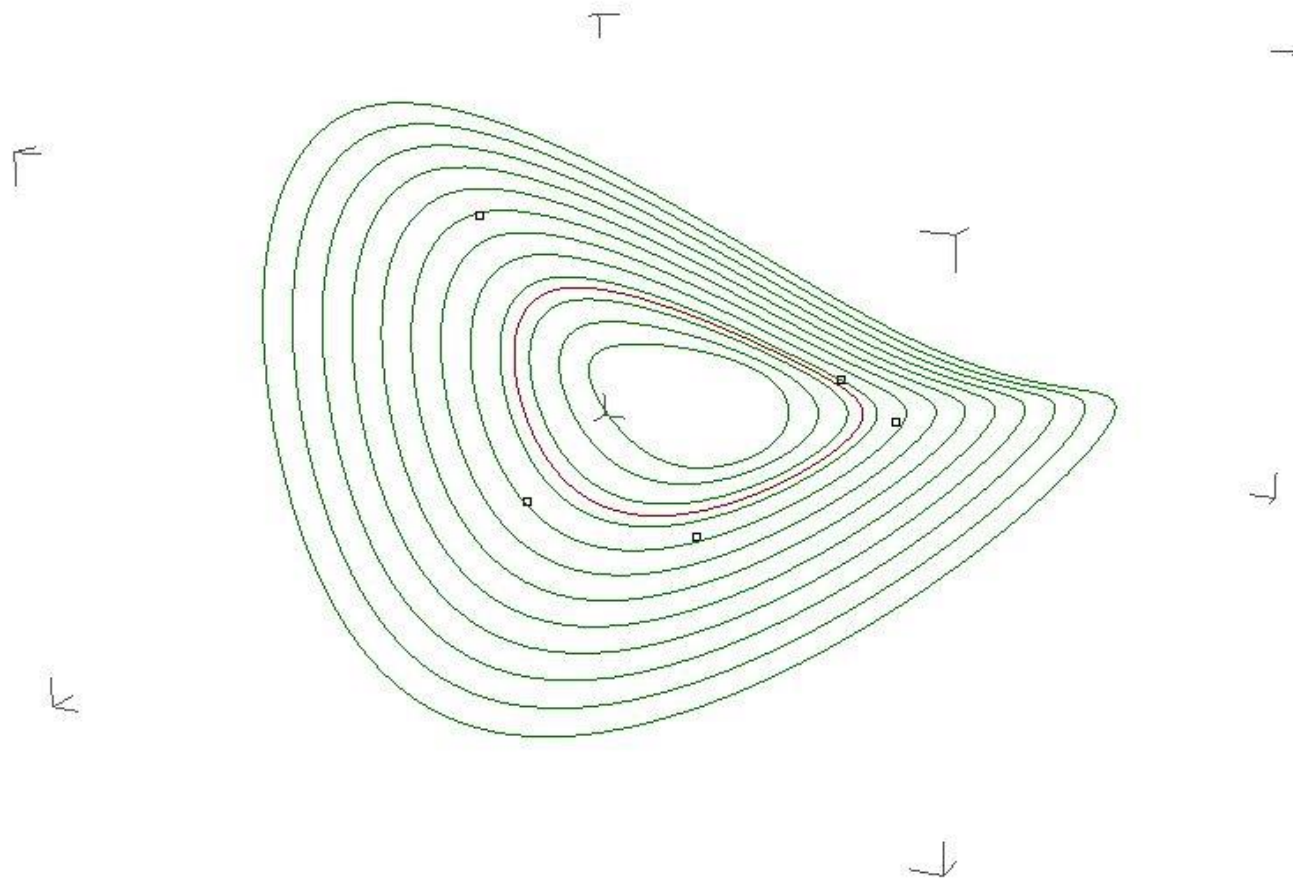
- Type of convergence?
- Sampling?
- Class of curves?

*Yes!*

# Discrete Differential Geometry

- **Different** discrete behavior
- **Same** convergence

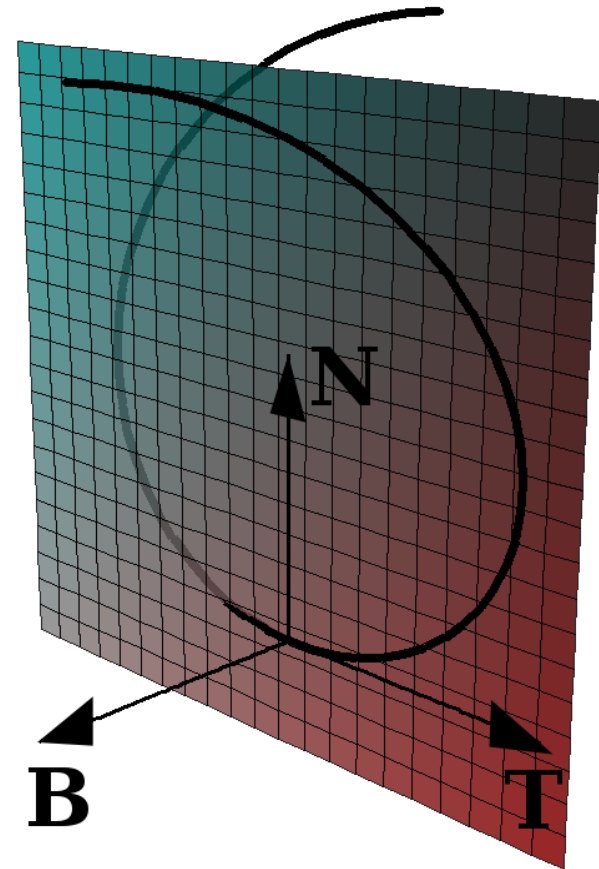
# Next



<http://www.grasshopper3d.com/forum/topics/offsetting-3d-curves-component>

## Curves in 3D

# Frenet Frame

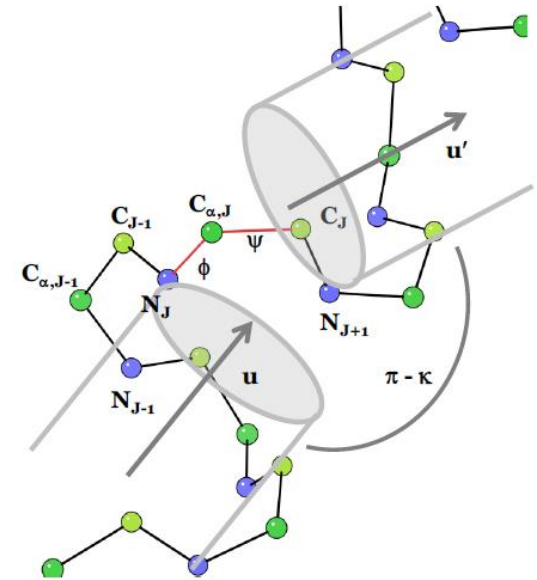
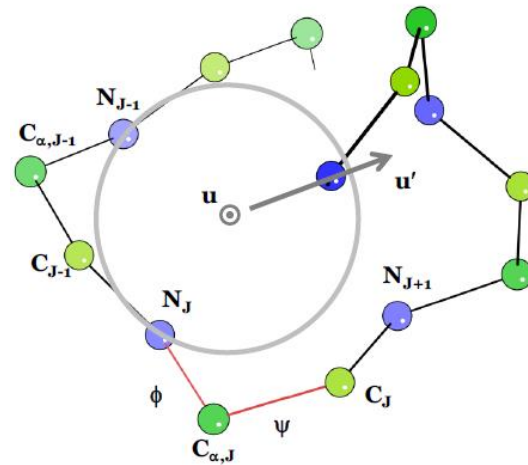


$$\frac{d}{ds} \begin{pmatrix} T \\ N \\ B \end{pmatrix} = \begin{pmatrix} 0 & \kappa & 0 \\ -\kappa & 0 & \tau \\ 0 & -\tau & 0 \end{pmatrix} \begin{pmatrix} T \\ N \\ B \end{pmatrix}$$

# Application



**NMR scanner**



**Kinked alpha helix**

**Structure Determination of Membrane Proteins Using Discrete Frenet Frame  
and Solid State NMR Restraints**

Achuthan and Quine

*Discrete Mathematics and its Applications*, ed. M. Sethumadhavan (2006)



# Potential Discretization

$$T_j = \frac{p_{j+1} - p_j}{\|p_{j+1} - p_j\|}$$

$$B_j = t_{j-1} \times t_j$$

$$N_j = b_j \times t_j$$

**Discrete Frenet frame**

$$T_k = R(B_k, \theta_k) T_{k-1}$$

$$B_{k+1} = R(T_k, \phi_k) B_k$$

**“Bond and torsion angles”**  
(derivatives converge to  $\kappa$   
and  $\tau$ , resp.)

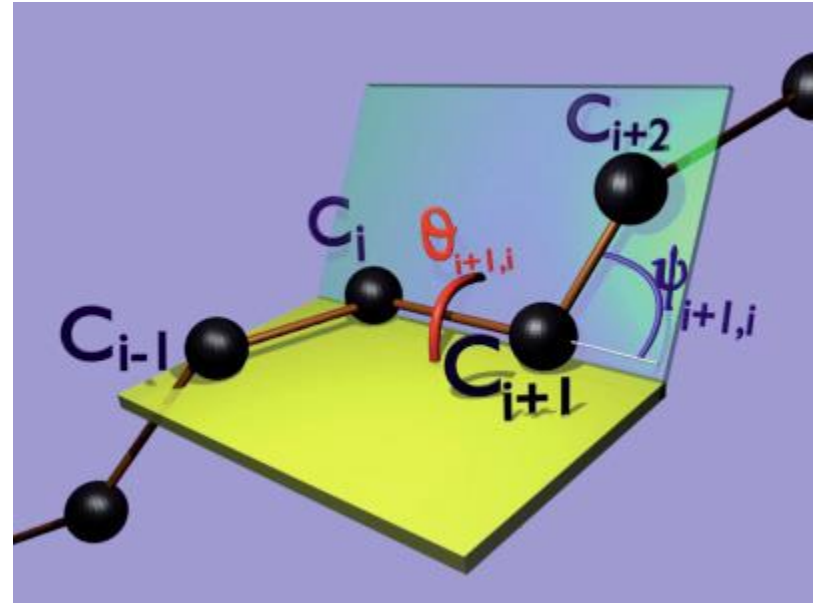
Discrete frame introduced in:

**The resultant electric moment of complex molecules**

Eyring, Physical Review, 39(4):746—748, 1932.

# Transfer Matrix

$$\begin{pmatrix} T_{i+1} \\ N_{i+1} \\ B_{i+1} \end{pmatrix} = R_{i+1,i} \begin{pmatrix} T_i \\ N_i \\ B_i \end{pmatrix}$$



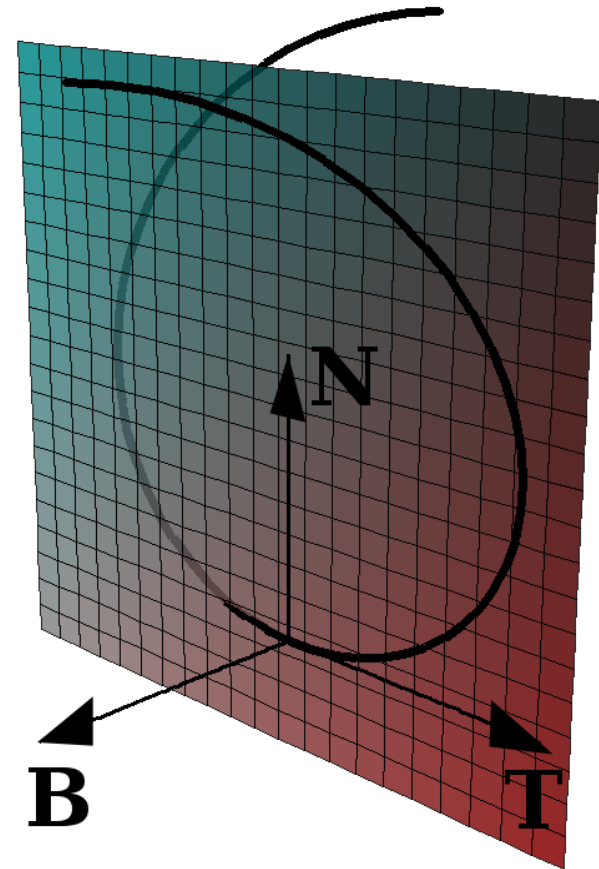
**Discrete construction that works for fractal curves  
and converges in continuum limit.**

Discrete Frenet Frame, Inflection Point Solitons, and Curve Visualization  
with Applications to Folded Proteins

Hu, Lundgren, and Niemi  
*Physical Review E* 83 (2011)

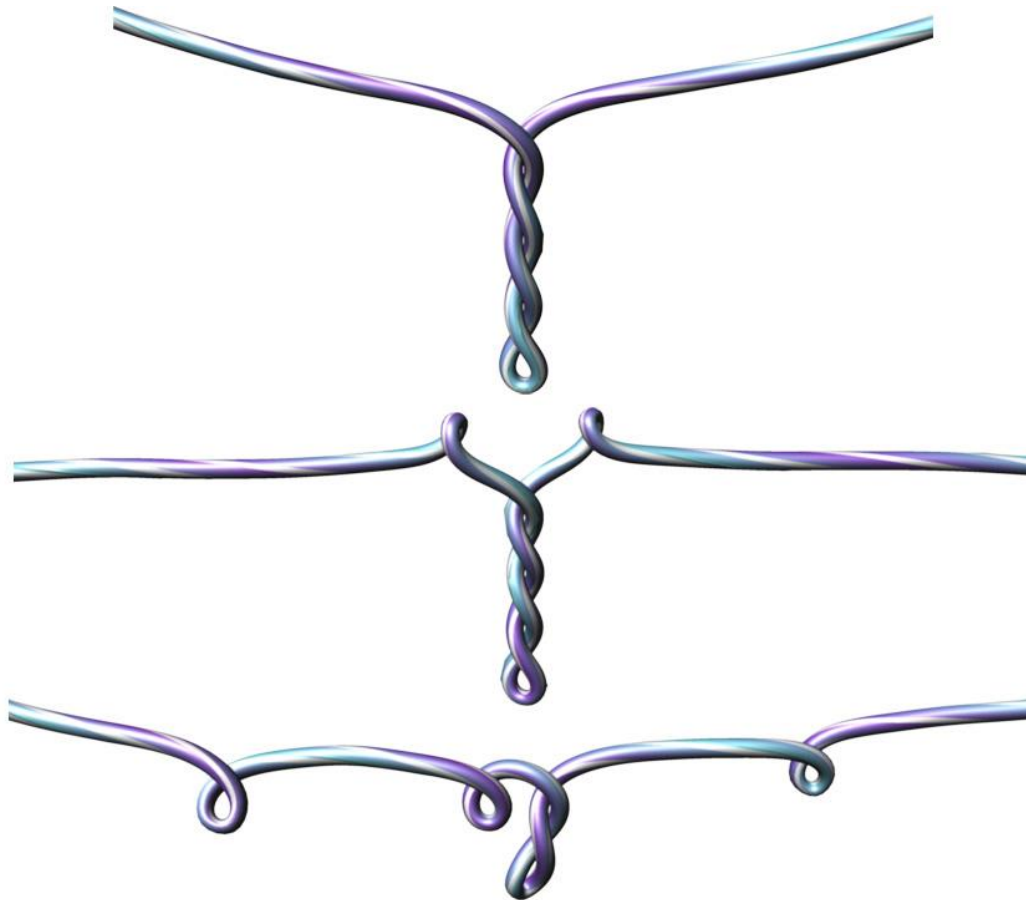
# Frenet Frame: Issue

$\kappa = 0?$



$$\frac{d}{ds} \begin{pmatrix} T \\ N \\ B \end{pmatrix} = \begin{pmatrix} 0 & \boxed{\kappa} & 0 \\ -\kappa & 0 & \tau \\ 0 & -\tau & 0 \end{pmatrix} \begin{pmatrix} T \\ N \\ B \end{pmatrix}$$

# Segments Not Always Enough

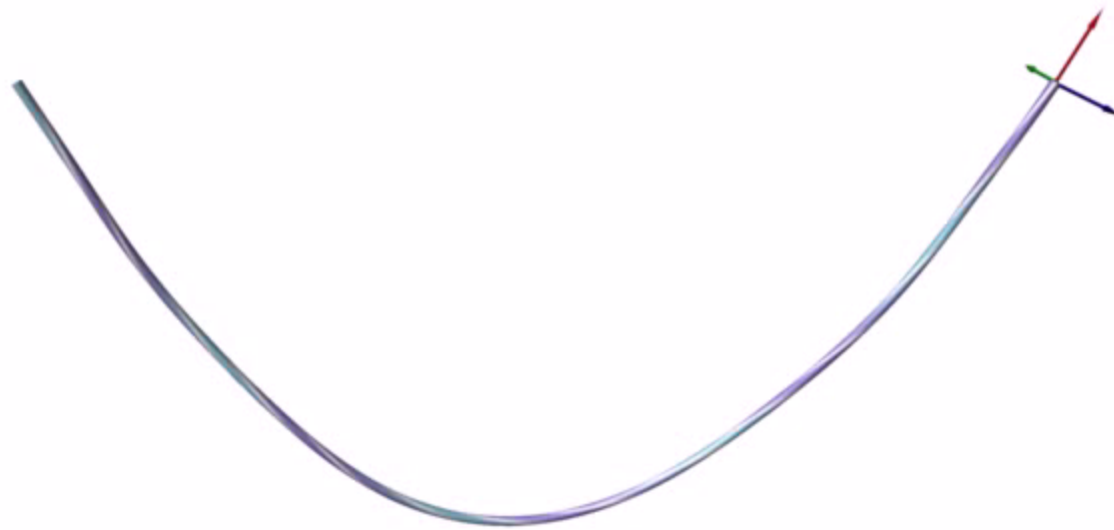


## Discrete Elastic Rods

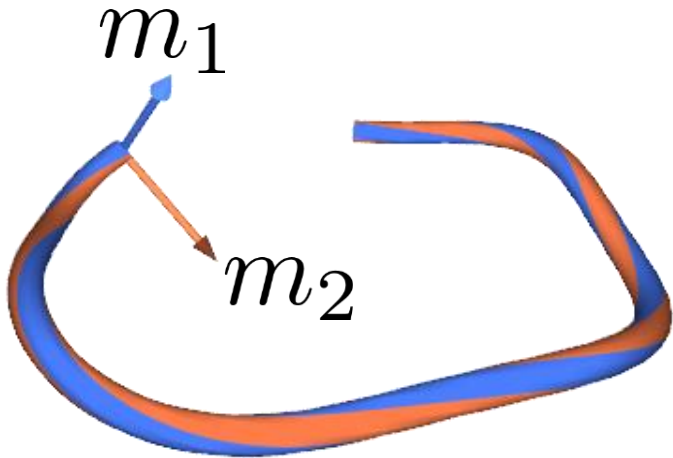
Bergou, Wardetzky, Robinson, Audoly, and Grinspun

*SIGGRAPH* 2008

# Simulation Goal



# Adapted Framed Curve



$$\Gamma = \{\gamma(s); T, m_1, m_2\}$$

**Material frame**

**Normal part encodes twist**

# Bending Energy

$$E_{\text{bend}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \alpha \kappa^2 ds$$

**Punish turning the steering wheel**

---

$$\begin{aligned} \kappa N &= T' \\ &= (T' \cdot T)T + (T' \cdot m_1)m_1 + (T' \cdot m_2)m_2 \\ &= (T' \cdot m_1)m_1 + (T' \cdot m_2)m_2 \\ &:= \omega_1 m_1 + \omega_2 m_2 \end{aligned}$$

# Bending Energy

$$E_{\text{bend}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \alpha(\omega_1^2 + \omega_2^2) ds$$

**Punish turning the steering wheel**

---

$$\begin{aligned} \kappa N &= T' \\ &= (T' \cdot T)T + (T' \cdot m_1)m_1 + (T' \cdot m_2)m_2 \\ &= (T' \cdot m_1)m_1 + (T' \cdot m_2)m_2 \\ &:= \omega_1 m_1 + \omega_2 m_2 \end{aligned}$$



# Twisting Energy

$$E_{\text{twist}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \beta m^2 ds$$

**Punish non-tangent change in material frame**

---

$$\begin{aligned} m &:= m'_1 \cdot m_2 \\ &= \frac{d}{dt} (m_1 \cdot m_2) - m_1 \cdot m'_2 \\ &= -m_1 \cdot m'_2 \end{aligned}$$

# Twisting Energy

$$E_{\text{twist}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \beta m^2 ds$$

Punish non-tangent change in material frame

---

$$m := m'_1 \cdot m_2$$

$$= \frac{d}{dt} (m_1 \cdot m_2) - m_1 \cdot m'_2$$

$$= -m_1 \cdot m'_2$$

Swapping  $m_1$  and  $m_2$   
does not affect  $E_{\text{twist}}$ !

# Which Basis to Use

## THERE IS MORE THAN ONE WAY TO FRAME A CURVE

RICHARD L. BISHOP

The Frenet frame of a 3-times continuously differentiable (that is,  $C^3$ ) non-degenerate curve in euclidean space has long been the standard vehicle for analysing properties of the curve invariant under euclidean motions. For arbitrary moving frames, that is, orthonormal basis fields, we can express the derivatives of the frame with respect to the curve parameter in terms of the frame itself, and due to orthonormality the coefficient matrix is always skew-symmetric. Thus it generally has three nonzero entries. The Frenet frame gains part of its special significance from the fact that one of the three derivatives is always zero. Another feature of the Frenet frame is that it is *adapted* to the curve: the members are either tangent to or perpendicular to the curve. It is the purpose of this paper to show that there are other frames which have these same advantages and to compare them with the Frenet frame.

**1. Relatively parallel fields.** We say that a normal vector field  $M$  along a curve is *relatively parallel* if its derivative is tangential. Such a field turns only whatever amount is necessary for it to remain normal, so it is as close to being parallel as possible without losing normality. Since its derivative is perpendicular to it, a relatively parallel normal field has constant length. Such fields occur classically in

# Bishop Frame

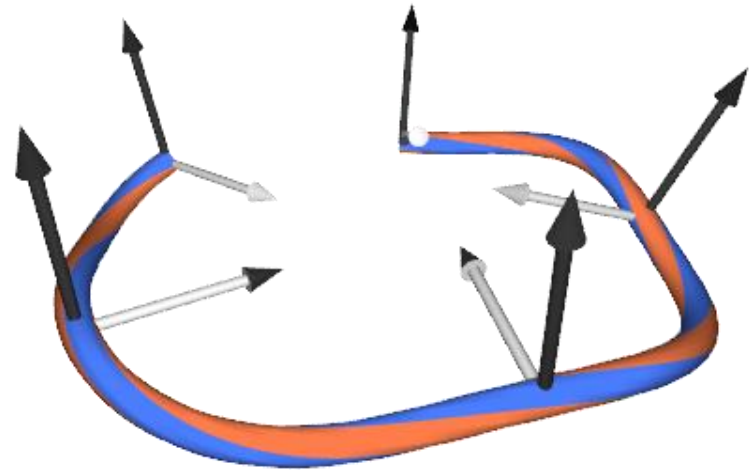
$$T' = \Omega \times T$$

$$u' = \Omega \times u$$

$$v' = \Omega \times v$$

$\Omega := \kappa B$  (“curvature binormal”)

**Darboux vector**



**Most relaxed frame**

# Bishop Frame

$$T' = \Omega \times T$$

$$u' = \Omega \times u$$

$$v' = \Omega \times v$$

$$\Omega := \kappa B \text{ (“curvature binormal”)}$$

$$u' \cdot v \equiv 0$$

**No twist**  
 (“parallel transport”)

**Most relaxed frame**

# Curve-Angle Representation

$$m_1 = u \cos \theta + v \sin \theta$$

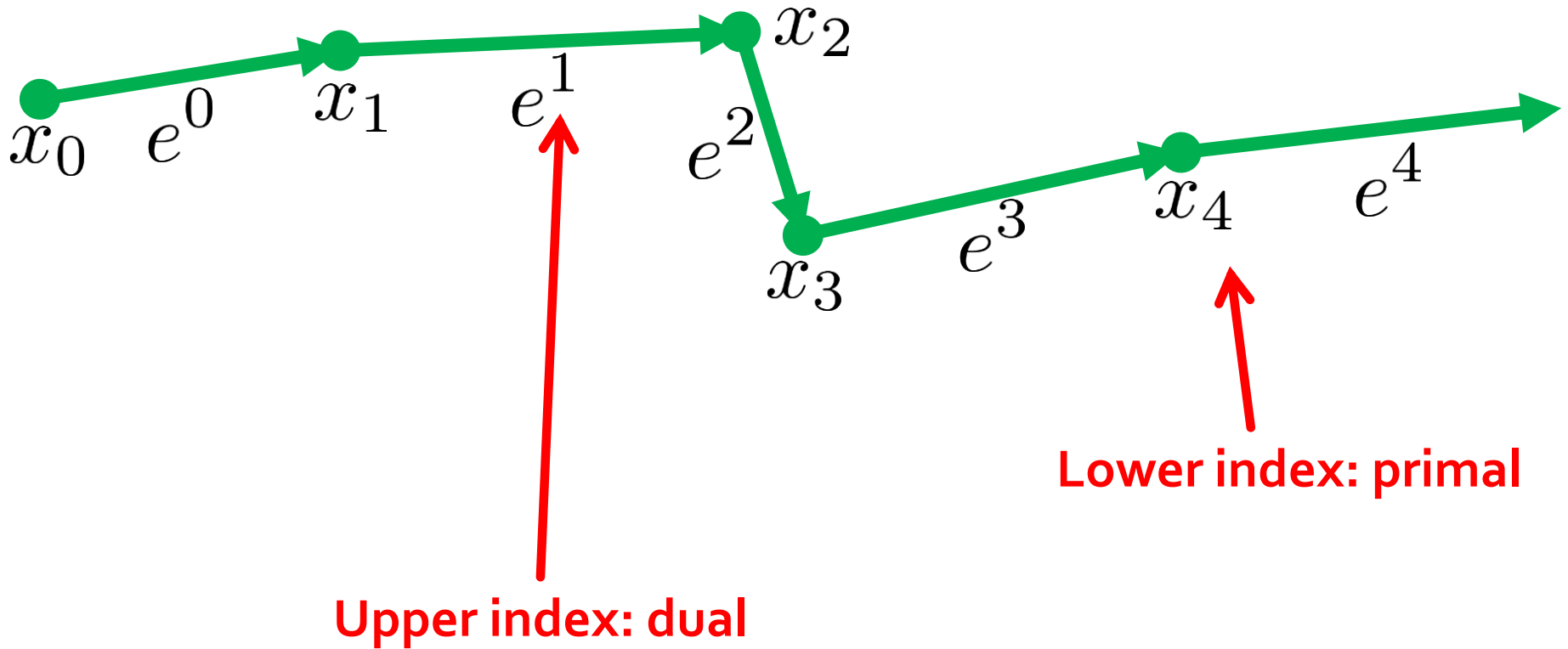
$$m_2 = -u \sin \theta + v \cos \theta$$

$$E_{\text{twist}}(\Gamma) := \frac{1}{2} \int_{\Gamma} \beta(\theta')^2 ds$$

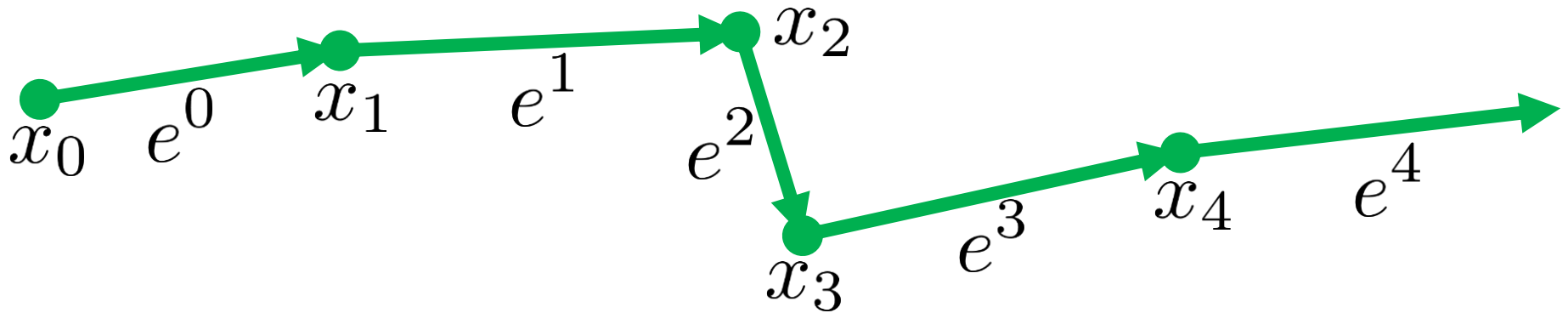
**Degrees of freedom for elastic energy:**

- Shape of curve
- Twist angle  $\theta$

# Discrete Kirchoff Rods



# Discrete Kirchoff Rods

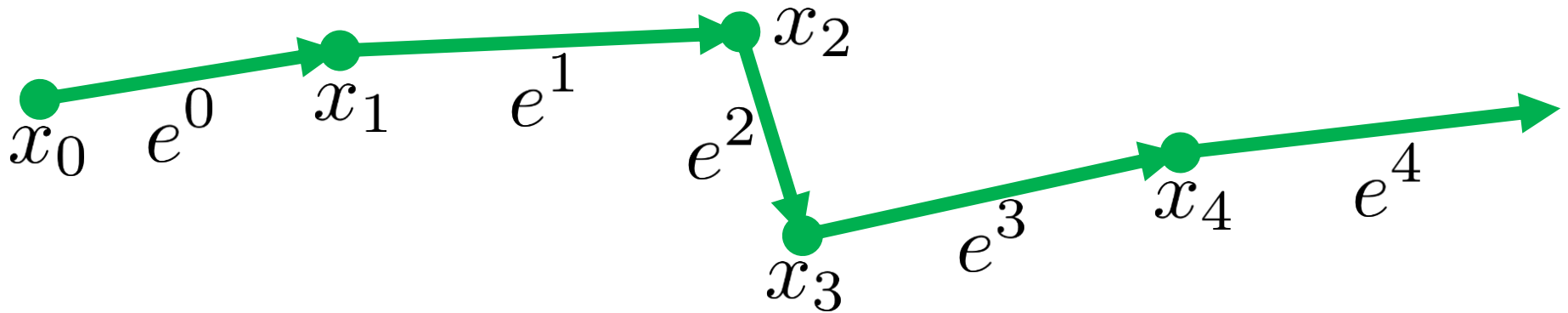


$$T^i := \frac{e^i}{\|e^i\|}$$

**Tangent unambiguous on edge**



# Discrete Kirchoff Rods



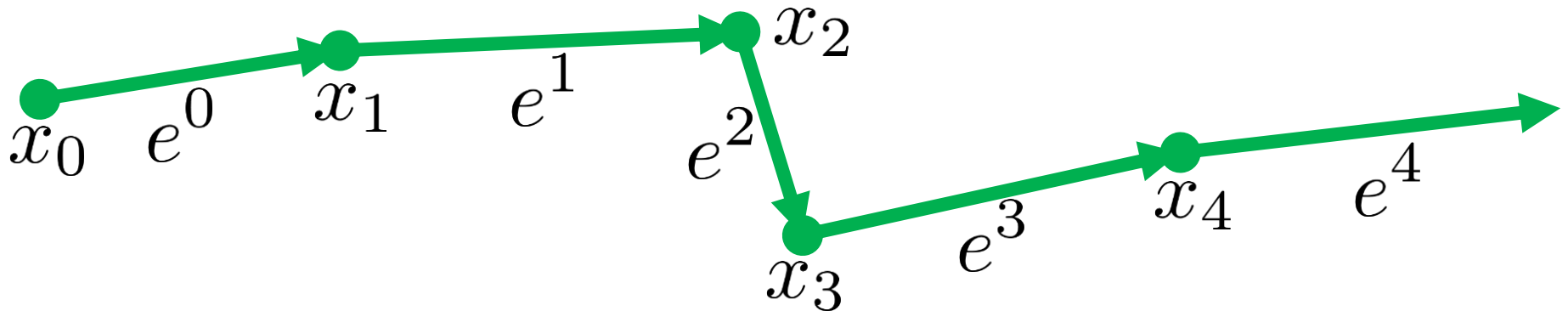
$$\kappa_i := 2 \tan \frac{\phi_i}{2}$$

Turning angle

Yet another curvature!

Integrated curvature

# Discrete Kirchoff Rods



$$\kappa_i := 2 \tan \frac{\phi_i}{2}$$

$$(\kappa B)_i := \frac{2e^{i-1} \times e^i}{\|e^{i-1}\| \|e^i\| + e^{i-1} \cdot e^i}$$

Orthogonal to osculating plane,  
norm  $\kappa_i$

Yet another curvature!

**Darboux vector**

# Bending Energy

$$E_{\text{bend}}(\Gamma) := \frac{\alpha}{2} \sum_i \left( \frac{(\kappa B)_i}{l_i/2} \right)^2 \frac{l_i}{2}$$
$$= \alpha \sum_i \frac{\|(\kappa B)_i\|^2}{l_i}$$

Can extend for  
natural bend

Convert to pointwise and integrate

# Discrete Parallel Transport

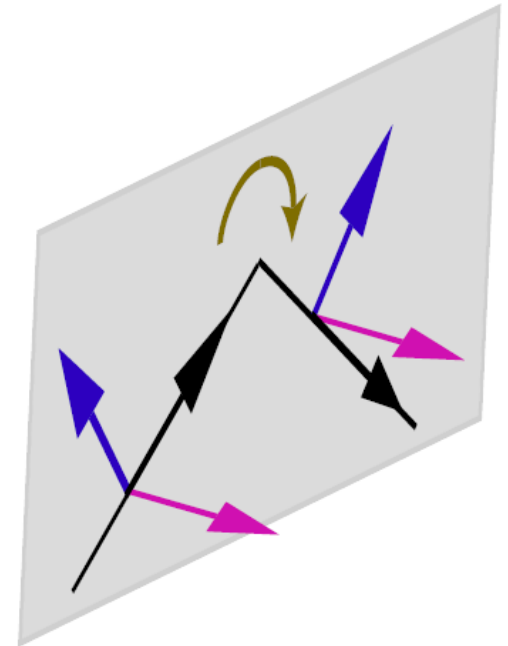
$$P_i(T^{i-1}) = T^i$$

$$P_i(T^{i-1} \times T^i) = T^{i-1} \times T^i$$

- Map tangent to tangent
- Preserve binormal
- Orthogonal

$$u^i = P_i(u^{i-1})$$

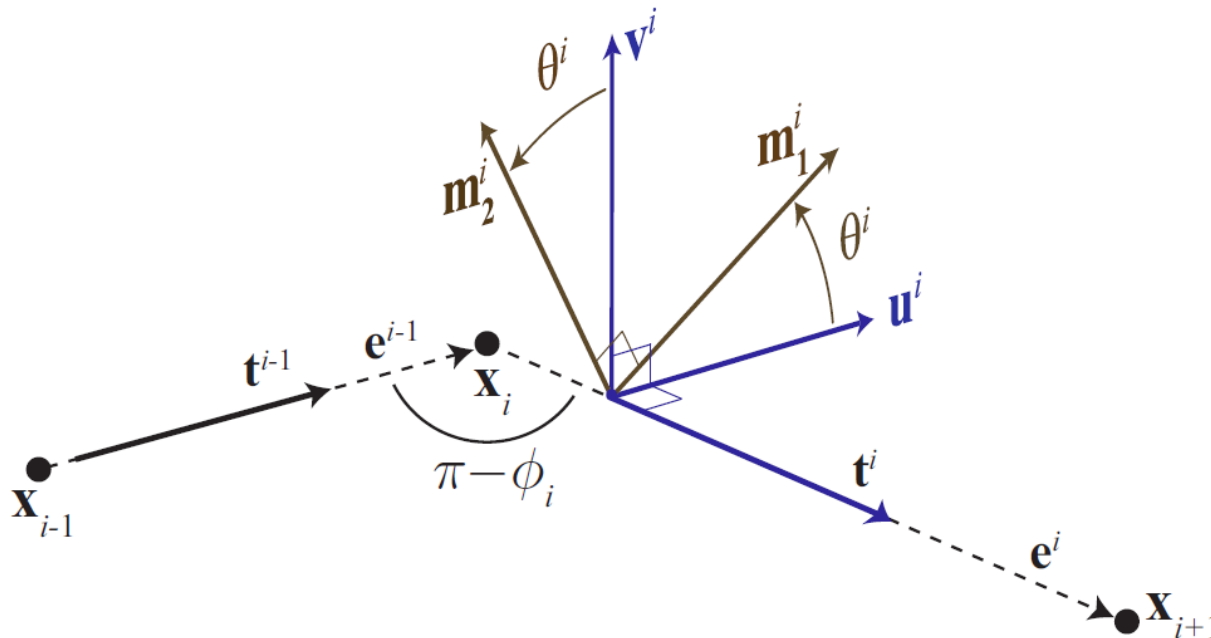
$$v^i = T^i \times u^i$$



# Discrete Material Frame

$$m_1^i = u^i \cos \theta^i + v^i \sin \theta^i$$

$$m_2^i = -u^i \sin \theta^i + v^i \cos \theta^i$$



# Discrete Twisting Energy

$$E_{\text{twist}}(\Gamma) := \beta \sum_i \frac{(\theta^i - \theta^{i-1})^2}{l_i}$$

Note  $\theta_0$  can be arbitrary

# Simulation

`\omit{physics}`

*Worth reading!*

# Extension and Speedup

## Discrete Viscous Threads

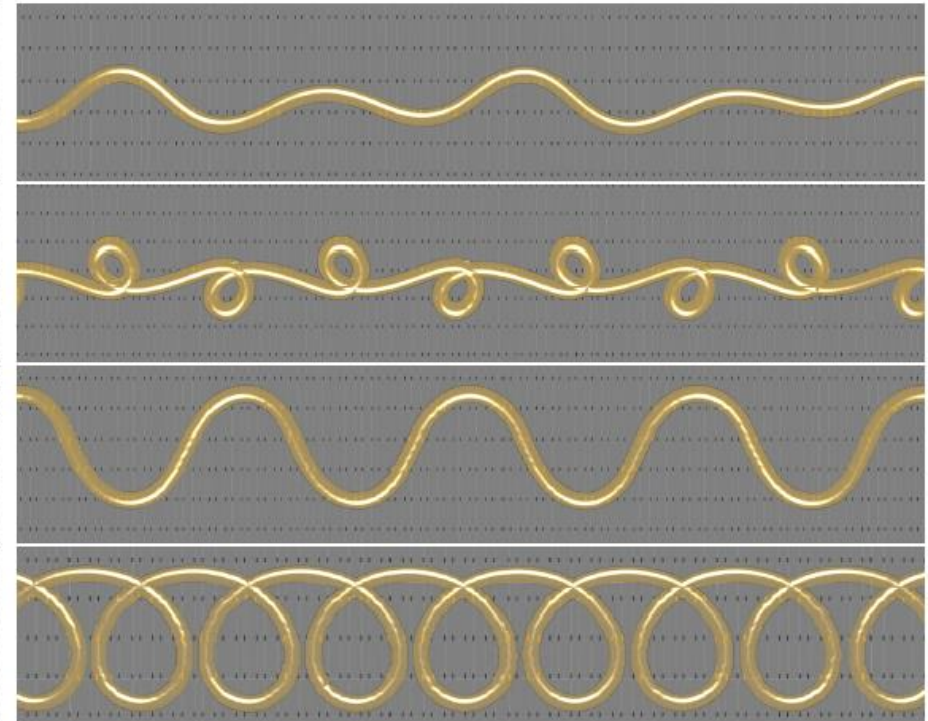
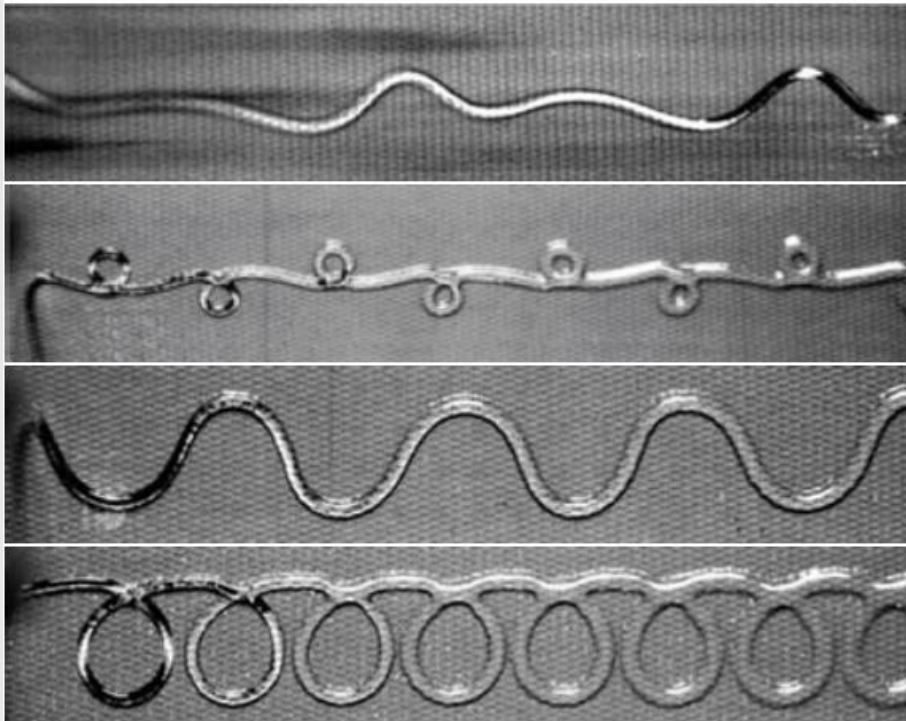
Miklós Bergou  
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Basile Audoly  
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Etienne Vouga  
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Max Wardetzky  
Universität Göttingen

Eitan Grinspun  
Columbia University





# Extension and Speedup

## Discrete Viscous Threads

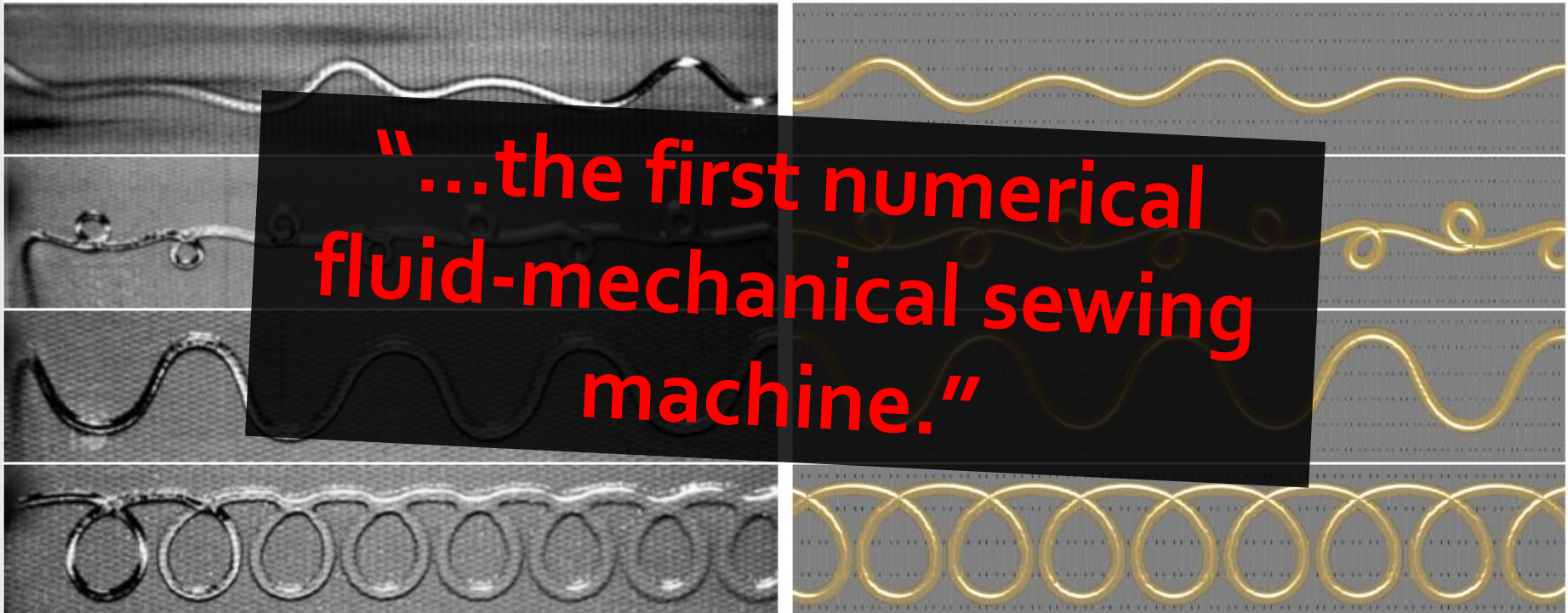
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# Morals

One curve,  
three curvatures.

$$\theta \qquad 2 \sin \frac{\theta}{2} \qquad 2 \tan \frac{\theta}{2}$$

# Morals

Easy theoretical object,  
hard to use.

$$\frac{d}{ds} \begin{pmatrix} T \\ N \\ B \end{pmatrix} = \begin{pmatrix} 0 & \kappa & 0 \\ -\kappa & 0 & \tau \\ 0 & -\tau & 0 \end{pmatrix} \begin{pmatrix} T \\ N \\ B \end{pmatrix}$$

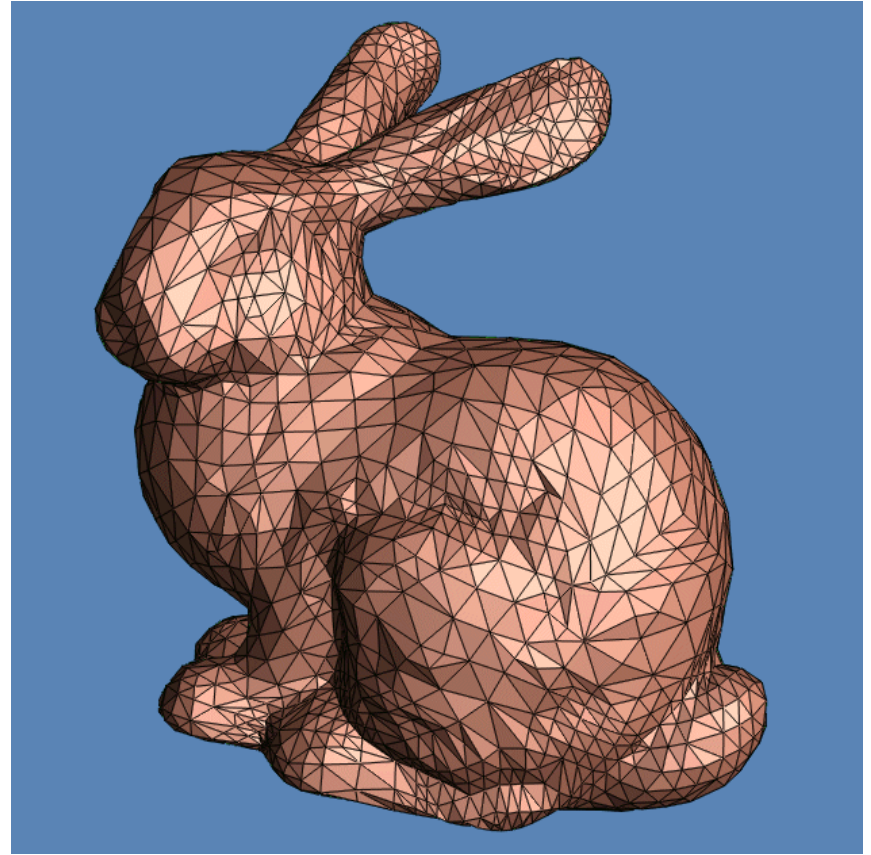
# Morals

Proper frames and DOFs  
go a long way.

$$m_1^i = u^i \cos \theta^i + v^i \sin \theta^i$$

$$m_2^i = -u^i \sin \theta^i + v^i \cos \theta^i$$

# Next



<http://graphics.stanford.edu/data/3Dscanrep/stanford-bunny-cebal-ssh.jpg>  
<http://www.stat.washington.edu/wxs/images/BUNMID.gif>

# Surfaces





# Curves: Continuous and Discrete

Justin Solomon

MIT, Spring 2017

